GENERATING EARLY CONTINENTAL CRUST

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Kurzfassung

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Die Entstehung erster kontinentaler Kruste

Archaische Kratone sind Relikte der geodynamischen Prozesse, die das Antlitz der Erde in ihrer frühen Entwicklung prägten. Sie bestehen aus Plutoniten felsischer Zusammensetzung, umschlossen von gefalteten vulkanisch und sedimentär geprägten Abfolgen. Jedoch bilden diese Gesteine kein repräsentatives Archiv der krustalen Entwicklung, sondern sind einzelne Fragmente, räumlich und zeitlich voneinander getrennt. Je älter die geologischen Formationen, desto uneindeutiger ist ihre Entstehungsgeschichte, nicht zuletzt aufgrund von zum Teil mehrfacher metamorpher Überprägung. Vor allem die Zusammensetzung der Granitoide unterscheidet sich deutlich von jüngeren, postarchaischen magmatischen Gesteinen. Am weitesten verbreitet in archaischen Plutonen ist eine Assoziation von Tonaliten, Trondhjemiten und Granodioriten (TTG). Deren gemeinsames Auftreten ist möglicherweise der Schlüssel zum Verständnis des vorherrschenden geodynamischen Systems im Archaikum und beinhaltet entscheidende Hinweise zum Einsetzten der modernen Plattentektonik. Die wahrscheinlich größten Unsicherheiten in der Entstehung von TTGs ist die Verfügbarkeit von Wasser während der Schmelzbildung und ihr Differentiationsmechanismus.

Ziel der vorliegenden Arbeit ist, die Druck- und Temperaturbedingungen sowie Menge des benötigten Wassers bei der Entstehung von TTG Schmelzen mithilfe verschiedener Herangehensweisen einzugrenzen: (i) einer experimentellen Ti-Sättigungsstudie an einem eoarchaischen Granodiorit aus dem Nuvvuagittuq Grünsteingürtel der Nordöstliche Superior Provinz in Kanada sowie der Kalibration eines Ti-Löslichkeitsmodells für Silikatschmelzen; (ii) der Betrachtung der in Liquidusnähe gesättigten Mineralphasen mithilfe von Kristallisationsexperimenten und Modellierung, sowie der Herausarbeitung möglicher kotektischer Pfade an dem selben Granodiorit und (iii) der Kalibration eines auf publizierten, wasserhaltigen Schmelzexperimenten beruhenden Hilfsvektorregressionsmodells (SVR) zur Bestimmung von Temperatur und Druckbedingungen sowie Wassergehalt der Schmelze am Liquidus, basierend auf der Hauptelementzusammensetzung. Die drei Methoden werden auf einen TTG Datensatz chemischer Analysen, zusammengetragen aus verschiedenen Publikationen, angewendet. Die Ti-gesättigten Liquidustemperaturen, berechnet für den TTG Datensatz, liegen im

Durchschnitt zwischen 750 und 900 °C und definieren ein Minimum für die Schmelzbildungstemperatur. Jedoch sind viele berechnete Ti-Temperaturen unterhalb einer aufgrund der Hauptelementzusammensetzung zu erwartenden Liquidustemperatur. Entsprechend können diese Gesteine an ihrem Liquidus nicht mit Rutil oder Ilmenit gesättigt gewesen sein, was Konsequenzen für die Interpretation der TTG-typischen Nb-Verarmung hat. Diese, generell mit der Liquidussättigung mit Rutil in Verbindung gebracht, ist vorhanden, unabhängig davon ob die jeweilige Zusammensetzung am Liquidus mit Rutil oder Ilmenit gesättigt sein kann oder nicht. Daher ist die Bedeutung von Rutil und Ilmenit für die TTG Schmelzentstehung wahrscheinlich begrenzt und die Nb-Verarmung entweder vom Ausgangsgestein ererbt oder das Resultat anderer Titan-führender Phasen wie zum Beispiel Amphibol oder Glimmer. Basierend auf dem Vergleich mit experimentellen Schmelzen müssen 8-12 Gew.% H₂O in den TTG-Schmelzen gelöst sein, damit der Liquidus innerhalb des berechneten Temperaturintervalls erreicht wird. Diese Wassermenge spricht für die Anwesenheit eines freien Fluides während der Schmelzbildung. Das SVR-Modell bestätigt die Menge des benötigten Wassers für die Ti-gesättigten Liquidustemperaturen mit einer unabhängigen Kalibration.

Für wässrige Bedingungen sprechen auch mögliche TTG-Differentiationspfade. Die Verhinderung von Plagioklaskristallisation bei Wassergehalten über 5 Gew.% führt zu einem konstanten K_2O/Na_2O -Verhältnis, typisch für die Differentiation hin zu trondhjemitischen Schmelzen. Unter wasserärmeren Bedingungen entstehen durch Anwesenheit von Plagioklas granodioritische und granitische Schmelzen, vergleichbar mit rezenten Magmen. Daher muss das archaische magmatische System wasserreich gewesen sein.

Es ist wahrscheinlich, dass TTGs nicht auf einem einzelnen kotektischen Pfad liegen sondern, eher auf mehreren von Hornblende/Klinopyroxen - Granat/Orthopyroxen kontrollierten kotektischen Pfaden, deren Position von Druck und Wassergehalt abhängig ist.

Das geodynamische System, in dem sich TTGs entwickeln, muss in der Lage sein genügend Wasser für eine K_2O arme Schmelzentwicklung zur Verfügung zu stellen. Ein Recyclingmechanismus, der subduktionsartig hydratisierte basaltische Kruste in die Schmelzentstehungsregion bringt, ist dafür ein plausibler Rahmen.

Abstract

Alexander Wellhäuser

Generating early continental crust

Archean cratons are the products of geodynamic processes governing the evolution of the early Earth. They comprise felsic granitoids enclosed by folded volcano-sedimentary successions. However, these rocks may not be representative archives but rather accidental fragments in time and space. The further back the rock record reaches in time, the more ambiguous it becomes, not least because of multiple subsequent overprinting events. The composition of Archean granitoids is distinctly different to post-Archean felsic rocks that are associated with modern continental crust forming processes. Most common is an association of tonalites trondhjemites and granodiorites (TTG). The joint occurrence of TTG potentially holds key insights about the Archean geodynamic environment, including the timing of the onset of modern-day plate tectonics, which is yet to be resolved. A major uncertainty regarding their formation is the availability of H_2O during melting of their protolith and the mechanism of their differentiation.

This research focusses on constraining P-T-H₂O conditions of TTG melt formation by combining different approaches: (i) an experimental Ti saturation study on an Eoarchean granodiorite from the Nuvvuagittuq greenstone belt, North-eastern Superior Province and subsequent calibration of a Ti solubility model for silicate melts, (ii) an experimental and modelling investigation of saturated liquidus phases and potential cotectic paths on the same rock and (iii) using published glass analyses of hydrous melting experiments to calibrate a support vector machine regression (SVR) model capable to predict temperature, pressure and H₂O conditions of a TTG sample based on the major element composition. The three methods are applied to a compilation of natural TTG analyses from published literature. Ti saturated liquidus temperatures for natural TTGs are on average between 750 and 900 °C,

constraining a minimum melt formation temperature. However, many TTGs have temperatures below expected liquidus temperatures based on their major element composition. Congruously these can not have been saturated with rutile or ilmenite at their liquidi. This has consequences for the interpretation of the Nb depletion in TTGs, as it is observed, irrespective of whether or not a composition could have been saturated in Ti. Therefore the role of Ti accessory phases in TTG formation might be limited. The Nb depletion could instead be inherited from a precursor rock or the result of other Ti-bearing phases involved in TTG formation, as for example amphibole or mica.

Based on comparison with experimental data, TTGs in equilibrium with a Ti phase at the liquidus require 8-12 wt% H_2O dissolved to be at liquidus conditions. This elevated amount favours the presence of a free fluid during melting. The SVR model independently confirms the amount of H_2O required for Ti saturated liquidus temperatures.

Hydrous conditions are also favoured when retracing the differentiation paths of TTG via crystallisation experiments and modelling. Plagioclase suppression by H_2O contents >5 wt% results in a low K_2O/Na_2O ratio throughout differentiation that is typical for melt evolution towards a trondhjemitic composition. Less hydrous conditions result in granodioritic and granitic melt compositions, as is commonly observed in post-Archean magmatic systems. Therefore the Archean environment producing TTGs must have been more hydrous than recently active magmatic systems that produce felsic crust.

It is most likely that TTGs do not align along a single cotectic path, but along several hbl/cpx - grt/opx controlled cotectics, whose position is shifted by varying pressure and/or H₂O conditions.

The geodynamic environment that gave rise to TTGs must provide an elevated amount of H_2O . This favours a model of the recycling of hydrated basalt into the region of melt formation in a subduction-like setting.

Statement of Originality

This thesis is being submitted to Macquarie University and Georg-August University Göttingen in accordance with the Cotutelle agreement dated 12.12.2016.

To the best of my knowledge and belief, the thesis contains no material previously published or written by another person except where due reference is made in the thesis itself.

A. Cellaix

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Acronyms

Notation	Description					
E-MORB	enriched mid oceanic ridge basalt					
EPT	East Pilbara Terrane					
FQM	fayalite-quartz-magnetite					
HFSE	high field strenght element					
HP	high pressure					
HREE	heavy rare earth element					
ISB	Isua Supercrustal Belt					
LILE	large ion lithophile element					
LP	low pressure					
MP	medium pressure					
NAC	North Atlantic Craton					
NBO/T	non bridging oxygen per tetrahedra					
NCC	North China Craton					
NESP	Northeastern Superior Province					
NGB	Nuvvuagittuq Greenstone Belt					
NNO	nickel-nickel oxide					
PM	primitive mantle					
REE	light rare earth element					
REE	rare earth element					
RMSE	root mean square error					
sd	standard deviation					
SVM	support vector machine					

Notation	Description
SVR	support vector machine regression
TTG	tonalite-trondhjemite-granodiorite
WM	wüstite-magnetite

List of Symbols

Notation	Description
\mathbb{R}	real numbers
α	Lagrange multiplier
ϵ	distance of hyperplane to margin
Λ	optical basicity
ω	orthogonal vector to hyperplane
ξ	soft margin for SVR

V

CHAPTER 1

Introduction

The face of the earth, as we see it today, is the result of a complex interaction between litho-, hydro- and atmosphere. The steady exchange between these chemical reservoirs gave rise to a manifold biosphere, unique in our solar system. Driving force of the exchange is a high temperature gradient toward earth's interior, resulting in magmatism and plate tectonics. The questions how, when and why these mechanisms, especially Wilson Cycle plate tectonics started operating, remain unresolved to date. What processes governed the newly accreted planet? Were they different than today's processes? How did the first continents form? A window into earth's early history is given by rock formations having outlasted time since the Archaean in cratons. These are commonly an amalgamation of magmatic plutons enclosed by greenstone belts that consist of volcanic and sedimentary sequences (Condie, 1981). However, the rock record preserved in cratons is not continuous, becoming more sparse with age and is often overprinted by younger magmatic or metamorphic events (O'Neil et al., 2012; Zhang et al., 2012; Upadhyay et al., 2014; White et al., 2017), which leads to ambiguity in understanding the geodynamic processes governing early earth and the emerge of life. It is not trivial to interpret rocks of Archean age and great care has to be taken as even the applicability of one of the most fundamental principles in geology, uniformitarianism is uncertain (Glikson, 1981; Park, 1982; Smithies et al., 2003).

1.1 Early continental felsic crust

The majority of Archaean felsic plutonic rocks are distinct from granitoids that form during the Proterozoic and Phanerozoic aeon (Moyen and Martin, 2012). Whereas post-Archaean plutonic felsic rocks are mainly of granitic composition, most Archaean plutonic rocks are tonalite-trondhjemite-granodiorites (TTGs). Monzodiorites and granites are of subordinate importance.

The classification as TTG suite was first introduced by Jahn et al. (1981) in a trace element and isotope study on plutonic rocks from the Pilbara craton, Western Australia. They distinguished the suite from other Archaean granitoid rocks by their low-K and high-Na content, as well as a highly fractionated rare earth element (REE) pattern. A recent review (Moyen and Martin, 2012) summarises general geochemical features of TTGs. First order important feature is a sodic composition with a K_2O/Na_2O -ratio below 0.6. The $(La/Yb)_N$ ratio is typically between 15-50, but can reach values up to 200. This depletion in heavy rare earth element (HREE) is commonly associated with the presence of residual garnet, either in the residue or by crystal fractionation. A high Sr/Y ratio can be attributed to garnet as well, but furthermore hints to the absence of feldspar during the magmatic history. An on average missing Eu-anomaly, in contrast to modern granitoids, is used as further evidence for plagioclase not being involved in TTG melt formation and evolution. TTGs are enriched in large ion lithophile elements (LILEs), and depleted in Nb-Ta-Ti, considered as a classical arc signature (Pearce and Parkinson, 1993). The LILE enrichment is attributed to the source, though could be the result of the involvement of a fluid phase (Hastie et al., 2016).

Major mineral phases are quartz, plagioclase and biotite, with K-feldspar and amphibole occurring in respect to the degree of differentiation of the individual rock (Moyen and Martin, 2012). Common accessory phases are allanite, pistacite, apatite, zircon, titanite, titanomagnetite and epidote.

The subdivision in tonalite, trondhjemite and granodiorite is based on the normative anorthitealbite-orthoclase triangle (O'Connor, 1965). Adjacent to the classification via feldspar composition, Moyen (2011) introduced a subdivision for TTGs related to the potential P-Tconditions of their formation, respectively their melt extraction depth based on the ratios of La_N/Yb_N and Sr/Y and the amount of Al_2O_3 at 70 wt% SiO₂. Thereby TTGs were classified as low- medium- and high pressure origin rocks. However, recent studies propose that there was no high pressure melting ≥ 1.5 GPa in the Archean, ascribing the high pressure signature to either hornblende fractionation or feldspar accumulation (Smithies et al., 2019; Laurent et al., 2020).

1.2 Possible geodynamic environments on Early Earth

A key aspect of the research on TTGs is the geodynamic implication that arises from the common occurrence of these rocks and their difference to felsic granitoids that are associated with modern continental crust production (Moyen and Martin, 2012). The open question is whether or not some type of plate tectonics was already operating during the Archean (Hawkesworth et al., 2010; Tang et al., 2016; Brown et al., 2020). It is important to state that subduction is not the same as plate tectonics. Subduction can occur locally whereas plate tectonics is a globally operating system. Therefore the presence of subduction zone features in Archean cratons do not prove the existence of plate tectonics (Cawood et al., 2018; Brown et al., 2020). It is likely that not a single geodynamic environment is responsible for the formation of continental crust (Van Kranendonk, 2010; Sizova et al., 2015) as a single scenario cannot account for the heterogeneity of Archean cratons.

The presence of subduction zone settings already in the Eoarchean has been proposed for different cratons. Turner et al. (2014) describe a geochemical stratigraphy from the Nuvvuagittuq Greenstone Belt (NGB), Canada, as closely resembling the Izu-Bonin-Mariana forearc subduction initiation sequence. However, Pearce and Reagan (2019) argue that the sequence rather represents an arc-basin boninite, though still related to subduction. A subduction related origin is also proposed for the Isua Supercrustal Belt (ISB), North Atlantic Craton (NAC) in West Greenland, being interpreted as a "proto arc" (Komiya et al., 1999; Polat and Hofmann, 2003; Jenner et al., 2009; Nutman et al., 2015). Besides a lithostratigraphic sequence that resembles arcs, Eoarchean tectonic structures are preserved, interpreted as caused by convergence. Thereby slices of oceanic crust were piled up until a sufficient depth for melting in presence of garnet was reached to produce rock of TTG composition. In addition to individual areas of the NAC showing subduction features, an accretionary origin is proposed for the whole craton by Polat et al. (2015) due to Neoarchean shear zones amalgamating individual terranes. The difference in chemical composition of TTGs to granitic rocks formed in modern arc settings is ascribed to different conditions of melting. Whereas in modern subduction zones melting occurs in the mantle wedge (McCulloch and Gamble, 1991; Grove et al., 2006) due to fluid release of the subducting slab, the melt formation of TTG is thought to happen by melting of the lower, or respectively subducting slab (Drummond and Defant, 1990; Laurie and Stevens, 2012; Nagel et al., 2012; Hastie et al., 2016), comparable to modern day adakites (Defant and Drummond, 1990; Martin et al., 2005; Castillo, 2012). The interpretation of NAC terranes having formed by subduction related processes is recently been challenged (Webb et al., 2020; Yakymchuk et al., 2020). They propose a heat-pipe model (Moore and Webb, 2013; Rozel et al., 2017) to form intrusive and supracrustal sequences with subsequent folding/shearing as a feasible mechanism to form the NAC. Webb et al. (2020) reject the previously identified metamorphic gradient (Windley and Garde, 2009) and strain variation along the proposed subduction zone within the ISB based on field evidence. They identified homogenous prograde metamorphism and strain, from which they interpret the ISB to be an a-fold and not a subduction zone.

In contrast to convergent settings there are Archean cratons that do not show features indicating horizontal movement or subduction zone like stratigraphy. The most prominent example is the East Pilbara Terrane (EPT), consisting of a Paleoarchean dome and keel structure (Collins et al., 1998; Sandiford et al., 2004; Wiemer et al., 2018). This structure is thought to have formed by consecutive mantle plumes interacting with a "proto crust" to form a thick oceanic plateau. By remelting of the volcanic plateau, granitoids were emplaced leading to partial convective overturn within the crust (Smithies et al., 2009; Hickman and Van Kranendonk, 2012). Evidence for subduction in the Pilbara is not present before 3.12 Ga (Smithies et al., 2005). A similar setting involving a volcanic plateau is proposed for the Kaapvaal craton (Van Kranendonk et al., 2015).

Numerical modelling by Sizova et al. (2015) allows different geodynamic settings to coexist. The early crustal evolution is driven by lower crust delamination, underplating of basaltic melts as well as crustal overturns resulting in the formation of a dome and keel structure. Short lived subduction events are triggered by oceanic spreading due to hot mantle upwelling. Bédard (2018) proposes a similar environment where long-lived mantle upwelling reworked oceanic crust and induced mantle currents that dragged pre-existing continents, letting them develop convergent margins. A different option to trigger subduction events is by extraterrestrial impactors, which were common in the early solar system proposed by O'Neill et al. (2017) and King (2020).

1.3 Objective of the thesis

This work combines different methods to constrain the formation conditions of Archean TTG and infer relevant geodynamic processes in their origin. Their formation conditions bear uncertainty because additionally to the lack of knowledge about the geodynamic environment, the source of TTGs is not preserved or identified within the geologic record of Archean cratons. To bypass this limitation I focus on constraining their liquidus conditions based on their major element composition. Here, the term "liquidus conditions" is solely used for felsic compositions, describing the conditions at which they are almost completely molten. At these conditions they might have formed by partial melting of a protolith.

Appropriate liquidus conditions must provide a starting-point to account for the differentiation mechanism that results in the variety of compositions occurring in TTG suites. My major focus hereby is on the amount of H_2O present during TTG melt formation, the least certain, but most crucial parameter. The focus of the thesis comprises the following topics:

- I. An experimental Ti solubility study on the Archean granodiorite PC-103 comprising the calibration of a Ti solubility model for silicate melts and calculation of Ti saturated liquidus temperatures for TTGs.
- II. Crystallisation experiments and modelling of phase stabilities on the Archean granodiorite PC-103 under various conditions to investigate possible differentiation paths.
- III. The calibration and application of an experiment-based statistical P-T-H₂O-liquiduscondition prediction model to estimate TTG liquidus conditions by comparison to hydrous melting experiments.

In the following sections I will outline constraints made by experimental, modelling and field studies on the formation conditions of TTGs and introduce the literature relevant to each topic.

1.4 Mechanisms and conditions of TTG formation

It is not certain how TTGs formed, not even if they represent true magmatic liquids. In case they do, or at least part of the series, they could be formed by partial melting or by crystal fractionation. Distinguishing between these two processes is difficult as both result in similar major- trace and isotope compositions (Brophy, 2008). As there are no mafic to felsic evolutionary trends observed in Archean cratons, it is generally assumed that TTGs

formed by partial melting (Moyen and Martin, 2012). However, several authors argue for crystal fractionation being involved in forming TTGs (Martin, 1993; Kleinhanns et al., 2003; Bédard, 2006a; Jagoutz et al., 2013; Hoffmann et al., 2014; Liou and Guo, 2019; Smithies et al., 2019; Laurent et al., 2020).

1.4.1 The source of TTGs

A major uncertainty in respect to the origin of TTGs is the lack of knowledge about their source rocks, respectively, parental magmas. They are either not preserved in the geologic record or have not yet been clearly identified. This complicates setting constraints on TTG formation conditions as their geochemical features could result from forming under specific conditions or be inherited from their source (Hoffmann et al., 2019).

Based on a variety of experimental petrological studies on potential source rocks (Beard and Lofgren, 1991; Rapp et al., 1991; Rushmer, 1991; Rapp and Watson, 1995; Sen and Dunn, 1994; Patiño Douce and Beard, 1995; Skjerlie and Patiño Douce, 1995, 2002; Winther, 1996; Springer and Seck, 1997; Xiong et al., 2005; Adam et al., 2012; Hastie et al., 2016) and TTG like compositions (Green and Ringwood, 1968; Green, 1972; Lambert and Wyllie, 1974; Allen et al., 1975; Allen and Boettcher, 1978, 1983; Johnston and Wyllie, 1988) there is common agreement that hydrated basaltic compositions likely served as a TTG precursor (Wyllie et al., 1997; Moyen and Stevens, 2006; Hoffmann et al., 2019). The hydrated basalt hypothesis is supported by recent findings of heavy $\delta^{30}Si$ values for Archean granitoids, that are interpreted as signals from silicified basaltic precursor rocks (André et al., 2019). However, boron isotopes from different cratons suggest that the source was unaffected by seawater or seawater altered rocks (Smit et al., 2019).

Trace element modelling suggests that no depletion or an enrichment of the source is required to produce the trace element pattern typical for TTGs by melting (Springer and Seck, 1997; Martin et al., 2014; Johnson et al., 2017). An enrichment by fluids during melting is another possibility (Hastie et al., 2016). The signature comprises an enrichment of LILE and a depletion in Nb and Ta, similar to a classic arc signature. It could likely have formed by recycling of older crustal material into the region of melting. This kind of composition is preserved in different Archean cratons (Thurston and Fryer, 1983; Crow and Condie, 1987; Puchtel et al., 1997; Jenner et al., 2009; Hoffmann et al., 2011b; Adam et al., 2012; Parks et al., 2014), though making up only a subordinate fraction of the preserved basaltic rocks.

1.4.2 Experimental and modelling constraints on TTG formation

The formation conditions of TTGs have been intensively studied with numerous melting experiments and modelling on basaltic potential source compositions (the "forward" approach), as well as by liquidus studies on TTGs or similar compositions (the "reverse" approach). The forward approach implies the simplification that TTGs are produced by batch partial melting and TTG compositions are primary melts. However, this might only be true for part of the

TTG suite (Laurent et al., 2020).

Moyen and Stevens (2006) summarised forward melting experiments on basaltic rocks and favoured TTG melt formation above 1.5 GPa between 900 °C and 1100 °C under fluid absent conditions. Several forward melting experiments from different studies (Rapp and Watson, 1995; Winther, 1996; Skjerlie and Patiño Douce, 2002; Adam et al., 2012; Laurie and Stevens, 2012; Hastie et al., 2016) resulted in glasses of TTG composition (or came close), based on major element requirements as summarised in Moyen and Martin (2012). Rapp and Watson (1995) produced a trondhjemite at 1000 °C, 1.6 GPa by fluid absent melting of an amphibolite with a low-K enriched mid oceanic ridge basalt (E-MORB) composition, 4.25 wt% H₂O dissolved in the melt and a restite assemblage of amphibole, plagioclase, clinopyroxene (cpx) and garnet. Winther (1996) matched a trondhjemite major element composition at 800 °C, 2.14 GPa by water saturated melting of an artificial average Archean tholeiite mixture with 15 wt% H₂O dissolved in the melt and a residual assemblage of cpx, garnet, quartz and amphibole.

Skjerlie and Patiño Douce (2002) produced tonalitic compositions in three runs by fluid absent melting of a zoisite-bearing quartz eclogite. At 950 °C, 1.5 GPa with cpx, zoisite, quartz, plagioclase, kyanite and garnet as restite and for 1025 °C and 1050 °C at 2.1 GPa with a cpx, zoisite, plagioclase, quartz, kyanite and garnet phase assemblage. 4 to 5 wt% H₂O is present in the produced melts.

Adam et al. (2012) produced a tonalitic to granodioritic melt from a boninite with a subduction zone trace element signature at 950 °C and 2 GPa with a residual mineralogy comprising cpx, garnet, orthopyroxene (opx) and chromite without the addition of water. However, the K_2O content is slightly too high to be considered as a typical Archean TTG.

Laurie and Stevens (2012) produced trondhjemitic compositions by water-saturated eclogite melting at 870–900 °C and 1.9 to 3.0 GPa. Residual mineralogy is garnet, cpx, rutile and ilmenite at pressures up to 2.2 GPa. Their starting material is peculiar by being almost K_2O free, enriched in incompatible elements and depleted in HREE compared to MORB. Hastie et al. (2016) approached tonalitic compositions by melting a primitive and depleted (light rare earth element (REE), Th and U) tholeiite from the Java plateau at 900–950 °C at various depths (1.6-2.2 GPa) and 2-3 wt% H₂O present. However, their alkali content, especially K_2O is too low, which they argue can be solved by addition of a slab fluid or using a more differentiated rock as the starting materials that were particularly low in K_2O (0.08-0.17 wt%). The TTG formation by melting of basaltic compositions was furthermore studied by phase equilibrium modelling (Nagel et al., 2012; Palin et al., 2016; Johnson et al., 2017; Hoffmann et al., 2019). Nagel et al. (2012) modelled the melting of an Eoarchean hydrated tholeiite from the ISB and matched TTG-like major and trace element compositions at 1.0 and 1.4 GPa with 15-20 % melt. This corresponds to temperatures between 836 and 928 °C.

Palin et al. (2016) modelled TTG compositions by melting hydrated, enriched Archean

tholeiite (Condie, 1981) at H₂O saturated solidus conditions at 0.6, 1.2 and 2.0 GPa pressures which translates to 1.6, 2.1 and 1.0 wt% H₂O present during melting. Their modelling results suggest conditions of formation between 800-950 °C and 1.0-1.8 GPa.

Johnson et al. (2017) modelled partial melting along different geotherms of an average basalt composition from the 3.5 Ga Coucal Formation (Smithies et al., 2009), East Pilbara Terrane (EPT). These Coucal compositions are similar to the starting materials of Adam et al. (2012) and Laurie and Stevens (2012) and already bear an enrichment in LILE and mild depletions in HREE. Johnson et al. (2017) proposed TTG production at a melt fraction between 20 to 30 % along a geotherm higher than 700 °C/GPa resulting in melting temperatures between 800 to 950 °C at pressures below 1.3 GPa. Water content of 1.4 wt% was chosen to saturate the solidus at 1 GPa. The modelling did not result in TTG major element compositions of the partial melts according to the classification of Moyen and Martin (2012) as melts contained either too much K₂O or FeO and MgO. Closest fits were obtained around 900 °C and 30 % melt fraction.

Reverse studies on TTG compositions were conducted by Wyllie et al. (1997) and Clemens et al. (2006). The study of Wyllie et al. (1997) summarises the work of earlier liquidus studies on an Archean trondhjemite from Nuuk and a Sierra Nevada tonalite, with both being studied over a broad range of temperature, pressure and H₂O conditions. Furthermore, they combined forward and reverse approaches to identify P-T conditions of matching liquidus and residual phases. In amphibolite facies (< 1.2 GPa), trondhjemites will form between 750-900 °C and 5-12 wt% H₂O present, whereas tonalites need temperatures between 850-975 °C and 9-17 wt% H₂O. For this amount of H₂O, an external influx is required. However, amphibole partitioning coefficients are insufficient to account for HREE depletion in TTGs (Bédard, 2006a; Tiepolo et al., 2007). In eclogite facies conditions (> 1.2 GPa) Wyllie et al. (1997) proposed trondhjemite formation above 900 °C and 5 wt% H₂O and tonalite at approximately 975 °C and 9 wt% H₂O. Clemens et al. (2006) investigated the stability of garnet in a Barberton trondhjemite and defined the minimum pressure for TTG melting at 1.47 GPa.

The conclusions from these studies that consider TTGs a magmatic liquid are not unambiguous. Whereas in forward melting experiments TTG compositions do not form below 1.5 GPa, the modelling suggest a pressure range of 1-1.5 GPa. This difference might be at least partially caused by the different methods used. Hirschmann et al. (1998) observed differences between experimental and modelled phase stabilities resulting in an offset in melt fraction by 100 °C. The temperature range of formation is broad for both modelling and experiments from 800-1050 °C, with trondhjemites preferably forming at lower temperatures. The position of the liquidus is strongly dependent on the amount of H₂O available (Green, 1972; Green and Ringwood, 1972; Wyllie et al., 1976; Holtz and Johannes, 1994) which makes it the crucial major uncertainty for TTG formation.

1.4.3 TTG evolution by crystal fractionation

The alternative to TTGs being primary melts is that they were formed by crystal fractionation. Models proposing this vary strongly in the extend of which fractionation is involved in TTG formation. As an "end-member" model Kleinhanns et al. (2003) propose that Barberton TTGs evolve directly from mantle wedge derived basaltic magmas under hydrous conditions by fractionating garnet/amphibole \pm pyroxenes, plagioclase or olivine depending on conditions, similar to what Macpherson et al. (2006) proposed for adakites. Other studies favour a combination of partial melting and subsequent crystal fractionation (Martin, 1993; Bédard, 2006a; Jagoutz et al., 2013). Liou and Guo (2019) investigated a Neoarchean TTG suite from the North China Craton (NCC) and identified tonalites and trondhjemites with an complementary hornblendite to match a primary liquid of dioritic composition, which was also identified in the field. They propose up to 27 % hornblende fractionation are able to provide a generic link between the individual rocks. However, even though the diorites already have low K₂O/Na₂O ratios (mean = 0.42), hornblende fractionation is not capable to produce K₂O/Na₂O ratios of 0.13, the observed minimum ratio in the trondhjemites.

Based on a Neoarchean supracrustal felsic succession that follows a differentiation sequence toward high pressure TTG signature, Smithies et al. (2019) argue that this signature is the result of hornblende dominated fractionation and that high pressure melting (≥ 40 km) did not occur in the Archean. Laurent et al. (2020) argue, that because of TTGs being granitoids they should be affected by magma chamber processes involving fractionation, accumulation, mixing and melt segregation. Thereby they explain the compositional heterogeneity of Barberton TTGs by mid- to upper crustal feldspar and hornblende accumulation. Their model does not require high pressure melting. The two studies Smithies et al. (2019) and Laurent et al. (2020) contradict the conditions proven feasible by partial melting experiments shown above and are rather in line with thermodynamic modelling.

The same way as Archean crust was not formed by one geodynamic process (Van Kranendonk, 2010), the formation of TTGs is not either by partial melting or fractional crystallisation but rather an interplay of both with varying contribution of the two processes.

1.5 The Eoarchean granodiorite PC-103

In this thesis, experiments conducted on the granodiorite PC-103 from the Nuvvuagittuq Greenstone Belt (NGB), Northeastern Superior Province (NESP), Canada (O'Neil et al., 2008, 2012; Adam et al., 2012) play an important role, wherefore I give an introduction into the geologic setting. The NGB is part of the Hudson bay terrane, which is interpreted as the oldest part of the NESP (O'Neil and Carlson, 2017). It is one of the oldest known metavolcanic-sedimentary succession on earth with a disputed earliest formation age varying between 3.8 and 4.4 Ga (O'Neil et al., 2008, 2012; Guitreau et al., 2013). The minimum age is constrained by zircon ages of trondhjemitic bands intruded into the sequence (Cates and Mojzsis, 2007) and Sm-Nd/Lu-Hf data on metavolcanic and metasedimentary rocks (David

et al., 2009; Guitreau et al., 2013). The Hadean age (O'Neil et al., 2008, 2012) is based on the short-lived ¹⁴⁶Sm-¹⁴²Nd isotope system, however disputed by Guitreau et al. (2013) and interpreted as an early Hadean mantle refertilisation. In any case some Hadean component is reworked by the formation of the NGB due to a ¹⁴²Nd deficit (O'Neil and Carlson, 2017). Rocks within the sequence are interpreted to represent mainly primitive oceanic crust that has been hydrothermally affected (O'Neil et al., 2011). The majority of sediments are chemical (e.g. banded iron formations), with very few siliciclastic layers (O'Neil et al., 2019). Most of the NGB experienced at least upper amphibolite facies metamorphic conditions in two episodes (O'Neil et al., 2012) at 2.7 and 3.6 Ga, most likely related to the intrusion of felsic granitoids that enclose and intruded the belt. A part of the chemical stratigraphy of the NGB has similarities to modern forearcs (Turner et al., 2014) with high Ti-tholeiites being overlain by boninite-like rocks and a calc-alkaline suite on top, interpreted as a subduction initiation sequence (Stern et al., 2012).

Granodiorite PC-103 is part of the TTG plutonic rocks that surround and rarely intruded the NGB. Trondhjemitic bands that intruded the NGB bear an age of 3.75 to 3.82 Ga. The tonalites and granodiorites surrounding the NGB have an age of 3.66 Ga. The last felsic magmatic episode is marked by the intrusion of granitic pegmatites of Neoarchean age (2.69 Ga, David et al., 2009). The rocks bear typical signatures of Archean TTG as described in section 1.1, with a depletion in HREE and no Eu-anomaly in most rocks (O'Neil et al., 2012). As the metavolcanic rocks, they have a deficit in ¹⁴²Nd, hinting towards a Hadean source being reworked. The early trondhjemites tend to be more depleted in HREE than the later slightly less sodic compositions.

PC-103, classified as a tonalite in Adam et al. (2012), belongs to the 3.6 Ga intrusive suite (O'Neil et al., 2012) and was affected by metamorphism, seen by a preferred orientation of ferro-magnesian minerals. The rock consists of quartz, plagioclase, K-feldspar, biotite, hornblende, epidote, titanite, apatite and zircon. Opaque phases are small and rare. It was affected by alteration, visible by sericitised feldspars and chloritised biotite. Being of classic TTG composition, PC-103 is depleted in HREE, Nb-Ta-Ti and does not have an Eu-anomaly. Due to its major element dependent position in the feldspar classification diagram of O'Connor (1965), PC-103 is a granodiorite and not a tonalite as in Adam et al. (2012). The major element composition of PC-103 is displayed in table 1.1.

Table 1.1: Major element composition of the sample PC-103 from O'Neil et al. (2012) in wt%.

SiO_2	TiO_2	Al_2O_3	FeO_t	MnO	MgO	CaO	Na_2O	K_2O	P_2O_5	LOI
66.1	0.45	15.9	3.74	0.08	2.17	3.67	3.66	2.44	0.11	1.3

1.6 Manuscript contribution

The thesis design is cumulative, wherefore several authors contributed to the chapters. Chapters 3, 4 and 5 and are self-contained manuscripts and chapter 3 has been submitted to G^3 - Geochemistry, Geophysics, Geosystems. The following table 1.2 shows the contributions of each author based on the Contributor Roles Taxonomy.

		Ŧ	
	chapter 3	chapter 4	chapter 5
Conceptualisation	AW, TR, JA, GW	AW, TR, JA	AW
Data curation	AW	AW	AW
Formal analysis	AW	AW	AW
Investigation	AW	AW, JA	AW
Methodology	AW	AW	AW
Supervision	AW	AW	AW
Visualisation	AW	AW	AW
Writing - original draft	AW	AW	AW
Writing - review & editing	AW, TR, JA, GW	AW, TR, JA	AW, GW

 Table 1.2:
 Contribution to individual manuscripts

AW = Alexander Wellhäuser, GW = Gerhard Wörner, JA = John Adam,

TR =Tracy Rushmer

CHAPTER 2

The Eu-anomaly in tonalite-trondhjemite-granodiorites (TTGs) and its relevance

2.1 Preface

To investigate the formation conditions of tonalite-trondhjemite-granodiorites (TTGs) it is important to study compositions that are likely to have been primary melts and not have been affected by crystal fractionation, accumulation or magma mixing. Within the chapters chapters 3 to 5, I use a compilation of TTG datasets from different literature sources. One filter that I apply on the compilation is that the Eu-anomaly must be smaller than ± 0.1 In this chapter I argue why it is essential to apply such a strict condition.

2.2 Introduction

The argument about the geodynamic environment of tonalite-trondhjemite-granodiorite (TTG) formation comprises the issue of a clear definition for these rocks. Moyen and Martin (2012) showed that a large amount of rocks commonly called TTG gneisses are not of this composition. They blame a lacking formal definition and present a classification scheme for Archean TTGs based on major and trace elements. However, an implementation of their classification ($SiO_2 \ge 64$, ($FeO_t + MgO + MnO + TiO_2$) ≤ 5 , $0.5 < K_2O < 2.0$, $Na_2O > 4.0$, $0.3 < K_2O/Na_2O < 0.6$, Yb < 1.5, $La_N/Yb_N > 15$, $0.9 < Eu-anomaly^1 < 1.1$, 20 < Sr/Y < 500) shrinks their own database of 1749 samples down to 18. This overreaches the goal to provide guidance for classification. La_N, Yb_N and the Eu-anomaly are chondrite normalised (Masuda et al., 1973).

Besides the very strict rules, the classification seems inconsistent in handling the Eu-anomaly. While stating Martin (1986) that TTGs lack significant Eu-anomalies, Moyen and Martin (2012) translate this as absence of an anomaly. When examining TTGs based on their classification, a positive Eu-anomaly is observable for high pressure (HP), low heavy rare earth element (HREE) and a negative anomaly for low pressure (LP), high HREE samples (fig. 2.1a), even though it is against their own rules of classification. This is apparent in the summary table for chemical composition of TTG groups in Moyen and Martin (2012), where low HREE TTGs have an average Eu-anomaly of 1.19 and high HREE TTGs an average

¹ The range is assumed based on their statement of no Eu-anomaly present.

value of 0.84. Medium pressure (MP) samples scatter around Eu-anomaly = 1. Only on average the Eu-anomaly in TTGs does not exist.

The formation of Eu-anomalies is well studied and quantified for magmatic processes. It

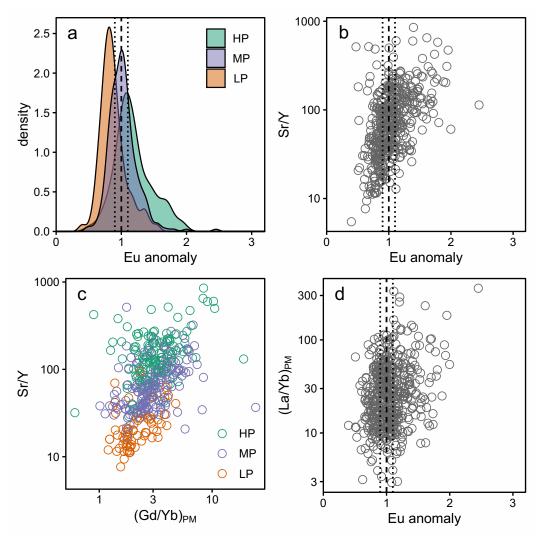


Figure 2.1: a: Eu-anomaly of TTGs categorised by their most likely formation conditions based on the classification of Moyen and Martin (2012). The dataset is from Moyen and Martin (2012). The dotted lines represent an Eu-anomaly of 1 ± 0.1 . b: Correlation between Sr/Y and the Eu-anomaly for TTGs. The Sr/Y ratio is plotted as \log_{10} . c: The two pressure indicating ratios Sr/Y and (Gd/Yb)_{PM} plotted colour coded by their pressure classification from Moyen and Martin (2012). Both ratios are plotted as $\log_{10} \mathbf{d}$: Scatter plot without a correlation between $(\text{La}/\text{Yb})_{PM}$ and the Eu-anomaly. The dotted lines represent an Eu-anomaly of 1 ± 0.1 . (La/Yb)_{PM} is plotted as \log_{10} . Theses and following diagrams were created via the R package ggplot2 (Wickham, 2016). The primitive mantle (PM) composition is from McDonough and Sun (1995).

is based on the reducibility of Eu^{3+} to Eu^{2+} by low oxygen fugacity in contrast to the rest of the rare earth element (REE) suite (Möller and Muecke, 1984). Therefore Eu behaves different during magmatic processes as rest of the REE and an so called Eu-anomaly forms. Most prominent is the negative Eu-anomaly of granites (Emmermann et al., 1975; Thorpe et al., 1977) associated with the fractionation of plagioclase, incorporating Eu^{2+} for Ca (Weill and Drake, 1973). Conversely the accumulation of plagioclase, results in a positive anomaly (Rudnick, 1992; Deering and Bachmann, 2010). Another process that generates a positive Eu-anomaly is the fractionation of hornblende (Arth and Barker, 1976; Klein et al., 1997). However, Dessimoz et al. (2012) attribute the negative Eu-anomaly in hornblende to crystallisation in presence of plagioclase. Fulmer et al. (2010) obtained hornblende partitioning coefficients from a plagioclase free natural system without an Eu-anomaly, though ascribe it to high oxygen fugacity. Based on a literature data review, Tiepolo et al. (2007) find the Eu partitioning of amphibole-melt variable, with positive Eu anomalies in potassic richterites and negative anomalies in calcic amphiboles. In the experimental study of Nandedkar et al. (2016), amphiboles bear a constant negative Eu-anomaly, however plagioclase is present in the experimental charges.

Other processes leading to the development of an Eu-anomaly are the stabilisation of Eu^{2+} by aluminosilicate complexes in highly polymerised, dry melts (Möller and Muecke, 1984) and the accumulation or fractionation of allanite (Martin, 1987), which has a strongly negative Eu-anomaly.

2.3 The Eu-anomaly in TTGs

In the context of TTGs, the Eu-anomaly is of striking importance to identify primary, unfractionated melt compositions and evaluate the applicability of the Sr/Y ratio. The Eu-anomaly correlates with the Sr/Y ratio, as observable in fig. 2.1b. Therefore the often used pressure indicator Sr/Y is most likely biased. When comparing Sr/Y to $(Gd/Yb)_{PM}$, another pressure indicator, a correlation between both of them is observable. However, it is not possible to distinguish between MP and HP rocks based on the $(Gd/Yb)_{PM}$ ratio (fig. 2.1c) as they overlap in range. Only the LP TTGs are distinguishable from MP and HP samples. It might be, as suggested by Smithies et al. (2019) and Laurent et al. (2020), that high pressure melting did not or only sparsely contribute to the formation of TTGs.

There are several possibilities that can produce a positive EU-anomaly. As TTGs are thought to form by melting of hydrous basaltic compositions (Moyen and Stevens, 2006; see also chapter 3 and 5), partitioning by an highly polymerised and dry melt (Möller and Muecke, 1984) can be ruled out. The fractionation of allanite is a feasible process, however this would also produce a flattening of the whole REE pattern correlating with an increasing Eu-anomaly, which is not observed (fig. 2.1d). There is no correlation between the slope of REE and the amplitude of the Eu-anomaly.

The two other possibilities to create a positive Eu-anomaly are (i) by hornblende fractionation, as hornblende carries a negative Eu-anomaly in most cases (Arth and Barker, 1976; Klein et al., 1997; Liou and Guo, 2019), and (ii) accumulation of plagioclase bearing a positive anomaly, (Rudnick, 1992; Deering and Bachmann, 2010; Laurent et al., 2020).

2.3.1 Alteration of petrogenetic markers by Eu-anomaly generating processes

By modelling crystal fractionation it is possible to quantify the impact of feldspar accumulation and hornblende fractionation on trace and major elements in relation to the amplitude of the Eu-anomaly. My focus hereby is on changes in Sr/Y. To quantify the influence of plagioclase accumulation on the Eu-anomaly, I use an average Eu-anomaly free TTG (table 2.1, Euanomaly = 1 ± 0.1) as starting composition, calculated from the dataset of Moyen and Martin (2012). The composition of the cumulate is calculated by crystal fractionation from a Eu-free melt into the same composition by adding the calculated residue to the average Eu-anomaly free TTG. For this I use an adjusted version of the fractional crystallisation equation:

$$C_{cum} = C_0 (2 - F^{D-1}) \tag{2.1}$$

with C_{cum} being the element concentration in the cumulate, C_0 the concentration of the starting composition, F the melt fraction and D the partitioning coefficient. Feldspar partitioning coefficients are calculated via the equations from Bédard (2006b):

$$RTln(D_{Sr}^{plag/liq}) = -10 + 0.38 * \text{SiO}_2 - 3.5 * An$$

$$RTln(D_Y^{plag/liq}) = -118 + 1.3 * \text{SiO}_2 - 2 * An$$

$$RTln(D_{Sm}^{plag/liq}) = -82 + 0.9 * \text{SiO}_2 - 6 * An$$

$$RTln(D_{Eu}^{plag/liq}) = 88 - 3.0 * log(fO_2) - 2 * \text{SiO}_2 - 2.9 * \text{MgO}$$

$$RTln(D_{Gd}^{plag/liq}) = -80 + 0.9 * \text{SiO}_2 - 20 * An$$

$$(2.2)$$

R is the gas constant, T the temperature in Kelvin, SiO₂ and MgO are in wt% melt concentration and An is the normative molar anorthite component of plagioclase calculated via CIPW norm in *GCDkit* (Janoušek et al., 2006). As all equations contain the same temperature factor and the results of interest are ratios, the actual temperature for partitioning can be neglected and is chosen to be 850 °C. I calculated partitioning coefficients for varying $\log_{10} fO_2$ from -7 to -17, resulting in $D_{Eu}^{plag/liq}$ between 0.03 and 0.93. The partitioning coefficient being below 1 even under reduced conditions is caused by the differentiated composition used for modelling (table 2.1). At lower silica content $D_{Eu}^{plag/liq}$ can be easily above 2 (Bédard, 2006a). Archean magmatic processes are thought to have been more reduced than today's. (Foley, 2011), with Archean cratonic lithosphere having a mean $\log fO_2$ of -2.83 Δ fayalite-quartzmagnetite (FQM), two log units below the average of post-Archean continental lithosphere. Considering this, $\log fO_2 = -17$ is a reasonable estimate at 850 °C.

Results of the accumulation calculation are displayed in fig. 2.2a. At the maximum D_{Eu} calculated with the compositional terms (table 2.1) and $\log fO_2 = -17$, up to 30 % of feldspar addition are required to produce the observed Eu-anomaly in natural TTGs. A small amount

of accumulation (<10 %) results in an Eu-anomaly of 1.1 while almost doubling the Sr/Y ratio from 66 to 127. The formation of a negative Eu-anomaly by plagioclase accumulation under high $\log fO_2 = -7$ is an artefact of the model. At high $\log fO_2$ Eu behaves as the rest of the REE and no anomaly should develop. At $\log fO_2 = -10$ no Eu-anomaly forms, which seems to be the limit of the model.

A similar calculation can be done for hornblende, based on the partitioning regressions of

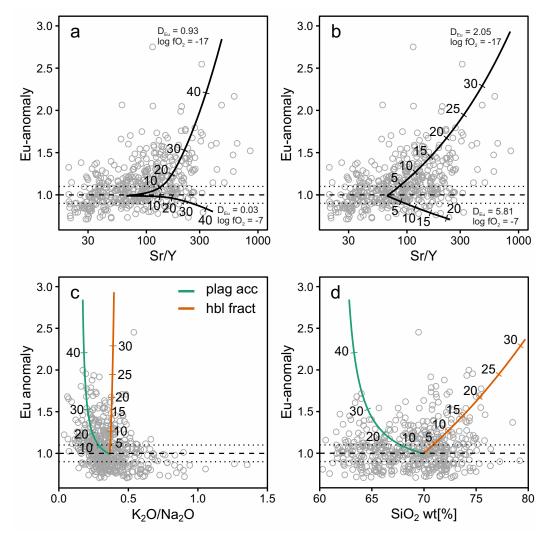


Figure 2.2: Modelling results for trace and major element evolution by fractional crystallisation of hornblende and accumulation of feldspar starting from an average Eu-anomaly free TTG composition (table 2.1). Values along evolution lines represent the amount of fractionation/accumulation in %. Natural TTG compositions from from Moyen and Martin (2012) are plotted as open circles. **a**: Change in Eu-anomaly and Sr/Y ratio by feldspar accumulation calculated via partitioning coefficients from Bédard (2006b). The Sr/Y ratio is plotted as \log_{10} . **b**: Change in Eu-anomaly and Sr/Y ratio by hornblende fractionation calculated via partitioning coefficients from Nandedkar et al. (2016). The Sr/Y ratio is plotted as \log_{10} . **c**: Change in Eu-anomaly and K₂O/Na₂O by plagioclase accumulation and hornblende fractionation. Both are modelled for $\log fO_2 = -17$. **d**: Change in Eu-anomaly and SiO₂ by plagioclase accumulation and hornblende fractionation. Both are modelled for $\log fO_2 = -17$.

Table 2.1: Average Eu-anomaly free (1 ± 0.1) TTG element concentrations based on the database of Moyen and Martin (2012) and the temperature used for calculating partition coefficients. Oxides are in given in wt% and trace elements in ppm. An is the molar anorthite content calculated by CIPW norm via the *R* package *GCDkit* (Janoušek et al., 2006).

SiO_2	MgO	Sr	Y	Sm	Eu	Gd	An	T [$^{\circ}$ C]
68.9	1.18	522	7.87	3.30	0.89	2.33	0.27	850

Nandedkar et al. (2016). Their trace element partitioning depends on the partitioning of Ca between amphibole and melt as proposed by Sisson (1994) and displayed in following equations:

$$ln(D_{Sr}^{hbl/liq}) = 0.25 * ln(D_{Ca}^{hbl/liq} - 1)$$

$$ln(D_{Y}^{hbl/liq}) = 1.8 * ln(D_{Ca}^{hbl/liq} - 0.2)$$

$$ln(D_{Sm}^{hbl/liq}) = 1.6 * ln(D_{Ca}^{hbl/liq} - 0.5)$$

$$ln(D_{Gd}^{hbl/liq}) = 1.5 * ln(D_{Ca}^{hbl/liq} \pm 0)$$
(2.3)

As I only investigate ratios, the actual value of $D_{Ca}^{hbl/liq}$ is negligible. However, as Nandedkar et al. (2016) determined the partitioning coefficients of Eu²⁺ and Eu³⁺ by Young's modulus of the M4 site for each experiment individually and not by regression, I choose $D_{Ca}^{hbl/liq} =$ 3.02 from their experiment RN13V2. In this experiment $D_{Eu^{2+}}^{hbl/liq}$ is 0.50 and $D_{Eu^{3+}}^{hbl/liq}$ 5.85. Selecting both, Ca and Eu partitioning coefficients from one experiment ensures consistency between the partitioning of Eu and the other trace elements. By varying the proportion of Eu oxidation state I calculate trace element behaviour during hornblende fractionation the same way as for plagioclase accumulation (fig. 2.2). In experiment RN13V2 Nandedkar et al. (2016) calculate 35 % Eu^{2+} and 65 % Eu^{3+} while being above the nickel-nickel oxide (NNO) buffer at 860 °C. To translate the $Eu^{2+}-Eu^{3+}$ proportion into oxygen fugacity for comparability to the feldspar modelling, I use the empirical equation of Burnham et al. (2015):

$$\frac{Eu^{3+}}{\sum Eu} = \frac{1}{1 + 10^{(-0.25*\log fO_2 - 6410/T - 14.2A + 10.1)}}$$

T is the temperature in Kelvin and Λ is the optical basicity calculated from Lebouteiller and Courtine (1998). Applied to the glass composition of the experiment RN13V2 the model of Burnham et al. (2015) confirms oxygen fugacity being above NNO.

The change in oxygen fugacity for modelling purpose does not affect the other trace elements of interest. The calibrations of Nandedkar et al. (2016) (eq. (2.3)) are solely dependent on Ca partitioning, which is not influenced by fugacity (Spear, 1981; Dalpé and Baker, 2000). Fractionation paths are calculated for $\log fO_2 = -17$ and -7. At $\log fO_2 = -7$, Eu³⁺ makes up 99 % of the total Eu. With a $\log fO_2 = -17$, Eu³⁺ makes up 29 %. Results of the fractional crystallisation of hornblende are displayed in fig. 2.2b. As for plagioclase accumulation, a positive Eu-anomaly is present at $\log fO_2 \leq -10$. At reasonable conditions of $\log fO_2 = -17$ (Foley, 2011), the majority of Eu-anomalies can be produced within 15 % of hornblende fractionation, of course depending on fugacity. The effect on Sr/Y is smaller than observed by plagioclase accumulation, due to a smaller difference between $D_{Sr}^{hbl/liq}$ and $D_Y^{hbl/liq}$.

The magmatic process that leads to the development of an Eu-anomaly can be determined by the major element composition. The K_2O/Na_2O ratio and SiO₂ concentration allow to distinguish between the two processes. As the K_2O/Na_2O ratio of plagioclase is very low, accumulation will result a decrease of the ratio (fig. 2.2c). Hornblende slightly prefers Na₂O over K_2O which produces an increasing ratio along fractionation. However, this effect would be small unless large amounts of hornblende fractionate. The process results are diametrical to each other. The same is true for SiO₂ (fig. 2.2d), as it decreases by feldspar accumulation and increases by hornblende fractionation.

It is difficult and not the scope here to determine the governing process behind the Eu-anomaly for the literature compilation. Depending on the chosen starting composition of the model, either hornblende fractionation or feldspar accumulation can be possible. The magmatic evolution of a sample needs to be interpreted in context of its surrounding cogenetic rocks as done by Liou and Guo (2019).

The point at which a deviation in Eu^{*}/Eu is an Eu-anomaly is not tightly constrained. To quantify this, the approach of O'Neill (2016) who describes the REE pattern by orthogonal polynomials can be used. The polynomials return an idealised REE slope with the real samples scattering around it. Only samples with 7 or more REE analysed should be considered for the calculation. The deviation of individual element analyses from the calculated slope is analytical noise and if Eu deviates significantly from that, an Eu-anomaly is present. I consider the Eu-anomaly not an analytical noise if the standard deviation (sd) is greater than 4 σ of the scatter of the analyses, Eu and Ce excluded. 2 σ are considered as analytical uncertainty of Eu and 2 σ for the other REE. With an average 1 σ of 0.07 for the TTG dataset from Moyen and Martin (2012) it can be assumed that the range of Eu-anomaly = 1 \pm 0.1 may be partly or completely caused by analytical uncertainty only and not by a magmatic process.

2.4 Conclusions

Considering the Eu-anomaly is of great importance for investigating the magmatic history of TTGs. Already small anomalies of ± 0.1 can indicate big changes in Sr/Y, disqualifying this ratio as a petrogenetic marker. Furthermore the increase of K₂O/Na₂O by plagioclase accumulation shifts the major element composition towards a more trondhjemitic characteristic. Based on major element trends accompanying the Eu-anomaly in local cogenetic rock suites, it is possible to determine the process responsible for creating a positive Eu-anomaly. The natural TTG dataset shows that TTGs have not only been formed by partial melting but that processes as crystal fractionation and accumulation were involved as well. For the investigation of primary tonalitic and trondhjemitic magmas, it is necessary to remove samples bearing an Eu-anomaly from the data. Samples with an Eu-anomaly smaller ± 0.1 can be safely regarded as non affected by Eu-anomaly producing magmatic processes. The deviation is more likely to be of analytical origin.

CHAPTER 3

A new titanium solubility model for silicate melts with implications for conditions of Archaean crust formation

3.1 Preface

This manuscript was submitted to G^3 - Geochemistry, Geophysics, Geosystems on the 14^{th} of January 2020. Co-authors are Tracy Rushmer, John Adam and Gerhard Wörner. The idea for studying Ti solubility of TTGs was brought up by John Adam in a discussion about where the liquidi of these rocks are. This study is designed to provide reasonable liquidus temperatures for further investigation of phases saturating the liquidus. I conducted the Ti solubility experiments with the help of John Adam. Data analysis, literature review and the calibration of the model were done by myself. All authors were involved in the interpretation of the data. The first draft of the manuscript was written by myself and significantly improved in respect to content, structure and style by Tracy Rushmer, John Adam and Gerhard Wörner.

Key points

- TTGs can form in presence of a Ti rich accessory phase between 750 and 900 $^\circ\mathrm{C}$
- The temperature range requires 8-12 wt% H_2O dissolved, thus the presence of an aqueous fluid.
- Ti-temperatures for many TTGs are lower than expected liquidus temperatures; they can not have formed at these conditions.

3.2 Abstract

We calibrated a new Ti solubility model for silicate melts that are saturated in either rutile and/or ilmenite by a regression on published data for 389 experiments. This calibration has been validated using new Ti-solubility data for an Archean tonalite. We find that temperature, melt polymerisation (expressed as non bridging oxygen per tetrahedra (NBO/T)) and the ratio of singly to doubly charged cations ((Na+K)/(Fe+Mg+Ca)) are the most significant parameters controlling Ti solubility. Additional parameters, such as pressure, H₂O and oxygen fugacity, are insignificant for the solubility of Ti in natural igneous systems.

We apply the Ti-saturation thermometer to tonalite-trondhjemite-granodiorite (TTG) compositions, which are the characteristic granitoids of Archean cratons, to better constrain their conditions of formation. By comparing the temperatures required for Ti saturation with expected whole-rock liquidus temperatures we can distinguish between TTG melts that were either saturated or under-saturated in Ti. More evolved compositions are more likely to have been saturated in Ti with calculated saturation temperatures of 750-900 °C. Corresponding liquidus relations for the bulk rocks require dissolved H_2O of 8 to 12 wt%. Such concentrations may reflect the presence of aqueous fluid during the melting of basaltic source rocks. Both, Ti-saturated and under-saturated TTGs carry Nb depletions. Consequently, fractionation involving rutile and/or ilmenite cannot be the sole reason for Nb depletions in TTGs. These must have been either inherited from source rocks and/or parent magmas, caused by other crystal phases (e.g. amphibole or sphene), or be the result of mixing between Ti-saturated and under-saturated melts.

Plain Language Summary

The formation mechanisms of the first continents on Earth are uncertain because their composition is different to modern continents. It is unknown if modern plate tectonics were operating at that time or when they started. To better understand the formation conditions of early continents we calibrated a thermometer based on the solubility of titanium into melt to constrain temperatures of melt generation. This method works because rocks from early continents are depleted in Nb, Ta and Ti. This is commonly associated with the presence of a titanium rich accessory phase (e.g. ilmenite or rutile) during melt formation, buffering the Ti concentration in the melt and retaining Nb and Ta.

Applied to rocks from early continental crust we calculate melt formation temperatures of 750-900 °C. From these temperatures we can infer the amount of water present during melting because water significantly influences the temperature of melting. Estimated water is between 8 and 12 wt% which requires the presence of free water during melting, because dehydration melting cannot produce such elevated water concentration. This leads to the requirement of a process that provides enough water to the melt formation region which is easiest by recycling of water-rich oceanic crust into the mantle.

3.3 Introduction

Archaean cratons are a significant fraction of the modern continental crust and generally consist of greenstone belts and enclosed granitoids. The latter are mostly rocks of the tonalite-trondhjemite-granodiorite (TTG) series that differ significantly from the rocks usually associated with post-Archaean continent formation (Martin, 1986). These differences have prompted questions about the continuity of crust-forming processes over time, including the timing of the onset of modern plate tectonics (Martin et al., 2005; Smithies et al., 2009; Moyen and Martin, 2012; Turner et al., 2014; Hastie et al., 2016; Tang et al., 2016; Greber et al., 2017; Bédard, 2018; Moyen and Laurent, 2018; Wiemer et al., 2018). Within this context, a range of contrasting mechanisms and geodynamic settings have been proposed for the origin of TTGs. These include: (i) the melting of steeply-subducted basaltic crust directly analogous to what has been proposed for modern adakites (Martin et al., 2005); (ii) shallow subduction and underplating as described for the Isua province (Polat et al., 2015; Nutman et al., 2015) with the melting of stacked slabs of oceanic crust (Nagel et al., 2012; Hastie et al., 2016); and (iii) construction of thick oceanic plateaus, or "proto-crust" (Johnson et al., 2017), with basal melt generation at high pressures (Smithies et al., 2009) and subsequent crustal overturns (Collins et al., 1998; Bédard, 2006a, 2018; Wiemer et al., 2018). These alternative proposals do not necessarily preclude one another as observations from different cratons are not accounted for by any single model of TTG formation (Van Kranendonk, 2010).

There is common agreement that hydrated basalts are likely source rocks for TTG magmas (Smithies, 2000; Condie, 2005; Moyen and Martin, 2012) and that variations in HREE concentrations are reflective of different depths of source rock melting (Moyen, 2011). The hydrated basalt hypothesis is supported by numerous experimental studies (see Moyen and Stevens (2006) and Hoffmann et al. (2019) for compilation). However, just how hydrous TTG magmas actually were isn't known. Thus the validity of generally accepted models of TTG formation are difficult to rigorously assess. To address this problem, we have developed a temperature-dependent solubility model for TiO₂ in silicate melts and used this to first constrain the liquidus temperatures of TTG magmas, and then (indirectly) their H₂O concentrations as well. On this basis, we show that TTG magmas are likely to have been strongly hydrous (with up to 8-12 wt% of H₂O) necessitating a fluid-saturated source.

3.4 Ti-thermometry on TTGs - a key to their origin

The behaviour of titanium in TTGs holds a potential clue to their conditions of origin due to the consistent negative correlation between TiO_2 and SiO_2 (fig. 3.1) that suggests a temperature-dependent solubility control. If it can be shown that a Ti-rich mineral (rutile, ilmenite) was a liquidus phase during TTG crystallisation, the minimum temperatures of their formation can be constrained and the potential role of rutile or ilmenite in controlling the Nb depletion in TTGs can be assessed. We use the term "Ti-rich mineral" for Ti bearing minerals that buffer Ti-activity at 1.0 in an equilibrium silicate melt and thus would only form in Ti-saturated melts. Even though the Ti-activity of ilmenite is below 1.0, we do not see a statistically significant difference for saturation between ilmenite and rutile, as described later.

TTGs characteristically show relative depletions of Nb-Ta-Ti on mantle-normalised plots (Moyen and Martin, 2012). However, the role of rutile as a saturating oxide during TTG formation has been strongly debated due to the highly variable but commonly subchondritic Nb/Ta ratios (5-60) of TTGs. Low ratios can be produced by amphibolite fractionation (Foley et al., 2002; Hoffmann et al., 2011a) whereas higher ratios should result from the presence of rutile (Xiong et al., 2011; Hoffmann et al., 2011a). Furthermore, mica also has the potential

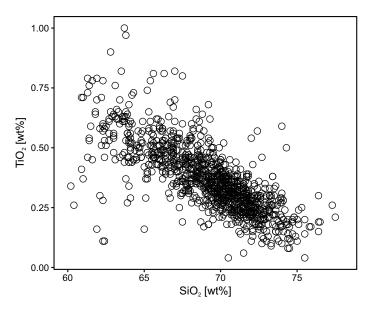


Figure 3.1: TiO_2 vs SiO_2 for TTGs. Data from Nutman et al. (1999), Moyen (2011), Huang et al. (2013), Laurent et al. (2014), O'Neil and Carlson (2017) and Johnson et al. (2019). After merging the data, duplicates are identified by the normalised major element composition and removed. This and all following images were made with *ggplot2* (Wickham, 2016).

to fractionate Nb/Ta towards low ratios (Stepanov and Hermann, 2013). Variability of the Nb/Ta ratio might also be inherited from fluid alteration prior to melting (Rapp et al., 2003). However, these objections can be set against the need for some kind of Ti-rich phase to control TiO₂ variations during the differentiation of TTGs. The most effective phases are rutile and/or ilmenite whose solubility in silicate melts is sensitive to temperature, SiO₂ content and other compositional variables, but not to magmatic H₂O (Hellman and Green, 1979; Green and Pearson, 1986). Thus there is the potential for using Ti-solubility to constrain the liquidus temperatures of TTG magmas which can then be used to estimate magmatic H₂O concentrations via the concentration-dependent liquidus point depressions caused by dissolved H₂O in silicate melts.

3.4.1 Previous experimental studies of titanium solubility in silicate melts

The first experimental study of Ti solubility in silicate melts was conducted by Hellman and Green (1979) who recognised the regular occurrence of Ti-rich accessory phases (rutile, ilmenite and titanite) in natural rocks as well as experimental charges. They identified rutile as a dominantly high pressure phase with titanite predominating at intermediate pressures (< 1.5 GPa). Green and Pearson (1986) conducted an extensive solubility study for rutile and ilmenite using a range of mafic to felsic starting compositions at temperatures of 900–1100 °C and pressures from 0.75 to 3.0 GPa, with 2, 5 and 10 wt% of dissolved H₂O. Their experiments revealed that TiO₂ solubility correlates positively with temperature and negatively with SiO₂ but is relatively unaffected by H₂O in melts. Ryerson and Watson (1987) conducted a similar study of rutile solubility in mafic to felsic melts at 1000-1350 °C and 0.6-3.0 GPa and found similar dependencies on temperature and melt composition. However, they also found a negative pressure dependence as well as a positive effect of excess alkalis relative to alumina (i.e. there is an increased solubility of Ti for peralkaline compositions).

Green and Adam (2002) determined a negative correlation between Ti-solubility and pressure as well as a slightly decreased solubility with increasing K₂O concentration in melts. Hayden and Watson (2007) presented a solubility model for a lower temperature range (650-1000 °C) at 1 GPa with evolved compositions. The model was based on a combination of temperature dependence and melt composition effects. Gaetani et al. (2008) published a Ti solubility model for a pressure range from 0.0001 to 3.5 GPa and temperatures from 1150 to 1450 °C for a similar compositional range. Xiong et al. (2009) calibrated a rutile solubility model specifically for TTG compositions at 1.5–3.5 GPa, 750–1250 °C, and dissolved melt H₂O concentrations of 8-14 wt%. Their solubility model is dependent on rutile composition, temperature, pressure, melt composition and dissolved water concentration.

In conjunction, the described studies show that the primary controls on Ti-solubility in silicate melts are temperature and melt composition. In particular, the effect of melt polymerisation is important together with alkali to alumina relations that exert a strong secondary effect on melt polymerisation. Pressure and H_2O dissolved in melts have subordinate influences on Ti-solubility.

3.4.2 Assessment of previously published Ti-solubility models

We assessed published Ti-solubility models using the results from 465 experiments in which the melt phase was saturated in a Ti-rich accessory mineral (ilmenite, rutile and/or sphene). The data used for this assessment are from Green and Pearson (1986), Ryerson and Watson (1987), Conrad et al. (1988), Beard and Lofgren (1991), Patiño Douce and Johnston (1991), Rapp et al. (1991), Skjerlie and Johnston (1992), Skjerlie and Johnston (1993), Skjerlie and Johnston (1996), Sen and Dunn (1994), Gardien et al. (1995), Patiño Douce and Beard (1995, 1996), Rapp and Watson (1995), Skjerlie and Patiño Douce (1995), Springer and Seck (1997), Pickering and Johnston (1998), Castro et al. (1999), Green and Adam (2002), Pertermann and Hirschmann (2003), Klemme et al. (2002), Yearron (2003), Spicer et al. (2004), Patiño Douce (2005), Sisson et al. (2005), Xiong et al. (2005), Xiong et al. (2009, 2011), Hayden and Watson (2007), Gaetani et al. (2008), Spandler et al. (2008), Alonso-Perez et al. (2009), García-Arias et al. (2012), Laurie and Stevens (2012), and Qian and Hermann (2013). A list of the experimental conditions and results for individual studies is given in table 3.5. In the next section we apply published thermometers to our experimental dataset and compare recorded experimental temperatures with calculated values.

The first model we examine is that of Ryerson and Watson (1987) (fig. 3.2a). It describes the solubility of rutile in silicate melts as a function of temperature, pressure, and melt composition with the latter described by the parameter FM (eq. (3.1)). All iron is assumed to be ferrous. The calibration range is from 1000 to 1300 °C and pressures of 0.8 to 3.0 GPa. A total of 66 six experiments from the experimental dataset are both within the calibration range and saturated with rutile (fig. 3.2a). For these experiments there is an average temperature deviation of -82 ±138 °C (1 σ uncertainty). Temperatures outside of the calibration range are also underestimated. An exception are temperatures around 700 °C which are calculated correctly.

$$FM = \frac{Na + K + 2(Ca + Fe + Mg)}{Al * Si}$$

$$(3.1)$$

The solubility model of Hayden and Watson (2007) (fig. 3.2b) also describes solubility as a function of temperature and the melt parameter FM (eq. (3.1)) but at a constant pressure of 1 GPa. It is calibrated for a temperature range between 650 and 1000 °C and FM between approximately 0.75 and 2.0. Temperatures for 12 experiments within calibration range are estimated by -124 ± 45 °C, with the deviation increasing with temperature. Temperatures calculated for experiments outside of the calibration range also increase in underestimation with increasing temperature. A possible reason for the persistent underestimation of temperature is that most of the experiments used to calibrate the Hayden and Watson (2007) thermometer were saturated only with rutile. Because of this, FM values for the melts are not codependent on temperature and pressure as they would be in the presence of silicate minerals and thus the relative effects of melt structure and temperature on Ti solubility are insufficiently described without additional information.

Xiong et al. (2009) (fig. 3.2c) described Ti-solubility as a function of temperature, pressure, melt composition as FM (eq. (3.1)), $\ln(\text{TiO}_2)$ for rutile, and wt% H₂O dissolved. The calibration is for temperatures of 750-1250 °C, pressures of 1.5-3.5 GPa, and FM between 1.35 and 2.47. 57 experiments are within the range of calibration and are overestimated by an average of 19 °C. Only Xiong et al. (2009) provide data for TiO₂ concentrations in rutile and on this basis we set the TiO₂ content of rutile at 90 wt%. This produces good results even for experiments where rutile is not present but instead ilmenite is the saturating phase. Experiments outside of the calibration range are underestimated by an average of -16 °C. Xiong et al. (2009) do not report uncertainties based on their regression but give an estimated error of 10-15 %.

In summary, the model of Ryerson and Watson (1987) is not reliable for temperatures $< 1000 \,^{\circ}$ C due to the systematic underestimation of temperatures. The model of Hayden and Watson (2007) also has limited utility as its calibration is limited to 1 GPa and even within the range of its calibration temperatures are systematically underestimated. The model of Xiong et al. (2009) returns good results even outside of its calibration range, however, its application requires prior knowledge about pressure, temperature and/or melt H₂O concentrations.

Ti-solubility can be adequately described by less parameters because the melt composition

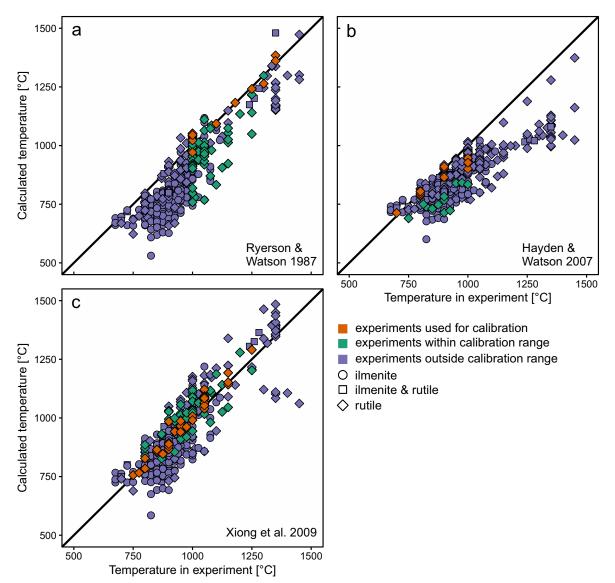


Figure 3.2: Published Ti-solubility models of a: Ryerson and Watson (1987), b: Hayden and Watson (2007) and c: Xiong et al. (2009) applied to the Ti excess phase saturated experiments (table 3.5). Calculated temperatures are plotted against recorded experimental temperatures.

depends on the unconstrained parameters. It changes with pressure, temperature and H_2O . By performing regression analysis on Ti as \log_{10} in mol% (table 3.1) we see that the model does not significantly improve by adding H_2O and pressure into the regression as displayed by r^2 . Using the two parameters improves the models r^2 by 0.02 and decreases the residual standard error by 0.01 Therefore, pressure and H_2O parameters are not necessary to describe Ti-solubility. However, by neglecting them, uncertainty is introduced because for a given melt composition a decreased solubility could be result of either higher pressure, less H_2O or lower temperature. This uncertainty remains well within error of the method. Due to the identified deficiencies of published Ti-solubility models, we calibrate a new model based on

	Intercept	T [°C]	\mathbf{FM}	P [GPa]	$H_2O [wt\%]$	RSE	r^2
Estimate	-3.33	0.0027	0.126	-0.06	0.02	0.20	0.81
Std. error	0.09	0.0001	0.009	0.01	0.003		
t value	-37.27	26.9	14.5	-4.63	7.91		
$\Pr(> t)$	< 2e-16	< 2e-16	< 2e-16	4.64e-06	1.38e-14		
Estimate	-2.87	0.00223	0.141	-	-	0.21	0.79
Std. error	0.07	0.00008	0.009	-	-		
t value	-40.3	27.53	15.89	-	-		
$\Pr(> t)$	< 2e-16	< 2e-16	< 2e-16	-	-		

the experimental dataset.

Table 3.1: Statistical evaluation of parameters controlling Ti solubility: temperature, FM, pressure and H_2O . Ti is described as log_{10} in mol%. RSE is the residual standard error.

3.5 Calibration of a new Ti-saturation thermometer by regression of previously-published experimental data

Before calibrating our model we filtered the database of previously-published experiments based on three criteria. These were that: (1) experiments are saturated in either rutile and/or ilmenite, (2) experimental glasses contain > 0.10 wt% TiO₂, and (3) experiments are saturated in one or more silicate minerals. This reduces the original total of experiments from 465 to 389. In spite of this, the filtered dataset covers a wide range of physical conditions and melt compositions with temperatures of 675-1350 °C, pressures of 0.0001-5.0 GPa (fig. 3.3a), melt H_2O concentrations from 0-20.8 wt%, and melt SiO_2 concentrations from 43.0-82.0 wt%. Further processing of the data is necessary owing to the over-representation of experiments at temperatures between 850 and 1000 °C (see fig. 3.3a, density distributions). This complicates the regression of the entire range of conditions, since sparsely sampled regions are underweighted. In order to remove the effects of the sampling bias without discarding individual experiments, we used the $group_by()$ function of the dplyr package (Wickham et al., 2018) in R (R Core Team, 2017). Group_by() reads a dataset and bins it according to one or multiple parameters, in our case \log_{10} of the mol% Ti. Using a cut option we decided the number of bin based on the \log_{10} of Ti mol% which was cut into 200 equi-spaced bins. This resulted in 116 data points with 84 bins remaining empty. Average values for all dataset parameters were then calculated for each bin. This procedure attenuates the scatter in oversampled areas and accentuates less well determined areas in the modified dataset. The value 200 was chosen after testing different cut values to create the best working model.

After initial tests, we found that temperature, non-bridging oxygens per tetrahedra (NBO/T, eq. (3.3), Virgo et al., 1980), and the ratio of single to doubly charged cations ((Na+K)/(Fe+Mg+Ca)) are the most significant factors controlling the solubility of Ti in silicate melts (fig. 3.4a & b). We tested several other parameters as for example the alumina saturation index but discarded them due to low statistical significance for Ti-solubility. All iron is

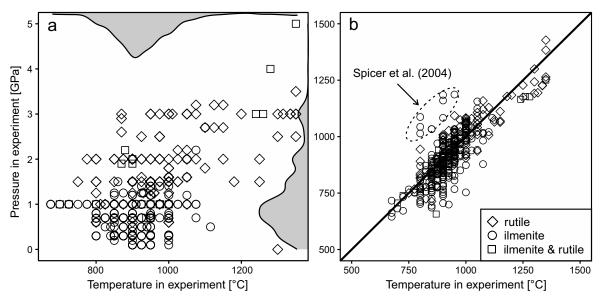


Figure 3.3: a: P-T plot of the filtered literature dataset comprising 389 rutile and/or ilmenite saturated experiments. Grey areas on the secondary axes display the density distribution of experiments regarding pressure and temperature settings without a scale. b: The model calibrated on the modified dataset (table 3.1) applied to the filtered dataset shown in fig. 3.3a. Outlying data from Spicer et al. (2004) are melts produced in pelite melting with very high K_2O content.

assumed as ferrous for both parameters. While ferrous/ferric ratios are available in the experimental dataset, they would have to be assumed for natural data, wherefore we decided to simplify the model. Ti solubility correlates positively with both temperature and NBO/T (fig. 3.4a) but negatively with the ratio of uni to divalent cations (fig. 3.4b). In general, the less polymerised the melt the greater the Ti solubility. There is no or only a weak correlation between the ratio of uni to divalent cations and the other two parameters (temperature and NBO/T). With these factors in mind, we chose a regression based on temperature, NBO/T and the uni to divalent cation ratio. This predicts Ti solubility more accurately (with r² of 0.84, table 3.2) than regressions including the effects of pressure and melt H₂O, with r² of 0.81, (table 3.1). It also results in a good fit over the whole range of temperatures (Figure 3b). Besides an expected scatter around the target temperature there is a significantly overestimated group of samples. These are from the study of Spicer et al. (2004) and are characterised by elevated K₂O generated by pelite melting.

The final calibration on the modified dataset is displayed in Table 3.2 and Equation 3.4. The 1 σ deviation is around 11 %.

	Intercept	$T [^{\circ}C]$	NBO/T	Cation ratio	RSE	r^2
unmodified dataset						
Estimate	-2.42	0.00212	1.2	-0.053	0.16	0.84
Std. error	0.09	0.00009	0.1	0.005		
t value	-28.5	22	10.5	-10.18		
$\Pr(> t)$	< 2e-16	< 2e-16	< 2e-16	< 2e-16		
modified dataset						
Estimate	-2.63	0.00248	0.8	-0.097	0.11	0.92
Std. error	0.08	0.00009	0.1	0.007		
t value	-31.7	28.4	7.57	-14.5		
$\Pr(> t)$	< 2e-16	< 2e-16	2.75E-13	< 2e-16		

Table 3.2: Regression analysis for Ti solubility on the original and the modified dataset. Ti is described as \log_{10} in mol%. RSE is the residual standard error.

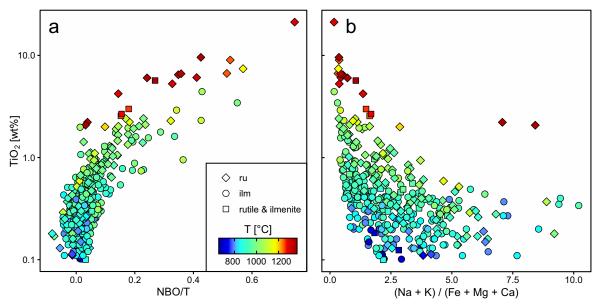


Figure 3.4: Literature experimental data plotted to display the relation of NBO/T (\mathbf{a}) and the cation ratio (\mathbf{b}) with Ti concentration in silicate melts.

3.6 Ti solubility experiments on an Archaean tonalite

To independently test our new calibration we performed solubility experiments at Macquarie University on an ilmenite-doped Archaean tonalite (PC-103 of O'Neil et al., 2012) from the Nuvvuagittuq Belt of the Superior province, Canada. Classified via feldspar diagram of O'Connor (1965), the composition is granodioritic, however we will keep the original classification as set in Adam et al. (2012). A list of run conditions and results is given in table 3.3.

3.6.1 Experimental methods

All experiments were conducted in end-loaded piston-cylinder apparatus of the type described by Boyd and England (1960) using a cold piston-in technique. Furnace assemblies were of 12.7 mm diameter and 32 mm length with talc outer sleeves and Pyrex inner sleeves. Internal components were made of ALSIMAG. Temperatures were monitored using $Pt-_{90}Rh_{10}$ thermocouple and automatically controlled by a Leeds & Northrup Electromax V temperature controller. A minus 10 % correction for the effects of friction were applied to measured pressures (Green et al., 1966). Oxygen fugacity was unbuffered but believed to have been between fayalite-quartz-magnetite (FQM) and wüstite-magnetite (WM) in the furnace type used (Green, 1976). Run conditions varied from 700 to 1100 °C and 0.5 to 2.0 GPa.

The starting materials used in experiments were powdered glass prepared from the natural tonalite PC-103, natural ilmenite, and distilled H₂O. To ensure Ti saturation for the broad range of experimental conditions 4 wt% of ilmenite was added to starting compositions. This was in-creased to 6 wt% for run 2077 (at 1000 °C and 0.5 GPa) as the previously run 2070 conducted under the same conditions was Ti-undersaturated with only 4 wt% of added ilmenite. The use of ilmenite has the advantage that rutile stability can also be assessed. The concentration of added H₂O varied from 5-15 wt% to ensure a broad range of liquidus temperatures. For comparison, two titanite-doped (5 wt%) experiments (2103, 2104) were also conducted owing to its common occurrence as an accessory mineral in TTGs.

During experiments starting materials were contained in $Ag_{70}Pd_{30}$ capsules with a total sample mass of 15 mg in each capsule. H₂O was added with a graduated micro-syringe and a careful check of weights kept at each stage of capsule preparation to guard against unwanted loss. Capsules were sealed using a PUK 3 spot-welder with capsules wrapped in wet tissue during welding. After welding, the watertight integrity of capsules was checked by placing capsules in an oven at 110 °C for ten minutes before re-weighing. To enhance crystal growth during experiments, experiments were first overheated by 100 °C for 30 minutes and then progressively cooled to target temperatures at 4-5 °C/minute. At the finish of experiments, samples were quenched by turning off power to the furnace assemblies. After capsule recovery, capsules were longitudinally sectioned with a diamond saw and then mounted in epoxy and polished preparatory to analysis.

3.6.2 Analytical methods

The major element compositions of the run products were analysed with a Caméca SX100 based at Macquarie University Sydney and a JEOL JXA-8900RL at the Geoscientific Centre Göttingen University. Beam diameters between 20 and 30 μ m were used for glass analyses with an acceleration voltage of 15 kV and beam current of 15 to 20 nA. Acquisitions times were 10 s for Na; 15 s for K, Al, Si, Fe, Mn, Mg and Ca; 30 seconds for P and 60 seconds for Ti. To evaluate Na loss during measurement we explored different beam diameters from 5 to 30 μ m over time. Figure 3.5a displays the decline of Na counts during a measurement with

Run	E	Ч	+	H_2O					hd hd	lase a	phase abundance	lce						$\sum r^2$
	$[O_{\circ}]$	[GPa]	[h]	[wt%]	<u></u>	ldh	xdo	grt	\mathbf{bt}	clz	pl	ъ	mag	tit	ilm	ru	Λ	
2076	200	0.5	168	10	55.4	7.8	1	1	7.6	ı	25.5	1	1	ı	3.8	ı	×	0.75^{*}
2075	700	1	171	10	74.3	18.8	tr	I	4.4	0.7	ı	tr	I	ı	1.7	I	х	0.60
R181	800	1	168	10	72.1	17.1	ı	I	0.7	ī	ı	ī	ı	I	2.3	I	х	0.24
2099	850	1	72	10	80.7	14.7	0.4	I	ı	ī	ı	ī	ı	I	4.2	I	х	0.68
2100	850	1	72	15	87.8	2.6	0.9	I	5.4	ı	ı	ī	ı	I	3.3	I	х	0.28
2105	850	2	72	15	82.2	8.4	1	2.4	3.2	I	ı	I	I	I	2.8	I	I	0.18
2103	850	1	96	10	84.5	9.7	I	I	ī	ī	ī	ī	2	3.8	0.1	I	ī	0.01
2104	000	1	84	10	86.6	9.3	ı	I	ı	ī	ı	ī	ı	2.5	1.6	tr	ī	0.58
R177	000	1	48	ю	86.6	ю	5.4	I	ı	ı	ı	I	ı	I	2.9	I	ı	0.05
2070	1000	0.5	24	ю	98.7	I	tr	I	I	I	ı	I	I	I	1.3	I	I	0.03
2077	1000	0.5	48	5	96.1	I	tr	I	ī	ī	ı	ī	ī	I	3.9	I	I	0.10
R174	1000	1	48	ъ	95.6	I	2.6	I	ī	ī	ı	ī	ī	I	1.8	tr	ī	0.03
R178	1000	1.5	48	ю	93.3	ı	5.2	I	ı	ī	ı	ī	ı	I	1.2	0.4	ī	0.17
2072	1100		10	ю	97.6	I	ı	I	I	I	I	ı	ı	I	1.1	1.3	ı	0.19

30

time as well as with smaller beam diameter. The counts per second (cps) are averages for 10 second intervals. Na loss during glass analyses was also assessed via mass-balances calculated between run products and starting compositions. Measured and corrected Na₂O concentrations are presented in table 3.4. The corrected Na₂O concentrations are indicated with an *.

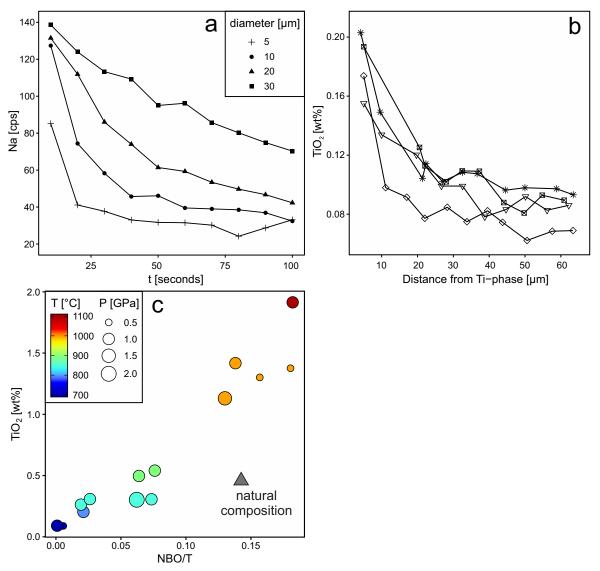


Figure 3.5: a: Na loss over time during analysis at different beam diameters. The cps is a 10 second average. b: Effect of secondary Ti-fluorescence in glass close to Ti phases. Profiles were measured in sample 2075 adjacent to ilmenite. c: TiO₂ content of melts produced in experiments on tonalite PC-103. The natural composition of PC-103 is plotted as a the grey triangle.

The spots chosen for glass analyses were randomly distributed through sample capsules although care was taken to ensure that all spots were sufficiently distance from Ti-rich accessory phases to avoid the effects of secondary fluorescence on measured TiO_2 (see Wark and Watson, 2006; Kronz et al., 2012). To assess the latter effect, we measured glass profiles with a 5 μ m diameter beam perpendicular to Ti phases. Results for Run 2075 are displayed in fig. 3.5b. At distances of $\geq 50 \ \mu$ m from rutile or ilmenite we could not detect any effect of secondary fluorescence.

3.6.3 Results

A list of run products and matching experimental conditions is presented in table 3.3. Analyses of run products are given in table 3.4. Even though no reversal experiments were conducted we assume that equilibrium was approached in our experiments based on homogenous glass compositions and euhedral crystal shapes. All experiments produced Ti-rich accessory minerals with ilmenite present in all run products. Excepting runs 2070 and 2072, all experiments were saturated with more than one mineral phase (Runs 2070 and 2072 contained ilmenite only). Runs 2076, R174, R178 and 2104 were additionally saturated in rutile. The titanite-doped runs 2103 and 2104 were both saturated in titanite together with ilmenite. Run 2104 also produced rutile. Runs 2076, 2075, R181, 2099 and 2100 contained a vapour phase, as demonstrated by the presence of vesicles in glasses. The TiO₂ concentrations of the experimentally produced glasses are positively correlated with NBO/T and temperature (fig. 3.5c). Glasses from near-liquidus experiments at around 1000 °C and with 5 wt% H₂O contain over twice the TiO₂ concentration present in the natural tonalite. Regardless of temperature, pressure and dissolved H₂O concentration, the TiO₂ concentration of the natural rock was not reproduced or even closely approached under near-liquidus conditions.

The Fe-loss resulting from experiments was calculated from mass-balances and varied from 0.1 - 9.8 % of the total Fe initially present in starting materials (table 3.4). Run 2076 experienced significant more Fe loss with 33.8 %. The low loss of run 2103 might be due to an underestimation of FeO of magnetite in the mass-balance calculation.

Table 3.4: Major element glass analyses of the experiments in wt%. Bracketed numbers are the respective standard deviation on the values last digit. Sum is given as hydrous, with presented oxides normalised to anhydrous. Na ₂ O [*] is calculated by mass balance adjusting for loss during analysis. b.d. = below detection. FeO _t is not corrected for Fe-loss. Fe-loss is presented as relative loss [%] based on mass balance

Run	n	SiO_2	TiO_2	Al_2O_3	FeO_t	MnO	MgO	CaO	Na_2O	K_2O	Sum	$\rm Na_2O^*$	Fe-loss
2076	IJ	78.1(9)	0.09(2)	13.1(4)	0.47(5)	b.d.	0.24(1)	2.0(2)	2.9(1)	3.12(3)	92.7	3.20	33.8
2075	∞	73.0(2)	0.09(2)	16.8(2)	(9) 60.00	0.07(1)	0.21(2)	2.90(5)	3.78(8)	2.20(6)	91.4	4.34	6.1
R181	9	72.5(1)	0.203(4)	16.3(1)	1.80(5)	b.d.	0.45(1)	2.48(4)	3.49~(6)	2.76(2)	92.7	4.12	0.9
2099	10	71.1(2)	0.26(2)	16.82(9)	1.50(9)	0.09(2)	0.62(2)	2.70(7)	3.99(5)	2.87(5)	93.0	4.00	9.4
2100	10	68.8(4)	0.31(2)	17.2(1)	3.19(7)	0.05(1)	0.97(4)	3.56(8)	3.4(3)	2.5(1)	89.0	3.98	0.1
2105	20	71.6(3)	0.30(1)	16.0(1)	2.73(8)	0.04(2)	0.78(3)	3.04(5)	3.1 (1)	2.40(7)	87.5	4.15	4.6
R177	10	68.7 (3)	0.50(1)	16.9(1)	2.89(9)	0.08(1)	0.75(3)	3.39~(6)	4.0(1)	2.79(3)	94.0	3.96	2.3
2070	∞	65.7(4)	1.37(5)	15.6(2)	5.5(5)	0.08(5)	2.15(8)	3.63(4)	3.3~(1)	2.47(2)	91.4	3.63	0.5
2077	ъ	66.0(1)	1.30(3)	15.97(7)	4.9(1)	0.107(2)	2.00(5)	3.58~(6)	3.60(5)	2.45(3)	95.8	3.66	2.2
R174	10	66.3 (1)	1.42(2)	16.20(8)	4.5(1)	0.09(1)	1.71(3)	3.61 (4)	3.66(7)	2.50(3)	94.2	3.79	3.6
R178	10	66.2 (2)	1.130(9)	16.32(9)	4.69(9)	0.10(1)	1.23(3)	3.73(5)	3.97(9)	2.59(4)	93.4	3.84	0.9
2072	10	65.3(2)	1.9(1)	15.84(8)	5.2~(1)	0.11(3)	2.14(2)	3.51(5)	3.54(7)	2.43(5)	93.4	3.62	4.0
2103	10	70.9(2)	0.31(2)	17.12(6)	0.92(3)	0.06(4)	0.71(4)	3.56(7)	3.66(8)	2.78(4)	91.3	3.99	0.1
2104	10	71.0(2)	0.54(3)	$16.2\ (1)$	2.41(3)	0.06(1)	0.94(4)	3.83(5)	2.51(5)	2.46(2)	89.2	4.00	1.6

3.7 Application of the new Ti-solubility model to the experimental results for PC-103

To test the accuracy of our new Ti solubility model (table 3.2, eq. (3.4)), including its applicability to melts of TTG composition, we applied it to the glass compositions given in table 3.4 of this study. The results (fig. 3.6) justify our strategy of sample filtering and noise-reduction. Whereas calibrations based on the modified and unmodified datasets give similar results for the temperature range 800-900 °C, the calibration on the unmodified dataset underestimates lower temperatures and overestimates higher temperatures. In contrast to this, the calibration on the modified dataset returns good results for both high and low temperatures with all temperatures estimated within the 1 σ uncertainty. The results are of similar accuracy to those returned by Xiong et al. (2009) but without the use of unconstrained parameters. A single exception is produced by estimates for Run R174 where both models overestimate the run temperature by 50 °C. Both models return a temperature for PC-103 of around 850 °C. As previously commented on, this is significantly less than possible liquidus temperatures as constrained by the composition of the bulk rock. The Fe-loss (table 3.4) results in lower Ti solubility but does not result in a bias of the model as the amount of Fe is accounted for in our regression.

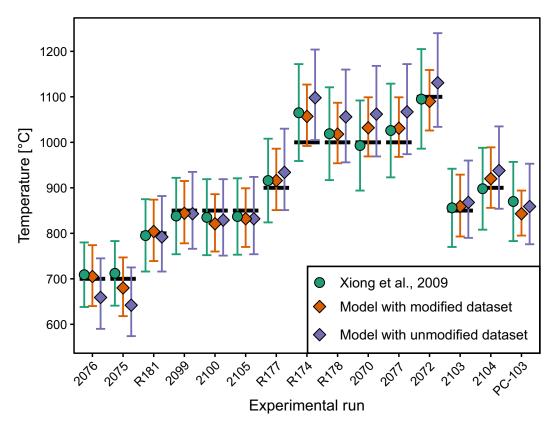


Figure 3.6: Calculated temperatures compared to actual conditions for PC-103 experiments (black bars) using the calibration model based on the modified and unmodified dataset. The modified dataset has reduced bias and scatter due to statistical operations explained in Section 3.5. Temperatures using the Xiong et al. (2009) calibration are given for comparison. 2103 and 2104 are doped with titanite. PC-103 is the natural composition. Uncertainty for Xiong et al. (2009) is a 10 % interval as given in their paper. Calculation of the natural rock PC-103 Ti-saturation temperature with Xiong et al. (2009) is based on a 1 GPa and a 5 wt% H₂O estimate.

3.8 Application of the new thermometer to Archean TTGs

Two datasets for Archean TTGs (Moyen, 2011; Johnson et al., 2019) were complemented here with data from Nutman et al. (1999) Huang et al. (2013), Laurent et al. (2014) and O'Neil and Carlson (2017). Samples appearing twice were identified and removed. The resulting dataset includes analyses for 1860 samples. This was filtered using the *GCDkit* of Janoušek et al. (2006) to include only samples with CIPW-norms conforming to the definition of either tonalite, trondhjemite or granodiorite. We further selected compositions with La > 10 ppm, Yb < 2 ppm and an Eu anomaly below 1.1 to assure the characteristic HREE depletions that define TTGs. Compositions with < 64 wt% SiO₂ (28 samples) were intentionally kept since they are potential parents to the more evolved granitoids. The filtered TTG dataset contains 359 samples.

3.8.1 Calculated Ti-saturation temperatures for TTGs

Applying our model to Archaean TTGs produces a generally positive correlation between temperature and NBO/T for a temperature range of 750 to 900 °C (fig. 3.7a). Based on the overlap with experimental data for Ti-saturated melts (fig. 3.7a), we can also distinguish between TTGs that could have been saturated (above the red line) and the ones that could not have been saturated (below the red line) in a Ti-rich accessory mineral. Many TTGs simply do not contain enough Ti to be in equilibrium with a Ti-rich accessory mineral at their expected liquidus temperatures. In any case, the calculated temperatures must be regarded as minimum estimates of potential liquidus temperatures. This is because TTG magmas may have evolved at higher temperatures where the behaviour of Ti was governed by the crystallisation of common Ti-bearing silicates, such as amphibole, pyroxene, garnet or mica. This is borne out by the consistent negative correlation between Ti and indices of fractionation in TTGs, irrespective of whether they were potentially saturated or under-saturated in a Ti-rich accessory phase.

The maximum Ti-saturation temperatures (~ 960 °C) calculated for Archaean TTGs are at

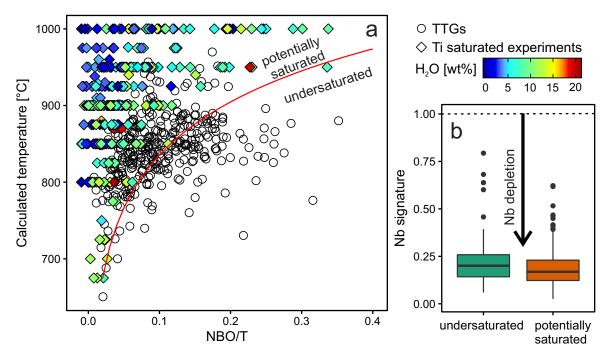


Figure 3.7: a) Ti saturated liquidus temperatures calculated from with our model for the natural TTG dataset. The Ti saturated experimental melts are plotted with colour-coded H₂O. The red line separates potentially saturated from undersaturated TTG compositions based on the extend of experimental data. b) Box plot of the Nb depletion for Ti excess phase saturated and undersaturated TTGs in comparison. Y-axis is a log₁₀ scale. The Nb signature is calculated as $Nb/Nb^* = Nb_{PM}/\sqrt{(U_{PM} * La_{PM})}$. The decision of saturation is based on the red line in fig. 3.7a. PM is from McDonough and Sun (1995).

NBO/T between 0.09 and 0.125 (fig. 3.7a). Less evolved compositions (higher NBO/T) have

lower calculated temperatures. We interpret this to be the point where more evolved TTG melts became saturated with a Ti-rich accessory mineral. More primitive compositions with NBO/T > 0.2 cannot have been saturated in Ti-rich accessory minerals at their expected liquidus temperatures. This has significant relevance for the role of Ti-rich accessory minerals in controlling high field strength element (HFSE) abundances in TTGs, as will be discussed the next section.

3.8.2 The controls on Nb-depletions in TTGs

To assess the relationship between Nb depletions in TTGs and saturation in a Ti-rich accessory phases, we calculated a Nb/Nb* signature for the 265 samples of the dataset that contain data for Nb, La and U. This was done using the relationship

$$Nb/Nb^* = Nb_{PM}/\sqrt{(U_{PM} * La_{PM})}$$

$$(3.2)$$

and mantle-normalized concentrations based on the primitive mantle of McDonough and Sun (1995). As shown in fig. 3.7b, potentially saturated as well as undersaturated TTGs both show relative Nb depletions, although the former are typically more depleted than the latter. This is consistent with a limited role for Ti-rich accessory phases in evolved TTGs magmas, but also requires a more general explanation for the Nb depletions in TTGs. This could be linked to magmas mixing whereby TTG melts that were initially saturated in a Ti-rich accessory phase mixed with Ti-undersaturated melts. Alternatively, the Nb depletions may have been inherited from source materials that were themselves already depleted in Nb.

In whatever case, it appears that earlier magmatic processes pre-dating TTG formation must be responsible for the Nb depletions in TTGs. Such an idea has already been debated in the literature. For example, Smithies et al. (2009) noted Nb depletions in the Archaean-aged Coucal basalts of the East Pilbara Terrane, which were considered by them as potential source material for TTGs. However, modelling by Johnson et al. (2017) showed that in this case rutile is still needed to explain observed Nb depletion in TTGs. Nb depletions similar to those found in the Coucal Formation are also present in other cratons (Thurston and Fryer, 1983; Crow and Condie, 1987; Puchtel et al., 1997; Jenner et al., 2009; Hoffmann et al., 2011b; Adam et al., 2012; Parks et al., 2014) and so similar arguments might be expected to apply. However, because the difference in Nb-depletions is small between Ti-saturated and undersaturated TTGs, the role of Ti-rich accessory phases would have to be limited making it likely that other phases that also fractionate Nb from La are involved. These include amphibole and mica (Foley et al., 2002; Stepanov and Hermann, 2013).

3.8.3 Implications for the evolution of TTG magmas

A corollary of low magmatic temperatures for TTGs is that their magmas can be expected to have been water-rich with between 8 to 12 wt % of dissolved H₂O (fig. 3.7). This has significant implications for potential TTG sources and settings of origin. Thus a comparison of our estimates with those of other studies is warranted. Our estimated liquidus temperatures of 750 and 900 °C are lower than those (900-1100 °C) suggested by Moyen and Stevens (2006) on the basis of melting experiments on dry basaltic starting materials. They are also lower than the temperatures suggested by Wyllie et al. (1997) for tonalitic and trondhjemitic melts under eclogite facies conditions. However, under amphibolite facies conditions TTG melts can be produced at a much lower temperatures (750-900 °C, see Wyllie et al., 1997). These conditions are comparable to estimates based on both mineral thermometry for TTGs (Bédard, 2003) and thermodynamic modelling (Palin et al., 2016; Johnson et al., 2017). Low magmatic temperatures may reflect low degrees of melting, the presence of an aqueousfluid phase during melting, evolution from hydrous parent magmas, or some combination of these factors. In the case of the first option, it can be shown that low degree melts produced by fluid-absent melting of amphibolite (Clemens and Vielzeuf, 1987; Rushmer, 1991) contain comparatively modest H_2O concentrations (4.6-6.5 wt%). This objection can be removed if melting occurred in a fluid-saturated environment, as in a lower crustal setting affected by underthrusting of hydrated oceanic crust. Such an option was favoured by Hastie et al. (2016) who argued for fluid involvement arising from the dehydration of oceanic basalt involved in

3.9 Summary and conclusions

the basal melting of oceanic plateaus.

We have formulated a new thermometer for silicate melts based on the solubility of Ti-rich accessory minerals (rutile and ilmenite). This is based on an extensive experimental dataset and constrains temperature as a function of Ti, NBO/T and (Na + K)/(Fe + Mg + Ca). Application of our thermometer to Archaean TTGs produces temperature estimates that are generally between 750 and 900 °C. We note that for many TTGs these temperatures are significantly less than expected liquidus temperatures and that consequently liquids of this composition are unlikely to have been saturated in either rutile or ilmenite. This has implications for the role of Ti-rich accessory phases in the production of Nb depletions in TTGs. These must be ascribed to either inheritance and/or the role of Ti-bearing silicate minerals, such as amphibole and mica. Another corollary of low magmatic temperatures is that they can only be achieved if TTG magmas were relatively hydrous, with 8-12 wt% of dissolved H₂O. This cannot be accounted for by low degrees of melting alone and favours the presence of a fluid.

3.10 Remarks and usage of the model

There are several things to consider with regard to the applicability of the Ti solubility model. One is that the model does not answer the question of whether the liquidus of a particular sample was ever saturated in either rutile or ilmenite. It only returns an expected saturation temperature. In addition, the thermometer is not calibrated for titanite. Furthermore, the model assumes that whole rocks are representative of original melts and is not suitable for rocks influenced by cumulate processes. Whether or not a sample was potentially saturated in either rutile and/or ilmenite can be assessed by comparing it to the experimental range shown in fig. 3.7a. If the sample lies within the covered range of experimental compositions, the Ti-saturated liquidus can be calculated and the result treated as a minimum temperature estimate. The thermometer is not recommended for samples that lie outside of this range.

NBO/T is calculated after Mysen (1990) as (eq. (3.3)):

$$\frac{NBO}{T} = \frac{2 * (2 * Si + 1.5 * Al + Fe + Mg + Ca + 0.5 * (Na + K)) - 4 * (Si + Al)}{Si + Al}$$
(3.3)

All elements in the equation are in mol%. The Ti saturated liquidus temperature is calculated as (eq. (3.4)):

$$log_{10}(Ti) = -2.63 + 0.00248 * T + 0.8 * \frac{NBO}{T} - 0.097 * \frac{Na + K}{Fe + Mg + Ca}$$
(3.4)

Temperature in eq. (3.4) is given in °C, Ti and the cation ratio are in mol%. The 1 σ uncertainty the model is at 11 % based on the comparison of calculated and recorded temperatures.

Table 3.5: List of studies containing Ti phase saturated experiments. H_2O is the amount dissolved in the melt, either given or estimated by the difference to 100 % total of the analyses.

study	n	T [°C]	P [GPa]	H ₂ O [wt%]	TiO ₂ [wt%]	NBO/T
Alonso-Perez et al. (2009)	16	800-1000	0.8-1.2	4-15	0.13-0.86	-0.01-0.32
Beard and Lofgren (1991)	59	800-1000	0.1-0.69	1-12	0.12-1.60	-0.04-0.25
Castro et al. (1999)	3	800-900	0.6-1.0	9-11	0.17-0.19	-0.03-(-0.01)
Conrad et al. (1988)	19	675-925	1.0	5-13	0.10-0.66	0.00-0.08
Gaetani et al. (2008)	22	1150-1450	0.0001 - 3.5	0	2.07 - 38.9	-0.02-0.80
García-Arias et al. (2012)	8	800-900	0.6-1.0	10-12	0.11-0.42	0.00-0.06
Gardien et al. (1995)	4	750-950	1.0	5-15	0.06-0.37	-0.06-0.05
Getsinger et al. (2009)	6	925-1000	1.4	4-6	0.13 - 0.54	0.01-0.08
Green and Pearson (1986),	114	900-1080	0.75 - 3.0	2-16	0.29-4.42	0.00 - 0.55
Hayden and Watson (2007)	13	700-1000	1.0	6-10	0.10-1.09	-0.06-0.06
Klemme et al. (2002)	2	1200-1300	3.0	0	2.00-4.22	0.10-0.14
Laurie and Stevens (2012)	6	870-900	1.9 - 3.0	16-19	0.10-0.50	0.02 - 0.05
Patiño Douce and Beard (1996)	33	840-950	0.3 - 1.5	1-6	0.07 - 0.47	-0.02-0.05
Patiño Douce and Johnston (1991)	18	825-1075	0.7 - 1.3	0-4	0.02 - 0.77	-0.03-0.03
Patiño Douce (2005)	6	975-1150	2.7 - 3.0	2-8	0.17 - 0.59	-0.08-0.01
Patiño Douce and Beard (1995)	44	875-1000	0.3 - 1.5	1-7	0.16-1.26	-0.03-0.12
Pertermann and Hirschmann (2003)	4	1250-1335	2.0 - 3.0	0	6.07-6.66	0.35 - 0.51
Pickering and Johnston (1998)	3	812-900	1.0	4-6	0.13-0.20	-0.06-(-0.01)
Qian and Hermann (2013)	8	800-1000	1.0 - 1.5	6-21	0.23-1.66	0.01-0.14
Rapp and Watson (1995)	11	1000-1150	0.8-3.2	5-15	0.36-2.31	0.05 - 0.43
Rapp et al. (1991)	6	1000-1150	1.6 - 3.2	6-9	0.85-2.23	0.05 - 1.18
Ryerson and Watson (1987)	10	1000-1350	0.6-3.0	1-14	1.42 - 9.57	0.03 - 0.57
Sen and Dunn (1994)	13	900-1150	1.5 - 2.0	6-9	0.26-2.29	0.03 - 0.32
Sisson et al. (2005)	22	825-925	0.7	5-9	0.06 - 0.78	0.01 - 0.16
Skjerlie and Johnston (1992)	2	1000-1050	1.0	3	0.28 - 0.31	0.06-0.08
Skjerlie and Johnston (1993)	9	875-1075	1.0	2-7	0.07 - 0.74	0.00-0.22
Skjerlie and Johnston (1996)	16	850-1000	1.0-2.0	2-7	0.11 - 0.72	-0.08-0.05
Skjerlie and Patiño Douce (1995)	3	900-950	1.0	4-7	0.40 - 0.64	0.02 - 0.08
Spandler et al. (2008)	4	1240-1350	3.0 - 5.0	0	2.56 - 5.68	0.15 - 0.26
Spicer et al. (2004)	16	800-1000	0.3-0.32	0-4	0.11 - 0.71	-0.01-0.04
Springer and Seck (1997)	3	940-1115	0.5	5-13	0.34 - 2.91	0.06 - 0.34
Xiong et al. (2009)	36	750-1250	1.5 - 3.5	8-14	0.11 - 2.44	-0.01-0.12
Xiong et al. (2011)	3	900-1350	2.0	6-11	0.30-3.80	0.02 - 0.05
Yearron (2003)	2	925-1000	1.6	-	0.57 - 0.75	0.04-0.09

3.11 Acknowledgements

A. Wellhäuser is supported by an iMQRES from Macquarie University. T. Rushmer and J. Adam acknowledge the support from Macquarie University. We gratefully thank A. Silbersdorf for statistical advice, A. Kronz for analytical assistance, S. Turner for valuable discussion and suggestions, J. O'Neil for providing the sample PC-103 and T. Green for remarks on the manuscript and providing an extensive experimental dataset. A. Audédat is thanked for comments on an earlier version of the manuscript.

CHAPTER 4

TTG suite differentiation paths as a function of water availability

4.1 Preface

This study was initially intended to be the main task of the thesis which, however shifted in focus while progressing. The original plan was to connect greenstone melting experiments from Adam et al. (2012), conducted on samples from the Nuvvuagittuq greenstone belt with a liquidus study on surrounding felsic granitoids. Thereby fields of matching residual and liquidus saturating phases should have been identified. The goal shifted due to acknowledging the study of Wyllie et al. (1997) who had the same study design with a far broader extend as possible for this thesis.

The original scope of the manuscript was designed by John Adam and Tracy Rushmer, the shift in focus was done by myself. Experiments were conducted by John Adam and myself. The discussion and interpretation of experimental results involved Tracy Rushmer, John Adam and me. I wrote the first draft of the manuscript. Subsequently the manuscript was reviewed by John Adam and Tracy Rushmer.

4.2 Abstract

We investigated the saturated liquidus of an Eoarchean granodiorite from the Nuvvuagittuq belt with crystallisation experiments and thermodynamic modelling to identify potential paths of differentiation. With piston cylinder experiments varying in pressure (0.5-2.0 GPa) and initial H₂O (5 and 10 wt%), we found several points of multiple saturation from which the granodiorite can further differentiate. We constructed P-T sections via THERMOCALC for 2, 5 and 10 wt% H₂O and extracted isobaric profiles at 0.5, 1.0, 1.5 and 2.0 GPa. No experimentally defined cotectic path or isobaric profile can retrace the observed geochemical variability of the Nuvvuagittuq tonalite-trondhjemite-granodiorite (TTG) suite, especially in respect to the alkali elements. However, we have identified a critical dependence of the differentiation path on H₂O. The suppression of plagioclase crystallisation in liquidus proximity under hydrous conditions at elevated pressure (≥ 1.0 GPa) is essential to produce trondhjemitic compositions by crystal fractionation along a cotectic path involving hornblende/clinopyroxene (cpx) and orthopyroxene (opx)/garnet. At low pressure, or dry conditions, melt evolves towards a granodioritic composition by fractionating plagioclase and hornblende/opx.

A large literature compilation of natural TTGs is difficult to describe by a single cotectic

path not involving plagioclase due to a parallel alignment of the data to the An-Qtz plane in the CMAS recalculated Qtz-Fo-An ternary diagram. As the lack of an Eu-anomaly, which rules out the involvement of plagioclase, is one of the TTG suite's distinct features, contrary to post-Archean granites, TTGs most likely do not align on a liquid line of descent. Instead, they formed at varying H_2O and pressure conditions outside of the plagioclase stability field.

4.3 Introduction

The possible formation mechanism(s) of tonalite-trondhjemite-granodiorite suites (TTG, Jahn et al., 1981) are yet to be resolved even though they are the major component of Archean continental crust (Martin et al., 2005). Their composition (K_2O poor while being enriched in large ion lithophile elements (LILEs), depleted in heavy rare earth elements (HREEs), Nb Ta and Ti, no Eu-anomaly and high Sr/Y ratios (Moyen and Martin, 2012)) is distinct from rocks that are associated with modern continent formation processes. Understanding the formation of TTGs provides an essential insight into the unknown Archean geodynamic environment(s) and addresses the major question at what point modern style plate tectonics started operating (Laurent et al., 2014; Turner et al., 2014; Hastie et al., 2016; Tang et al., 2016).

In general, there is agreement that TTGs formed from partial melting of hydrated basalt (Moyen and Stevens, 2006). The depletion in HREEs and high Sr/Y ratios are generally associated with the presence of garnet during their formation and/or evolution, directly connected to crustal depth. Furthermore, high Sr/Y ratios point to the absence of plagioclase contiguous to the lacking Eu-anomaly. Low K_2O concentration, the crucial major element feature of TTGs, can be linked to either high degree melting, low K_2O in the source, or the fractionation of a K_2O bearing phase. The enrichment in LILE is attributed to the source rock (Martin et al., 2014) or the involvement of fluid (Hastie et al., 2016). The depletion of Nb, Ta and Ti is associated with the presence of a Ti phase during melt formation/evolution (chapter 3).

Several geodynamic scenarios have been proposed in which TTGs could have been generated. These include (i) steep subduction with slab melting (Martin et al., 2005; Laurie and Stevens, 2012) as thought for modern adakites (Martin et al., 2005; Castillo, 2012); (ii) shallow subduction/underthrusting/stacking of oceanic crust with melt formation in the garnet stability field (Nagel et al., 2012; Nutman et al., 2015; Hastie et al., 2016) and (iii) basal melting of a thick oceanic plateau at high pressure with possible interplay with mantle plumes, resulting in crustal overturns (Collins et al., 1998; Bédard, 2006a; Smithies et al., 2009; Bédard, 2018; Wiemer et al., 2018).

Aside the uncertain Archean geodynamic environment, the mechanisms resulting in jointly occurring tonalites, trondhjemites and granodiorites are uncertain as well. A generally accepted model is that they formed at different depths (Moyen, 2011; Hoffmann et al., 2011a; Moyen and Martin, 2012) based on their trace element signature and in case of K_2O -richer

granitoids, by remelting of older TTG intrusions (Watkins et al., 2007). The formation of TTGs by crystal fractionation is generally discarded as no continuous trends from parental melts to TTGs are observed (Moyen and Martin, 2012). However, in numerous experimental basalt melting studies only few experiments resulted in glass compositions that resemble TTG. This is contrary to their common occurrence in Archean cratons, implying that it should be fairly easy to produce them. Either they must have formed under very specific conditions, spatially and temporarily separated during the Archean, or other magmatic processes as crystal fractionation, accumulation or magma mixing were involved. Several studies suggest that crystal fractionation and accumulation could be relevant to TTG formation (Arth et al., 1978; Martin, 1993; Kamber et al., 2002; Bédard, 2006a; Hoffmann et al., 2014). Proposed scenarios are high pressure fractionation of mantle wedge derived melts (Kleinhanns et al., 2003), a scenario similar as proposed for modern adakites (Macpherson et al., 2006; Coldwell et al., 2011), and mid to upper crustal fractionation / accumulation of feldspar and hornblende (Liou and Guo, 2019; Smithies et al., 2019; Laurent et al., 2020) alike observed by Jagoutz et al. (2013) in a recent arc system.

In this study, we examine the liquidus conditions of the Archean granodiorite PC-103 (O'Neil et al., 2008; Adam et al., 2012) by crystallisation experiments and petrological modelling to show that the amount of H_2O is critical for the differentiation of TTG suites and test how they can differentiate by crystal fractionation.

4.3.1 Formation conditions for TTGs

Out of a vast range of experimental studies, TTG-like compositions (as defined in Moyen and Martin, 2012) have been produced in only few melting experiments (Rapp and Watson, 1995; Winther, 1996; Skjerlie and Patiño Douce, 2002; Adam et al., 2012; Laurie and Stevens, 2012; Hastie et al., 2016) on mostly basaltic compositions between 1.5-3.0 GPa, 800-1050 °C, by both dehydration and fluid-present melting (Figure 4.1, Table 4.1). Notably, no TTG-like melt was produced at lower pressure conditions. A major factor for the experiments to result in glasses of TTG composition is the low K₂O content of their starting materials (0.08 - 0.17 wt%). The experimental melts of Laurie and Stevens (2012) and Hastie et al. (2016) do not match the field of TTGs (natural data from Nutman et al. (1999), Moyen (2011), Huang et al. (2013), Laurent et al. (2014), O'Neil and Carlson (2017), and Johnson et al. (2019), filtered for La > 10, Yb < 2 and an Eu-anomaly in between 0.9 and 1.1) because they do not contain enough K₂O as shown in fig. 4.1a. As observed by Wyllie et al. (1997) and visible in fig. 4.1b, tonalites tend to form at higher- and trondhjemites at lower temperature.

In the Qtz-Fo-An plane based on compositions being recalculated by CMAS (O'Hara, 1968), most experiments only marginally overlap with TTG compositions (fig. 4.1b) that could be primary liquids due to the absence of an Eu anomaly. Especially in some of the experiments of Laurie and Stevens (2012) and Hastie et al. (2016) the Qtz component is too large. The experimental melts of Skjerlie and Patiño Douce (2002) contain the least Qtz component and match well. However, their melts are in equilibrium with quartz, which shifts the melt composition away from the Qtz corner. Rapp and Watson (1995) produce a TTG composition at 1.6 GPa and it is possible to infer the cotectic path based on their comprehensive melting study for this pressure (fig. 4.1d). The interpreted cotectic path matches the array of TTGs, falling on a plag - hbl/cpx/grt controlled cotectic. However, the involvement of plagioclase will result in a negative Eu anomaly, which is generally not observed in TTGs (Moyen and Martin, 2012).

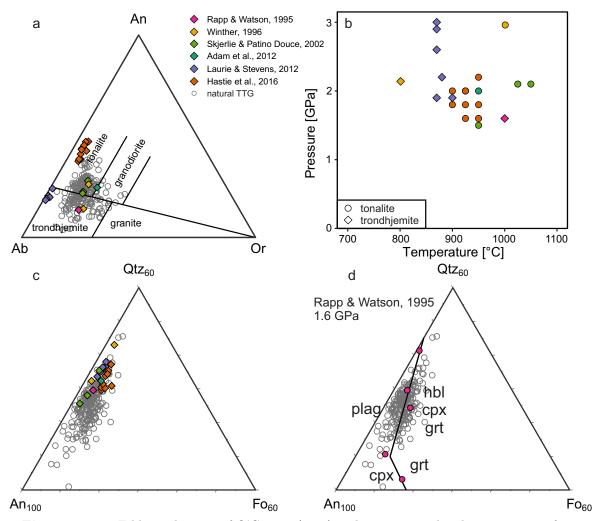


Figure 4.1: a: Feldspar diagram of O'Connor (1965) with experimental melt compositions from Rapp and Watson (1995), Winther (1996), Skjerlie and Patiño Douce (2002), Adam et al. (2012), Laurie and Stevens (2012), and Hastie et al. (2016) plotted together with natural TTG data from Nutman et al. (1999), Moyen (2011), Huang et al. (2013), Laurent et al. (2014), and O'Neil and Carlson (2017) and Johnson et al. (2019). The compilation is filtered for samples only containing tonalites, trondhjemites and granodiorites; La > 10, Yb < 2 and an Eu-anomaly in between 0.9 and 1.1. By this procedure, compositions not being TTG and affected by fractionation or accumulation are avoided. b: P-T condition plot of the experimental melts that match TTG composition. c: Qtz-Fo-An plot with the same data as in fig. 4.1a, recalculated as CMAS (O'Hara, 1968) d: Experiments by Rapp and Watson (1995) on an migmatic amphibolite at 1.6 GPa with interpreted cotectic path.

TTG like compositions were also produced by direct melting in several petrological modelling studies (Nagel et al., 2012; Palin et al., 2016; Johnson et al., 2017). The TTG melt production conditions were determined to be between 1.0-1.8 GPa and below 1000 °C. This is in contrast to most experimentally produced TTG melts, which were produced at higher pressures. The differentiation of TTGs by crystal fractionation is not covered by experimental work or modelling.

In this study, we examine the crystallisation sequence of an Archean granodiorite from the Nuvvuagittuq Greenstone Belt (NGB) experimentally by piston cylinder and rapid quench autoclave experiments as well as calculated P-T pseudosections using THERMOCALC (Powell et al., 1998). From that we can identify points of multiple saturation in liquidus proximity as origin for differentiation paths that lead to the compositional diversity of TTG suites. We use the 3.66 Ga granodiorite PC-103 (O'Neil et al., 2008, 2012; Adam et al., 2012) from the Hadean to Eoarchean NGB, Northeastern Superior Province (NESP) in Canada. The major element composition of PC-103 is displayed in table 4.2. The NGB major components are mafic to ultramafic rocks, chemical sediments and a minor fraction of felsic compositions. The whole belt is highly deformed and metamorphosed under at least upper greenschist facies conditions. The felsic rocks comprise the 3.66 Ga trondhjemite veins. The felsic rocks are interpreted to have formed from melting of the surrounding Hadean mafic lithologies (O'Neil et al., 2012).

Table 4.2: Major element composition of the sample PC-103 from O'Neil et al. (2012) in wt%	Table 4.2: Major element composition of the sample PC-103	from O'Neil et al. (2012) in wt%.
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SiO_2	TiO_2	Al_2O_3	FeO_t	MnO	MgO	CaO	Na_2O	K_2O	P_2O_5	LOI
66.1	0.45	15.9	3.74	0.08	2.17	3.67	3.66	2.44	0.11	1.3

Table 4.1: Partial melting experi	iments that result in glasses	s of TTG cc	mposition	as defined	experiments that result in glasses of TTG composition as defined in Moyen and Martin (2012).
Study	starting material	temp	press	H_2O	assemblage
		[0°C]	[GPa]	[wt%]	
Rapp and Watson, 1995	migmatic amphibolite	1000	1.6	7.8	plag, hbl, cpx, opx, grt, qz
Winther, 1996	AAT $3/2$	801	2.14	15.7	grt, qz, hbl
Winther, 1996	AAT $3/2$	1001	2.96	12.9	grt, cpx, qz
Skjerlie and Patiño Douce, 2002	quartz eclogite	950	1.5	5.4	cpx, zo, qz, plag, ky, grt
Skjerlie and Patiño Douce, 2002	quartz eclogite	1025	2.1	4.9	cpx, zo, plag, qz, ky, grt
Skjerlie and Patiño Douce, 2002	quartz eclogite	1050	2.1	3.9	cpx, zo, plag, qz, ky, grt
Adam et al., 2012	boninite	950	2	8.4	cpx, grt, opx, chromite
Laurie and Stevens, 2012	eclogite	870/900	1.9	15.9	grt, cpx, ru, (ilm)
Laurie and Stevens, 2012	eclogite	870-900	2.2 - 3.0	16-18.9	grt, cpx, ru
Hastie et al., 2016	depleted tholeiite	925	1.6	10.1	cpx, hbl, plag, mag
Hastie et al., 2016	depleted tholeiite	950	1.6	6.8	cpx, hbl, plag, opx, mag
Hastie et al., 2016	depleted tholeiite	006	1.8	10.4	hbl, cpx, plag, mag, qz
Hastie et al., 2016	depleted tholeiite	925	1.8	4.4	hbl, cpx, plag, mag
Hastie et al., 2016	depleted tholeiite	950	1.8	10.0	cpx, opx, hbl, plag, grt, mag
Hastie et al., 2016	depleted tholeiite	006	2	8.1	cpx, hbl, grt, st, qz, mag
Hastie et al., 2016	depleted tholeiite	925	2	11.1	cpx, hbl, grt, st, mag
Hastie et al., 2016	depleted tholeiite	925	2	12.9	cpx, hbl, grt, opx, st, mag
Hastie et al., 2016	depleted tholeiite	950	2.2	15.4	cpx, hbl, grt, st, mag
Abbreviation: $plag = plagioclase$, $hbl = hornblende$, $cpx = clinopyroxene$, $opx = orthopyroxene$, $grt = garnet$,	, $hbl = hornblende$, $cpx =$	= clinopyre	oxene, op	$\mathbf{x} = \text{ortho}$	pyroxene, $grt = garnet$,
qz = quartz, $zo = zoisite$, $ky = kyanite$, $ru = rutile$, $ilm = ilmenite$, $st = staurolite$, mag = magnetite	xyanite, ru = rutile, ilm =	= ilmenite,	st = stat	ırolite, m	ag = magnetite

4.4 Methods

4.4.1 Petrological modelling

THERMOCALC (version 3.45, Powell et al., 1998) calculations where performed in the Na₂O-CaO-K₂O-FeO-MgO-Al₂O₃-SiO₂-H₂O-TiO₂-O₂ (NCKFMASHTO) system, using version 6 of the internally consistent Holland and Powell (2011) a-x models dataset. Amphibole, clinopyroxene and melt a-x relations are from Green et al. (2016), orthopyroxene, garnet, biotite, muscovite and ilmenite from White et al. (2014), K-feldspar and plagioclase from Holland (2003), spinel from White et al. (2002) and epidote from Holland and Powell (2011). A restraint in investigating liquidus conditions with THERMOCALC version 3.45 is that no mixing models for TiO₂ and Fe³⁺ into the melt are present. Therefore a complete liquidus can not be reached, as there will always be a Ti-phase (ilmenite or rutile) present. The recently published expanded thermodynamic dataset from Holland et al. (2018) comprises a solution model for TiO₂ into melt but does not return reasonable near-liquidus phase assemblages, most likely due to our PC-103 composition being outside of the calibration range because the model is only valid for tholeiitic to mildly alkalic melt compositions.

We calculated P-T sections with different amounts of H_2O available (2, 5 and 10 wt%) because the availability of water during TTG formation is a major uncertainty (see chapter 3). Relevant for high H_2O calculations with the model is the limitation of H_2O being a pure phase that does not dissolve any components. Hence, the melt composition in presence of free H_2O would actually be different in a natural system or experiment. The THERMOCALC input for the different amounts of H_2O is displayed in table 4.3.

Table 4.3: PC-103 input composition for THERMOCALC at different H_2O contents displayed in mol% if not indicated otherwise in the column head.

$H_2O [wt\%]$	H_2O	SiO_2	Al_2O_3	CaO	MgO	FeO	K_2O	Na ₂ O	TiO_2	0
2	6.77	67.01	9.51	3.95	3.39	3.17	1.61	3.71	0.35	0.53
5	15.37	60.83	8.64	3.59	3.08	2.88	1.46	3.37	0.32	0.48
10	28.38	51.46	7.31	3.03	2.60	2.43	1.23	2.85	0.27	0.44

4.4.2 Experimental methods

We conducted near liquidus experiments on a glass made from the Archean tonalite PC-103 (O'Neil et al., 2012; Adam et al., 2012). Experiments were conducted between 750 and 1100 °C, pressure between 0.3 and 2.0 GPa and H_2O of either 5 or 10 wt%.

The experiments ≥ 0.5 GPa were conducted at Macquarie University on a piston cylinder apparatus as described by Boyd and England (1960) using a cold piston-in technique. A minus 10 % pressure correction due to friction is applied (Green et al., 1966). For temperature adjustment and monitoring we used a Pt-Pt₉₀Rh₁₀ thermocouple with a Leeds & Northrup Electromax V temperature controller. The oxygen fugacity condition during the experiment was unbuffered but believed to be between fayalite-quartz-magnetite (FQM) and wüstitemagnetite (WM) based on the furnace type (Green, 1976).

In the furnace assembly 15 mg of sample were sealed in $Ag_{70}Pd_{30}$ capsules via welding. Distilled water was inserted into the capsules before powder via micro-syringe. The capsule weight was carefully monitored after every step to guard against unwanted loss. To ensure leak tightness of the sealed capsule, it was heated to 100 °C for one hour and weighed subsequently. The furnace consists of an ALSIMG insert on both sides of the $Ag_{70}Pd_{30}$ capsule, inside a graphite tube surrounded by a Pyrex- and outermost talc sleeve.

Experiments at 0.3 GPa were carried out at Nanjing University using a vertical, externally heated, cold seal rapid quench autoclave system with a setup as described in Matthews et al. (2003). Oxygen fugacity was controlled by Ni rods. For the experiments 30 mg of sample, a mix of glass powder and distilled water, were sealed in gold capsules and heated subsequently to 110 °C for 2 hours to exclude pre-run leakage. The capsules were also weighed after the experiment.

4.4.3 Analytical methods

Major element composition of the experimentally produced glasses were analysed at Macquarie University using a Caméca SX100 and at Georg-August University using a JEOL JXA-8900RL. The analyses were conducted with an acceleration voltage of 15 kV, 15 to 20 nA beam current and beam diameters of either 20 or 30 μ m. Acquisition times were 15 s for Al, Si, Fe, Mg, Ca, Na and K; 30 s for Ti, Mn and P.

The analytical loss of Na was assessed by exploring different beam diameters over time as described in chapter 3 and displayed by fig. 4.2a. To better constrain H₂O dissolved in the melt we include H by difference into the matrix correction. It is peculiar for the JEOL software that including H into matrix correction only works for ZAF. Therefore we compare three different matrix corrections: (1) phi-rho-Z, (2) ZAF and (3) ZAF with H. The results are displayed in fig. 4.2b, for the glass analysis of R174 (see chapter 3). Whereas phi-rho-Z and ZAF are identical within error, including H into the matrix correction significantly increases the abundance of Al₂O₃ and SiO₂. The total sum is increased by almost 2 wt%. It can be concluded that the addition of H to the matrix correction improves the H₂O estimate by difference. The ZAF + H correction was used for the experiments 191001, 193001 and 194001.

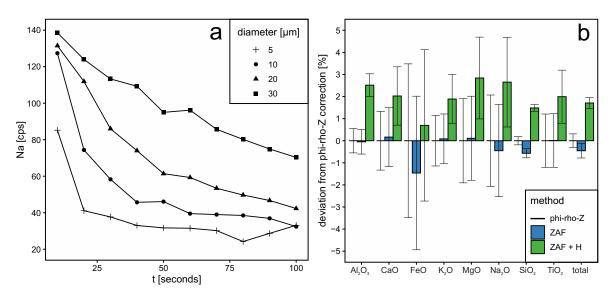


Figure 4.2: a: Na loss over time during analysis at different beam diameters. The cps is a 10 second average. b: Comparison of different matrix correction methods normalised to the values calculated from phi-rho-Z. The error bars are the 1 σ sd of 10 glass analysis in experiment R174 (chapter 3).

4.5 Results

4.5.1 Experimentally determined saturated liquidus

It is important to consider the potential source rock in context of the liquidus position in P-T space and saturation of phases in crystallisation experiments. As the source rock is unlikely to be mono-mineralic, it is expected that the liquidus would be multiply saturated.

The experimentally examined phase stabilities of PC-103 are displayed as a P-T sections in fig. 4.3 separated by initial H₂O content. With 5 wt% H₂O present (fig. 4.3a), opx is the dominant liquidus phase from 0.5 to 1.5 GPa. The liquidus forms a positive slope from 950 to 1050 °C. At 2 GPa garnet and cpx both saturate the liquidus at 1050 °C. Plagioclase crystallises pressure independent below 950 °C. Amphibole is stable at \leq 900 °C.

For 10 wt% H₂O (fig. 4.3b) the liquidus was not reached with 10 % of solid phase left at 900 °C and 1.5 GPa (see table 4.4, run 2091). Directly compared with 5 wt% H₂O at the same conditions, the degree of melting is 5 % higher with 10 wt% H₂O present. Hornblende is stable in all conducted experiments. Cpx stability is decreased by not being stable at 900 °C and 1.5 GPa. Garnet and opx have the same stability range as in the experiments with 5 wt% H₂O at 900 °C. An excess fluid phase is only present at 0.3 GPa.

In the two diagrams (fig. 4.3) several points of multiple saturation can be identified. At 5 wt% H₂O, points of multiple saturation are at 0.5 GPa, 925 °C (plagioclase and opx) and 2.0 GPa, 1050 °C (garnet and cpx). With 10 wt% H₂O the liquidus is multiply saturated in hornblende, plagioclase and Fe-oxide at 0.3 GPa, 800 °C, hornblende, opx and Fe-oxide at 1.0 GPa, 900 °C and in hornblende, opx and garnet at 1.5 GPa, 900 °C.

The major element compositions of analysed glasses are presented in table 4.5. We report and

use corrected Na₂O concentrations based on mass balance calculations by r^2 minimisation. Fe-loss is as well assessed by mass balance calculation and displayed in table 4.5. Harker diagrams for the analysed glasses are displayed in appendix fig. 4.7 and 4.8. The modes presented in table 4.4 are as well calculated by mass balance.

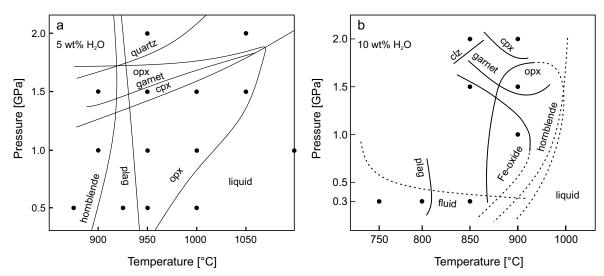


Figure 4.3: P-T sections for PC-103 based on crystallisation experiments with **a**: 5 wt% H_2O and **b**: 10 wt% H_2O present. Black filled circles are the P-T conditions at which experiments were conducted. Abbreviations: cpx = clinopyroxene, opx = orthopyroxene, plag = plagioclase and clz = clino-zoisite.

4.5.2 Calculated phase diagrams

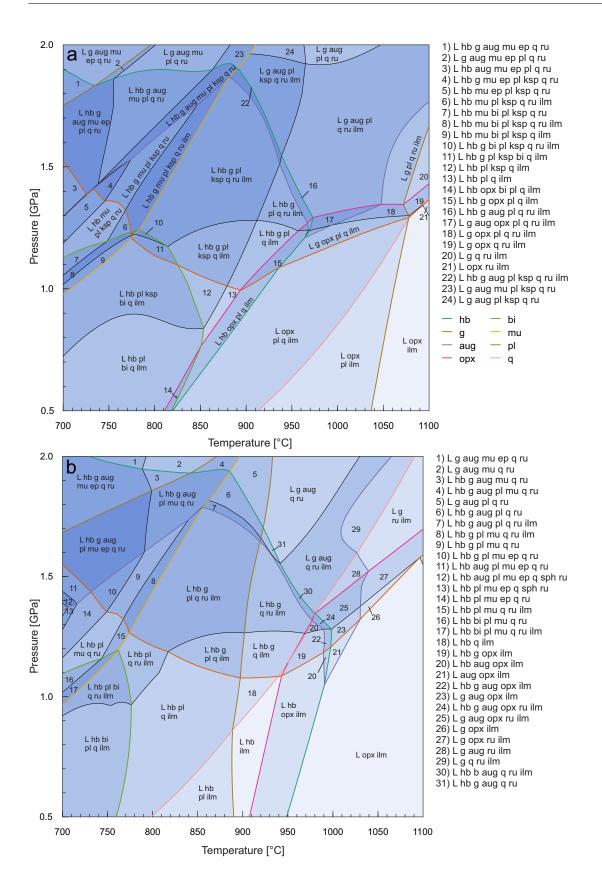
We calculated three pseudosections for PC-103 via THERMOCALC (Powell et al., 1998) with differing H₂O content of 2, 5 and 10 wt% and a Fe³⁺/Fe²⁺ ratio of 0.3, displayed in fig. 4.4. For the section with 2 wt% H₂O (fig. 4.4a) the liquidus is not reached within the temperature interval between 700 and 1100 °C. Phases stable at liquidus proximity are opx and plagioclase up to 1.3 GPa. An association of garnet, quartz, plagioclase and a minor amount of cpx are saturating phases above 1.5 GPa. Due to the high temperatures hornblende is not stable in liquidus proximity as the maximum temperature extend of its stability is 970 °C at 1.3 GPa. Modebox plots showing isobaric phase profiles through the diagram at 0.5, 1.0, 1.5 and 2.0 GPa are displayed in appendix fig. 4.9. Major element melt compositions of the profiles are given in table 4.6.

The pseudosection with 5 wt% H_2O (fig. 4.4b) is calculated between 700 and 1100 °C and from 0.5 to 2.0 GPa. As for 2 wt% H_2O , the liquidus is outside of the temperature range. Opx and hornblende are stable between 0.5 and 1.1 GPa in proximity of the liquidus. At higher pressure cpx becomes stable. Garnet is stable in proximity of the liquidus at 1.2 GPa, above 1.6 GPa in association with quartz and cpx. Mode box plots showing isobaric phase profiles through the diagram at 0.5, 1.0, 1.5 and 2.0 GPa are displayed in fig. 4.10.

Run	H	Ч	t	H_2O	<u></u>	hbl	cpx	xdo	grt	bt	$_{\rm klz}$	plag	dz	mag	tit	ilm	ru	Δ	Σr^2
	[0]	[GPa]	[µ]	[wt%]															
1997	825	0.5		ъ	77.9	9.3		3.1	ı		ı	9.5		ı		0.2	ı	ı	0.06
R100	006	1.5		5	85.2	2.6	2.9	0.3	6	ī	ı	ı	1.4	ı	ī	ı	ī	ı	0.22
1990	1050	1.5		5	97.9	ı	ī	2.1	ı	ī	ı	ı	ī	ı	ī	ı	ī	ı	0.84
1988	950	1.5		5	91.3	ı	3.3	5.4	ı	ī	ı	ı	ī	ı	ī	ı	ī	ı	0.26
1992	1050	2.0		5	89.9	ī	0.9	ī	9.2	ī	I	ī	ī	ı	ī	ı	ī	ī	0.13
1994	925	0.5		5	95.4	ī	ī	4.6	ı	ī	I	tr	ī	ı	ī	ı	ī	ī	0.05
R116	950	2.0		5	82.9	,	3.3	ŀ	13.8	ī	ı	I	ī	ı	ī	ı	ī	ī	0.29
R152	1000	1.0	48	Q	98.6	ı	ī	1.4	ı	ī	ı	ı	ī	ı	ī	ı	ī	ī	0.17
2060	950	0.5	48	J.	97.6	ŗ	ī	2.45	ı	ī	ı	ŗ	ī	ı	ī	ı	ī	ī	0.67
2072	1100	1.0	10	5	100	ı	ī	ī	ı	ī	I	ī	ī	ī	ī	I	ī	ī	ı
R168	950	1.0	48	5	96.3	ı	ī	3.7	ı	ī	ī	ī	ī	ī	ī	ı	ī	ı	0.59
2091	006	1.5	67	10	89.0	8.6	ī	2.4	tr	ī	I	ī	ī	ī	ī	I	ī	ī	0.29
2092	006	2.0	81	10	84.0	1.4	1.2	ı	13.4	ī	ı	ı	ı	ı	ī	ı	ı	ı	0.39
2093	850	2.0	96	10	78.3	17.8	ī	ı	tr	ī	3.9	ı	ı	ı	ī	ı	ī	ı	0.18
2097	006	1.0	96	10	88.6	10.1	ı	0.1	ı	ī	ı	ı	ı	1.1	ī	ı	ī	ı	0.53
191001	850	0.3	168	10	90.3	7.9	ī	ı	ı	ī	ı	ı	ı	1.8	ī	ı	ı	x	0.06
193001	800	0.3	264	10	78.5	9.2	ī	ī	ı	ī	I	9.8	ī	2.5	ī	ı	ī	x	0.32
194001	750	0.3	336	10	61.8	15	,	ı	ı	ī	ı	22.1	ı	1.1	ī	ı	ı	x	0.69

Table 4.4: Experimental run conditions and phase assemblages. The phase abundance was calculated via mass balance with the quality of fit presented by Σr^2 on Na₂O loss corrected major element compositions. "x" indicates the presence of a phase without quantification. "tr" is an abundance insignificant to the mass balance calculation but detected by microprobe.

Run	ч	SiO,	TiO,	Al ₂ O ₂	FeO+	MnO	MøO	CaO	Na.oO	KaO	$P_{2}O_{5}$	Sum	Na.0*	Fe-loss
1997	101	71 8 (3)	0.34 (2)	15.8 (2)	1.97 (6)	0.04 (1)	0.53 (3)	2.52 (4)	3.49 (3)	3.29 (2)	0.16 (1)	90.81	3.80	3.8
R100	9	70.8 (8)	0.5(2)	16.0(8)	1.4(2)	b.d.	0.7(2)	2.7 (4)	4.5(3)	3.3(2)	0.12(2)	91.74	4.20	0.7
1990	9	67.5 (6)	0.44(2)	16.64(7)	2.85(5)	0.06(1)	2.15(3)	3.68(3)	4.00(4)	2.53(4)	0.10(4)	95.24	4.00	19.5
1988	4	68.7 (1)	0.43(2)	17.12(1)	2.46(7)	0.05(1)	0.92(2)	3.46(2)	4.0(1)	2.75(3)	0.10(3)	94.14	4.09	9.0
1992	x	70(1)	0.41(2)	15.8(1)	2.01(6)	0.03(2)	1.15(4)	3.26(7)	4.29(4)	2.81(5)	0.10(3)	92.59	4.29	7.0
1994	x	67.9(2)	0.45(1)	16.83(5)	3.0(1)	0.07(2)	1.20(2)	3.73(3)	4.02(6)	2.64(2)	0.13 (3)	93.61	4.02	3.2
R116	x	71.9(2)	0.33(2)	16.00(3)	0.98(3)	b.d.	0.54(2)	2.56(3)	4.38(4)	3.12(3)	0.15(1)	91.27	4.38	9.4
R152	S	68.0(4)	0.45(1)	16.1(2)	3.64(6)	0.08(1)	1.78(4)	3.70(6)	3.57(4)	2.58(2)	0.14(1)	92.10	3.80	1.4
2060	4	68.3(1)	0.46(1)	16.08(9)	3.54(4)	0.08(1)	1.78(5)	3.70(4)	3.35(2)	2.57(1)	0.14(2)	92.05	3.81	0.2
R168	6	68.3(7)	0.47(1)	16.27(2)	3.03(5)	0.08(2)	1.65(2)	3.75(6)	3.7(1)	2.59(3)	0.13(2)	92.84	3.86	6.8
2091	11	70(1)	0.34(2)	17.2(2)	2.31(7)	0.05(1)	0.95(6)	3.2~(1)	3.29(6)	2.34(4)	0.10(1)	85.92	3.95	1.9
2092	10	73.8(6)	0.33(1)	15.4(1)	1.26(9)	b.d.	0.84(1)	2.58(6)	2.94(5)	2.75(7)	0.11(1)	89.68	4.36	8.4
2093	x	75.1(4)	0.20(1)	15.5(2)	1.10(4)	b.d.	0.55(2)	2.35(5)	2.6(8)	2.55(8)	0.11(1)	88.75	4.18	2.8
2097	10	70.7 (3)	0.39(1)	16.32(7)	2.72(4)	0.06(1)	0.92(2)	3.21(3)	3.00(7)	2.57(2)	0.11(1)	90.66	3.87	7.0
191001	10	70.4(2)	0.35(1)	16.71(8)	1.7(1)	0.05(1)	0.98(4)	3.03(5)	3.94(8)	2.71(2)	0.11(2)	92.69	4.00	1.4
193001	10	73.3(3)	0.21(3)	15.48(9)	1.27(8)	0.06(1)	0.6(1)	2.39(3)	3.84(7)	2.73(5)	0.10(1)	92.73	3.88	3.1
194001	10	(6) 0 22	0.14(2)	14.9 (1)	0 92 (4)	0.06 (1)	036 (9)	9 06 (4)	3.39(6)	2,83,(5)	0.06 (9)	93 32	3 33	7 1



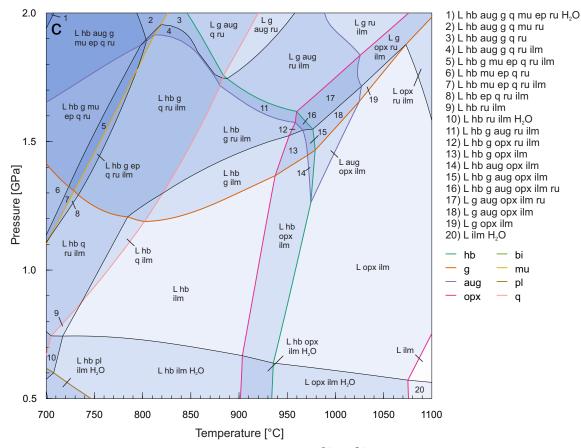


Figure 4.4: P-T pseudosections of PC-103 with Fe^{3+}/Fe^{2+} ratio of 0.3 and **a**: 2, **b**: 5 and **c**: 10 wt% H₂O. Abbreviations: L = liquid, hb = hornblende, g = garnet, aug = clinopyroxene, opx = orthopyroxene, mu = muscovite, bi = biotite, ep = epidote, pl = plagioclase, ksp = alkali feldspar, q = quartz, ru = rutile, ilm = ilmenite.

The pseudosection with 10 wt% H₂O (fig. 4.4c) is calculated between 700 and 1100 °C and from 0.5 to 2.0 GPa. In this section the true liquidus is present at 1075 °C and 0.5 GPa. The ilmenite stable under these conditions is an artefact of the missing mixing model of TiO₂ and silicate melt. Due to the high water content there is free H₂O present at pressures below 0.8 GPa. From 0.5 to 1.3 GPa the liquidus is multiply saturated with hornblende and opx. Above 1.5 GPa the stability of hornblende decreases to lower temperatures and the liquidus is saturated mainly in garnet and opx with a minor amount of cpx. The crystallisation of quartz and plagioclase is strongly suppressed. Mode box plots showing isobaric phase profiles through the diagram at 0.5, 1.0, 1.5 and 2.0 GPa are displayed in fig. 4.11.

4.5.3 Comparison of experimental and calculated phase stabilities

Phase stabilities in experiments and calculated sections are only partially consistent. Comparing the 5 wt% H₂O sections (4.3a and fig. 4.4b) shows that the stability of opx is increased in the calculated section by around 200 °C at 0.5 GPa. The stability of amphibole is 50 °C higher at 0.5 GPa and the discrepancy increases at 1.0 GPa to 100 °C. Quartz has an increased stability field in the calculated section as well. Whereas it is only stable at 950 °C and 2 GPa in the experiments, the calculated phase boundary reaches from 800 °C, 0.5 GPa to 1075 °C, 2 GPa. Garnet also has a greater stability field in the calculated section, extending to lower pressures at high temperatures. In contrast to the experiments, it is stable at 1000 and 1050 °C at 1.5 GPa. The plagioclase stability is similar for both methods.

Likewise is the case for 10 wt% H₂O. Opx is stable at temperatures of 900 °C and below in both methods. Fluid saturation is similar in both methods, however the experimentally determined saturation boundary is not well defined. Epidote and cpx stability are similar as well, within deviation of 50 °C. The stability field of garnet is larger in the calculated section as it did not occur experimentally at 850 °C and 1.5 GPa. Garnet precipitation can be kinetically inhibited in experiments, which could explain the difference. As for the other minerals, there might be differences in the experiments used to calibrate THERMOCALC and our experiments. The Fe loss observed in our experiments could contribute to the difference, however it is small for most of our experiments.

4.6 Melt evolution via crystal fractionation

For our interpretation we do not consider the age relations of the Nuvvuagittuq TTG suite, as the most differentiated trondhjemites bear the oldest ages. However, they must have differentiated and less evolved felsic compositions of similar age might not be disclosed or preserved.

To investigate the melt evolution of TTGs, we plot them together with our experimental/modelling results in two different types of ternary diagrams. The feldspar triangle by O'Connor (1965), illustrates the change in alkalis, a crucial point for TTGs. The second diagram is the Qtz-Fo-An plane of CMAS re-calculated compositions (O'Hara, 1965) to display melt evolution in a higher dimensional system. The natural TTGs plotted into the diagrams are only filtered via the feldspar diagram (O'Connor, 1965), La > 10 and Y < 2. Samples with Eu anomaly are intentionally kept, to include samples affected by fractionation or accumulation.

4.6.1 The experimental system

There are two distinct trends of melt differentiation for experimental glasses displayed in the normative feldspar diagram of O'Connor (1965) (fig. 4.5a and 4.5b). The first trend is a depletion of CaO without a change in the K₂O/Na₂O ratio, visible for 5 and 10 wt% H₂O. The trend is caused by the retardation of plagioclase crystallisation due to either high H₂O or high temperature. This is most distinct at 2 GPa where garnet and cpx are controlling the melt evolution, both not capable of fractionating Na₂O and K₂O. Plagioclase crystallises at 5 wt% H₂O, temperatures <950 °C (fig. 4.3a) and shifts the trend towards a K₂O enrichment. At 10 wt% H₂O plagioclase crystallises ≤ 800 °C which shifts the trend in the same way towards a K_2O enrichment, observable in the 0.3 GPa experiments.

We re-calculated the experiments and natural TTGs to CMAS components (CaO-MgO-Al₂O₃-SiO₂, O'Hara, 1968) and plot it in the Qtz-Fo-An plane (fig. 4.5c & 4.5d), again separated by the initial water content. The diagrams are reduced in their size to 60 % Qtz and Fo component for a more detailed presentation. In contrast to the feldspar diagrams, the TTGs from the Nuvvuagittuq plot on a narrow field around our starting material PC-103 with only 4 samples deviating from the field. Other natural TTG compositions trend almost parallel to the An - Qtz plane at Fo ≤ 10 .

At 5 wt% H_2O (fig. 4.5c) the melt is governed by an opx/cpx - hbl/grt cotectic, depending on pressure. The melt evolves almost straight towards the Qtz-An plane, perpendicular to the array formed by the Nuvvuagittuq TTGs. At 0.5 GPa plagioclase stability causes a cotectic path parallel to the Nuvvuagittuq TTG array. As the amount of crystals is below 20 % in all experiments, the trends are not very distinct and plot close to each other.

At 10 wt% H_2O (fig. 4.5d) there is a distinct cotectic path governed by hornblende and plagioclase at 0.3 GPa towards highly evolved compositions. This path resembles the differentiation trend seen in the Nuvvuagittuq TTGs, except for being offset towards a lower Fo component. The cotectic also fits well to the overall trend of the larger TTG dataset and is similar to the cotectic produced by Rapp and Watson (1995) displayed in fig. 4.1d. At higher pressure conditions, the number of experiments is insufficient to define cotectic paths. However, it is observable that at 2 GPa the melt compositions evolves in a quite similar direction, in this case in presence of hornblende, clinozosisite and garnet. The difference between both melt evolution paths at 0.3 and 2 GPa is more distinct in the feldspar diagram (fig. 4.3b).

The experiments show that the direction of differentiation within the feldspar diagram is strongly influenced by the amount of H₂O, however the trends are small and difficult to further quantify or generalise based on the amount of experiments. In the range of fractionation ($\leq 40\%$) seen in the experiments it is not possible to reproduce the natural rocks of the Nuvvuagittuq suite. On the one hand, due to mismatching alkalis (fig. 4.5a and 4.5b), and on the other, because of a lateral offset due to lacking the Fo component (fig. 4.5c and 4.5d). However, the general trend of TTGs can be retraced with both, a hornblende - feldspar cotectic at 0.5 GPa and a high pressure trend comprising hornblende, garnet and clinozoisite at 2 GPa.

4.6.2 The modelled system

We extracted isobaric profiles from the the THERMOCALC P-T diagrams (fig. 4.4) containing modes and phase compositions for 0.5, 1.0, 1.5 and 2.0 GPa. The recalculated normative melt compositions are plotted in fig. 4.6a, 4.6b and 4.6c. The two trends seen in the experimental melts are also present in the calculated melt compositions at 5 and 10 wt% H₂O. The modelling, which comprises higher degrees of fractionation at lower temperatures than our

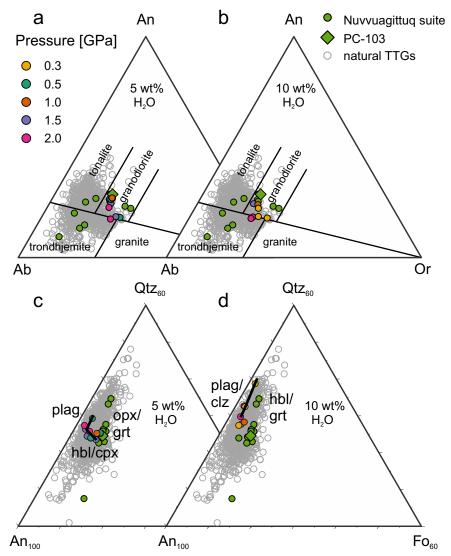


Figure 4.5: Feldspar diagram of O'Connor, 1965 with our experimental melts for a: 5 and b: 10 wt% H₂O, Nuvvuagittuq TTGs (O'Neil et al., 2012) and other natural TTG data (Nutman et al., 1999; Moyen, 2011; Huang et al., 2013; Laurent et al., 2014; O'Neil and Carlson, 2017; Johnson et al., 2019). Diagrams c and d contain the same datasets as a & b, recalculated to CMAS components (O'Hara, 1968) and projected in the Qtz-Fo-An plane. The diagrams are reduced in extend to 60 % Qtz and Fo. Abbreviations: plag = plagioclase, opx = orthopyroxene, cpx = clinopyroxene, grt = garnet, hbl = hornblende, clz = clinozoisite.

experiments, shows that the K_2O enrichment trend shifts to a K_2O depletion at pressures above 1 GPa, once mica becomes stable. The melt evolution at 2 wt% H₂O lacks the CaO depletion as plagioclase is already stable at 1050 °C. The melt enriches in K_2O until mica becomes a stable phase.

In contrast to the experimental melts, the calculated melts match several samples of the Nuvvuagittuq suite along their differentiation paths. Along the 1.0 GPa differentiation trend at 2 wt% H₂O the natural granodioritic compositions of the Nuvvuagittuq TTGs are matched.

Furthermore, at 2.0 GPa high degrees of fractionation (50 % for 10 wt% H₂O, 65 % for 5 wt% H₂O and 90 % for 2 wt% H₂O), trondhjemitic compositions of the Nuvvuagittuq suite are similar. This match is only an artefact within the feldspar diagram, apparent by trends in the Qtz-Fo-An projection (fig. 4.6d, 4.6e and 4.6f) based on recalculated melt compositions in CMAS (O'Hara, 1968).

At low pressure, for 2 and 5 wt% H₂O (fig. 4.6d, 4.6e) a similar cotectic path as for the 0.3 GPa, 10 wt% H₂O experiments is present, however at 2 wt% it is governed by opx - plagioclase instead of hornblende - plagioclase. The melts at pressures ≥ 1 GPa and 2 wt% H₂O evolve towards the An end-member due to the early presence of quartz within the crystallisation sequence. With 5 wt% H₂O present, quartz crystallisation is retained to lower temperatures wherefore the melt first evolves governed by either opx, garnet or hornblende towards the An-Qtz plane.

At H_2O contents of 10 wt% (fig. 4.6f) with 0.5 and 1.0 GPa, the melt has no cotectic path until 750 °C. The melt is evolving by the crystallisation of either opx or hornblende. At 1.5 GPa the melt is governed by a garnet - hornblende cotectic towards the An-Qtz plane until quartz crystallises at 850 °C. At that point the Fo component of the system is already almost exhausted. For 2.0 GPa the cotectic control starts at 900 $^{\circ}$ C with garnet/cpx - quartz on the An - Qtz plane. Except for isobaric crystallisation paths that contain feldspar, neither the evolution of the Nuvvuagittuq TTGs, nor the array of other natural TTGs can be retraced. As we have already seen for the experimental melts, the melt evolution path is strongly dependent on the amount of H_2O present. In the feldspar diagram, with 2 wt% H_2O , the melt evolves towards K_2O rich compositions, irrespective of pressure due to the presence of plagioclase. With 5 wt% H₂O the stability of plagioclase is already retarded by 150-200 $^{\circ}$ C and melt evolution in proximity of the liquidus is governed by either hornblende, garnet or cpx. Therefore, there is an initial depletion in CaO and once plagioclase crystallises the melt enriches in K_2O . The same is true for 10 wt% H_2O where plagioclase is almost completely suppressed. Irrespective of pressure, the melt evolves on a CaO depletion trend. Only once mica crystallises the melts are strongly depleted in K_2O .

4.6.3 Was crystal fractionation involved?

PC-103 cannot be the starting point of fractionation to produce the Nuvvuagittuq TTG suite. It is furthermore questionable that crystal fractionation shaped the majority of the suite as the individual samples differ in their alkali content but behave similar in regard to their decrease of Al_2O_3 , FeO_t and MgO along differentiation paths (appendix fig. 4.7). It is further reasonable to assume that the differences in K_2O/Na_2O within the suite are not the result of internal crystal fractionation. Alternatives are the fractionation of a less evolved parental magma under differing conditions or different degrees of melting. Accumulation of plagioclase can also lead to low K_2O/Na_2O ratios, however there is no positive Eu-anomaly present in

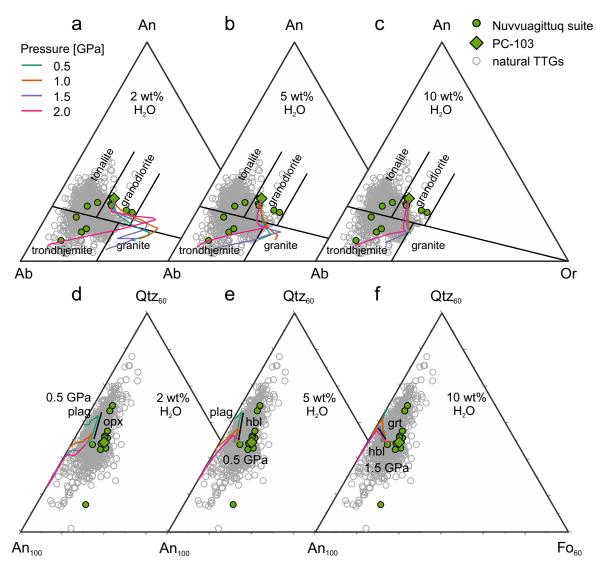


Figure 4.6: Feldspar diagram (O'Connor, 1965) with isobaric melt compositions profiles for a: 2, b: 5 and c: 10 wt% H₂O calculated with THERMOCALC for different H₂O contents with Fe^{3+}/Fe^{2+} ratio of 0.3. Natural TTG data is from Nutman et al. (1999), Moyen (2011), Huang et al. (2013), Laurent et al. (2014), and O'Neil and Carlson (2017) and Johnson et al. (2019). The sub-figures d, e & f display the same data recalculated as CMAS (O'Hara, 1968) and plotted into the Qtz-Fo-An plane. The diagrams are reduced in extend to 60 % Qtz and Fo. Modes of the isobaric profiles are in appendix fig. 4.9, 4.10 & 4.11. Abbreviations: plag = plagioclase, opx = orthopyroxene, hbl = hornblende, grt = garnet.

the Nuvvuagittuq suite. This is the same predicament as for the 1.6 GPa cotectic path from Rapp and Watson (1995) in fig. 4.1d and our experiments. A high pressure cotectic path of clinozoisite - grt/hbl as in fig. 4.5d might be an alternative, though clinozoisite drastically changes the trace element pattern (Bédard, 2006a), which is not observed. An option that avoids the presence of plagioclase is proposed by Adam et al. (2012). In their interpretation, TTGs can be formed along pressure dependent cotectic paths above 1.0 GPa, controlled by garnet and cpx/opx that lay perpendicular to the TTG array. Similar cotectic paths are present in fig. 4.5c where melt is controlled by garnet-cpx at 2 GPa and in fig. 4.6f with a hornblende - garnet cotectic at 1.5 GPa.

It was remarked by Kleinhanns et al. (2003) that H_2O is of significant importance in the differentiation/formation of TTGs by determining the path of fractionation by controlling plagioclase crystallisation. Starting from a tonalitic or less evolved composition (Liou and Guo, 2019), crystal fractionation under hydrous conditions involving garnet, hornblende or pyroxene will produce trondhjemitic compositions, whereas H_2O poor melts will produce granodioritic compositions as observable in fig. 4.6. Very hydrous conditions for TTG formation are favoured by Laurie and Stevens (2012) who explain trondhjemite formation by fluid present slab melting.

An option we did not explore in our experiments and modelling is the absence of plagioclase due to high pressure (> 2 GPa). This might also be a suitable environment to produce trondhjemitic compositions.

4.7 Conclusions

From our experiments and modelling we can conclude that the internal differentiation of TTGs is strongly dependent on the presence of H_2O . Water rich systems will trend towards tonalitic to trondhjemitic compositions along a cotectic path governed by hornblende, garnet and opx/cpx. Under dryer conditions the system will evolve towards granodioritic to granitic compositions due to plagioclase crystallisation.

It is difficult to retrace the array of Eu anomaly free TTGs without plagioclase involved in governing the cotectic. Therefore this array is most likely not a liquid line of descent. It rather seems that TTGs where formed along hbl/cpx - grt/opx controlled cotectic paths perpendicular to the array at different pressure conditions and/or elevated H₂O content. TTGs containing an Eu anomaly could likely have formed along a lower pressure plagioclase hornblende/opx cotectic path. We were not able to experimentally reproduce the compositional diversity of the Nuvvuagittuq TTGs, however identified the required differentiation paths to do so. Starting with a K_2O poorer composition than PC-103 should enable the evolution towards the trondhjemite members of the suite.

4.8 Acknowledgements

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4.9 Appendix

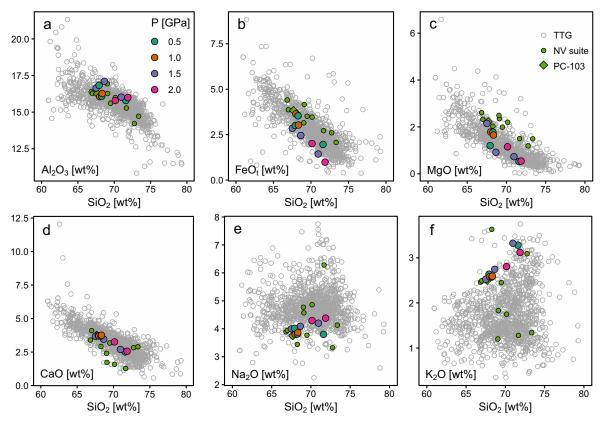


Figure 4.7: Major element scatter plots for glass compositions from PC-103 experiments with 5 wt% H_2O , the Nuvvuagittuq Suite (O'Neil et al., 2012) and other natural TTGs (Nutman et al., 1999; Moyen, 2011; Huang et al., 2013; Laurent et al., 2014; O'Neil and Carlson, 2017; Johnson et al., 2019).

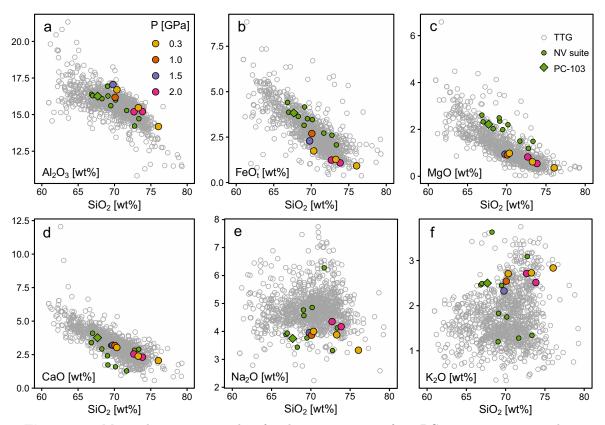


Figure 4.8: Major element scatter plots for glass compositions from PC-103 experiments with 10 wt% H₂O, the Nuvvuagittuq Suite (O'Neil et al., 2012) and other natural TTGs (Nutman et al., 1999; Moyen, 2011; Huang et al., 2013; Laurent et al., 2014; O'Neil and Carlson, 2017; Johnson et al., 2019).

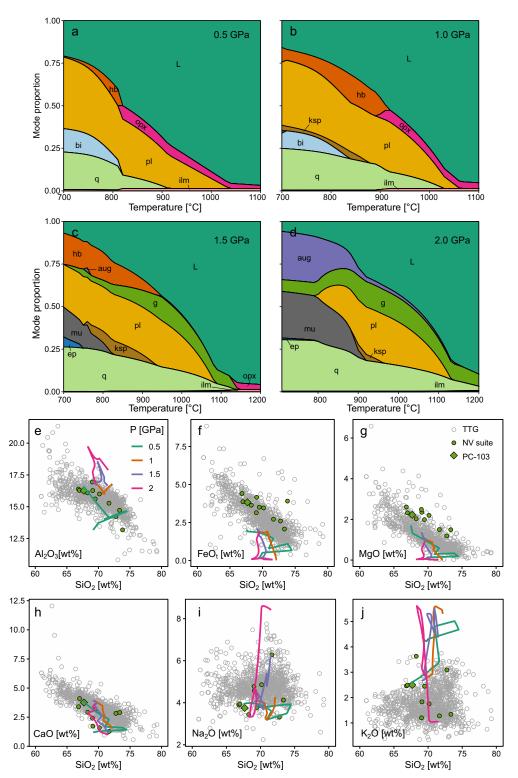


Figure 4.9: a-d: Modes for different pressure sections through the P-T pseudosection of PC-103 calculated with 2 wt% of H_2O (fig. 4.4a). Abbreviations : L = liquid, hb = hornblende, opx = orthopyroxene, pl = plagioclase, ilm = ilmenite, bi = biotite, q = quartz, ksp = K-feldspar, aug = augite, mu = muscovite, ep = epidote. e-j: Harker diagrams for melt compositions based on the profiles of a-d plotted with the Nuvvuagittuq TTGs (O'Neil et al., 2012) and natural TTG (Nutman et al., 1999; Moyen, 2011; Huang et al., 2013; Laurent et al., 2014; O'Neil and Carlson, 2017; Johnson et al., 2019).

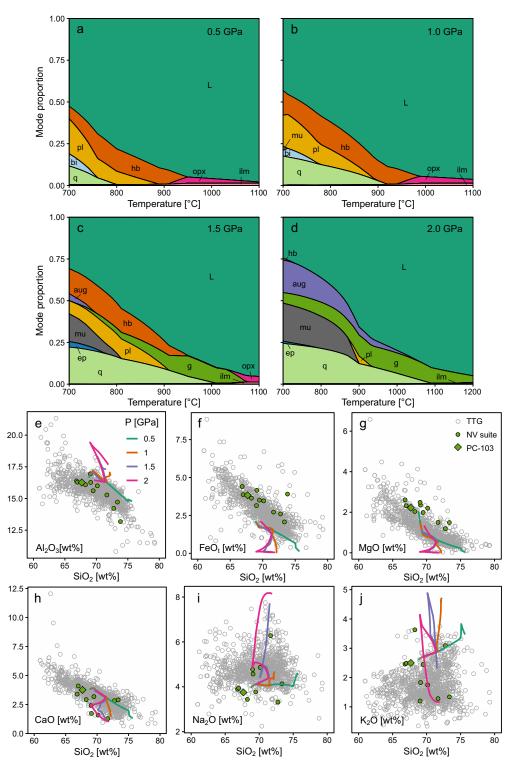


Figure 4.10: a-d: Modes for different pressure sections through the P-T pseudosection of PC-103 calculated with 5 wt% of H_2O (fig. 4.4b). Abbreviations : L = liquid, hb = hornblende, opx = orthopyroxene, pl = plagioclase, ilm = ilmenite, bi = biotite, q = quartz, aug = augite, mu = muscovite, ep = epidote. e-j: Harker diagrams for melt compositions based on the profiles of a-d plotted with the Nuvvuagittuq TTGs and natural TTG (Nutman et al., 1999; Moyen, 2011; Huang et al., 2013; Laurent et al., 2014; O'Neil and Carlson, 2017; Johnson et al., 2019)

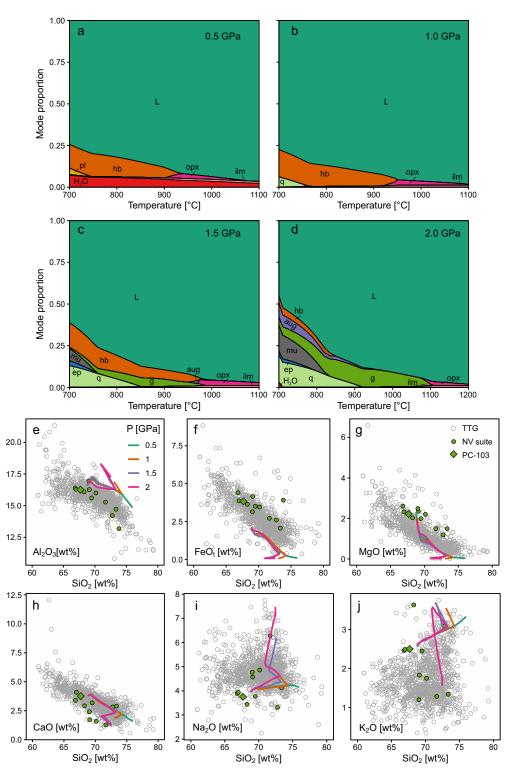


Figure 4.11: a-d: Modes for different pressure sections through the P-T pseudosection of PC-103 calculated with 10 wt% of H₂O (fig. 4.4c). Abbreviations : L = liquid, hb = hornblende, opx = orthopyroxene, pl = plagioclase, ilm = ilmenite, bi = biotite, q = quartz, aug = augite, mu = muscovite, ep = epidote. e-j: Harker diagrams for melt compositions based on the profiles of a-d plotted with the Nuvvuagittuq TTGs and natural TTG (Nutman et al., 1999; Moyen, 2011; Huang et al., 2013; Laurent et al., 2014; O'Neil and Carlson, 2017; Johnson et al., 2019)

H_2O^i	P	a is giver T	melt	H_2O^m	SiO_2	Al_2O_3	MgO	FeO_t	CaO	Na ₂ O	K ₂ O
20	[°C]	[GPa]	[%]	20		2 ~ 3		u		2 0	20
2	0.5	1100	96.8	2.1	67.5	16.4	1.70	2.03	3.76	3.92	2.58
2	0.5	1090	96.6	2.1	67.5	16.4	1.64	2.01	3.77	3.93	2.58
2	0.5	1080	96.4	2.1	67.6	16.5	1.58	2.00	3.78	3.93	2.59
2	0.5	1070	96.2	2.1	67.6	16.5	1.52	1.98	3.78	3.94	2.59
2	0.5	1060	96.0	2.1	67.6	16.5	1.46	1.96	3.79	3.95	2.60
2	0.5	1050	95.9	2.1	67.7	16.5	1.40	1.94	3.80	3.96	2.60
2	0.5	1040	95.7	2.1	67.7	16.6	1.34	1.92	3.80	3.97	2.61
2	0.5	1030	94.4	2.1	67.9	16.4	1.28	1.90	3.70	3.98	2.65
2	0.5	1020	92.5	2.2	68.2	16.2	1.22	1.90	3.55	3.98	2.70
2	0.5	1010	90.6	2.2	68.6	16.0	1.16	1.89	3.40	3.99	2.75
2	0.5	1000	88.8	2.3	68.9	15.8	1.10	1.87	3.26	3.98	2.81
2	0.5	990	86.9	2.3	69.2	15.6	1.04	1.85	3.13	3.96	2.87
2	0.5	980	85.1	2.4	69.5	15.4	0.98	1.82	3.00	3.94	2.93
2	0.5	970	83.2	2.4	69.8	15.2	0.92	1.78	2.88	3.91	3.00
2	0.5	960	81.3	2.5	70.2	15.0	0.86	1.74	2.77	3.87	3.06
2	0.5	950	79.5	2.6	70.5	14.8	0.80	1.69	2.66	3.83	3.13
2	0.5	940	77.6	2.6	70.8	14.6	0.74	1.63	2.56	3.77	3.20
2	0.5	930	75.8	2.7	71.1	14.5	0.69	1.57	2.47	3.71	3.27
2	0.5	920	73.9	2.8	71.5	14.3	0.63	1.50	2.39	3.64	3.35
2	0.5	910	71.7	2.9	71.6	14.1	0.58	1.43	2.30	3.58	3.45
2	0.5	900	68.6	3.0	71.6	14.1	0.55	1.38	2.22	3.56	3.59
2	0.5	890	65.7	3.1	71.5	14.1	0.52	1.33	2.14	3.53	3.74
2	0.5	880	63.0	3.3	71.4	14.1	0.49	1.26	2.06	3.50	3.90
2	0.5	870	60.4	3.4	71.3	14.1	0.45	1.19	1.99	3.46	4.05
2	0.5	860	58.1	3.6	71.3	14.1	0.42	1.12	1.92	3.41	4.20
2	0.5	850	55.8	3.8	71.2	14.1	0.39	1.04	1.85	3.36	4.35
2	0.5	840	53.8	3.9	71.1	14.0	0.35	0.96	1.79	3.31	4.51
2	0.5	830	51.8	4.1	71.1	14.0	0.32	0.88	1.73	3.26	4.66
2	0.5	820	50.0	4.2	71.0	14.0	0.29	0.80	1.68	3.20	4.81
2	0.5	810	40.1	4.6	73.9	14.6	0.34	1.10	1.59	3.49	5.02
2	0.5	800	36.8	5.0	74.0	14.6	0.29	1.00	1.54	3.59	4.96
2	0.5	790	33.8	5.4	74.2	14.6	0.25	0.90	1.50	3.70	4.88
2	0.5	780	31.2	5.8	74.3	14.6	0.21	0.78	1.45	3.82	4.78

Table 4.6: Melt compositions extracted from isobaric profiles of the calculated P-T sections (fig. 4.4) H_2O^i is the water content in the system, H_2O^m is dissolved in the melt. If not stated otherwise data is given in wt%.

			Tabl	e 4.6 – C	Continue	ed from p	previous	page			
H_2O^i	Р	Т	melt	H_2O^m	SiO_2	$\mathrm{Al}_2\mathrm{O}_3$	MgO	FeO_t	CaO	Na ₂ O	K_2O
2	0.5	770	28.9	6.2	74.5	14.6	0.18	0.67	1.41	3.93	4.68
2	0.5	760	27.0	6.3	70.0	13.7	0.14	0.52	1.29	3.79	4.31
2	0.5	750	25.4	6.6	69.9	13.6	0.11	0.41	1.27	3.84	4.24
2	0.5	740	24.1	7.0	69.7	13.5	0.09	0.32	1.25	3.87	4.22
2	0.5	730	23.1	7.3	69.6	13.5	0.07	0.24	1.24	3.87	4.23
2	0.5	720	22.2	7.6	69.5	13.4	0.05	0.18	1.23	3.85	4.27
2	0.5	710	21.5	7.9	69.3	13.3	0.04	0.13	1.22	3.81	4.33
2	0.5	700	20.8	8.2	69.1	13.2	0.03	0.10	1.21	3.76	4.39
2	1.0	1100	95.3	2.2	69.2	16.9	1.23	1.95	3.90	4.07	2.68
2	1.0	1090	95.1	2.2	69.3	17.0	1.18	1.93	3.90	4.08	2.68
2	1.0	1080	94.9	2.2	69.3	17.0	1.14	1.90	3.91	4.09	2.69
2	1.0	1070	94.8	2.2	69.3	17.0	1.09	1.88	3.91	4.09	2.69
2	1.0	1060	94.3	2.2	69.4	17.0	1.04	1.85	3.89	4.10	2.71
2	1.0	1050	91.8	2.2	69.8	16.7	0.99	1.85	3.75	4.07	2.78
2	1.0	1040	89.4	2.3	70.2	16.5	0.94	1.85	3.61	4.03	2.85
2	1.0	1030	86.9	2.4	70.6	16.3	0.89	1.83	3.48	3.98	2.92
2	1.0	1020	82.8	2.5	70.6	16.2	0.87	1.86	3.37	3.97	3.06
2	1.0	1010	78.7	2.7	70.6	16.2	0.85	1.89	3.27	3.95	3.21
2	1.0	1000	75.0	2.8	70.7	16.1	0.83	1.91	3.18	3.93	3.35
2	1.0	990	71.5	2.9	70.7	16.1	0.81	1.92	3.09	3.90	3.51
2	1.0	980	68.2	3.1	70.7	16.1	0.78	1.91	3.01	3.86	3.66
2	1.0	970	65.2	3.3	70.7	16.1	0.75	1.90	2.94	3.81	3.81
2	1.0	960	62.3	3.4	70.8	16.0	0.72	1.87	2.87	3.76	3.97
2	1.0	950	59.7	3.6	70.8	16.0	0.68	1.84	2.81	3.71	4.13
2	1.0	940	57.2	3.8	70.9	16.0	0.65	1.79	2.75	3.65	4.29
2	1.0	930	54.8	4.0	70.9	16.0	0.61	1.73	2.69	3.59	4.46
2	1.0	920	52.7	4.1	71.0	16.0	0.58	1.66	2.64	3.53	4.62
2	1.0	910	49.4	4.3	70.9	16.1	0.55	1.69	2.48	3.45	4.85
2	1.0	900	45.4	4.4	70.8	16.1	0.54	1.77	2.31	3.34	5.12
2	1.0	890	42.0	4.5	70.8	16.1	0.50	1.76	2.21	3.25	5.38
2	1.0	880	40.1	4.7	70.9	16.1	0.44	1.59	2.15	3.18	5.57
2	1.0	870	37.8	5.0	71.1	16.2	0.38	1.41	2.10	3.21	5.60
2	1.0	860	35.6	5.4	71.2	16.3	0.33	1.24	2.04	3.28	5.59
2	1.0	850	33.6	5.7	71.4	16.4	0.29	1.08	1.98	3.36	5.57
2	1.0	840	31.8	6.1	71.5	16.5	0.25	0.93	1.92	3.43	5.54
2	1.0	830	29.9	6.4	71.6	16.5	0.21	0.81	1.88	3.49	5.53

Table 4.6 – Continued from previous page

			Tabl	e 4.6 – C	continue	ed from p	previous	page			
H_2O^i	Р	Т	melt	H_2O^m	SiO_2	Al_2O_3	MgO	${\rm FeO}_t$	CaO	Na ₂ O	K_2O
2	1.0	820	28.2	6.8	71.7	16.6	0.18	0.70	1.84	3.54	5.52
2	1.0	810	26.6	7.2	71.8	16.6	0.15	0.60	1.81	3.58	5.51
2	1.0	800	25.1	7.6	71.8	16.6	0.12	0.51	1.78	3.64	5.50
2	1.0	790	23.8	8.0	71.9	16.7	0.10	0.42	1.75	3.69	5.49
2	1.0	780	22.6	8.4	71.9	16.7	0.08	0.34	1.73	3.74	5.48
2	1.0	770	21.5	8.9	72.0	16.7	0.07	0.28	1.71	3.79	5.47
2	1.0	760	20.6	9.3	72.0	16.7	0.05	0.22	1.69	3.85	5.46
2	1.0	750	19.7	9.8	72.1	16.7	0.04	0.17	1.67	3.90	5.44
2	1.0	740	18.9	10.3	72.1	16.7	0.03	0.13	1.65	3.95	5.43
2	1.0	730	18.2	10.8	72.1	16.7	0.03	0.10	1.63	4.00	5.42
2	1.0	720	17.6	11.3	72.1	16.7	0.02	0.08	1.61	4.05	5.40
2	1.0	710	16.9	11.9	72.1	16.8	0.02	0.06	1.59	4.10	5.39
2	1.0	700	15.8	12.5	72.2	16.6	0.01	0.05	1.54	4.27	5.31
2	1.5	1200	95.8	2.1	69.1	16.8	1.38	2.11	3.87	4.04	2.66
2	1.5	1190	95.6	2.1	69.1	16.9	1.32	2.09	3.88	4.05	2.67
2	1.5	1180	95.4	2.2	69.2	16.9	1.27	2.06	3.89	4.06	2.67
2	1.5	1170	95.3	2.2	69.2	16.9	1.22	2.04	3.89	4.07	2.68
2	1.5	1160	95.1	2.2	69.2	16.9	1.18	2.02	3.90	4.08	2.68
2	1.5	1150	95.0	2.2	69.3	16.9	1.13	1.99	3.90	4.08	2.69
2	1.5	1140	94.5	2.2	69.4	16.9	1.08	1.95	3.86	4.11	2.70
2	1.5	1130	92.8	2.2	69.6	16.7	1.04	1.90	3.75	4.19	2.76
2	1.5	1120	90.6	2.3	69.6	16.7	1.01	1.86	3.65	4.30	2.83
2	1.5	1110	89.4	2.3	69.6	16.8	0.95	1.80	3.63	4.36	2.87
2	1.5	1100	88.3	2.3	69.5	16.9	0.89	1.74	3.61	4.42	2.91
2	1.5	1090	87.1	2.4	69.4	17.1	0.83	1.67	3.58	4.49	2.95
2	1.5	1080	84.0	2.5	69.4	17.1	0.79	1.63	3.51	4.51	3.05
2	1.5	1070	79.2	2.6	69.5	17.0	0.76	1.62	3.42	4.48	3.19
2	1.5	1060	74.8	2.8	69.6	17.0	0.73	1.59	3.34	4.44	3.34
2	1.5	1050	70.7	3.0	69.7	16.9	0.69	1.55	3.27	4.40	3.48
2	1.5	1040	66.9	3.2	69.8	16.9	0.65	1.50	3.19	4.34	3.63
2	1.5	1030	63.5	3.4	69.9	16.9	0.61	1.43	3.12	4.29	3.77
2	1.5	1020	60.3	3.6	69.9	16.9	0.56	1.35	3.06	4.24	3.92
2	1.5	1010	57.4	3.8	70.0	16.9	0.52	1.26	2.99	4.18	4.06
2	1.5	1000	54.7	4.0	70.1	17.0	0.47	1.16	2.94	4.13	4.21
2	1.5	990	52.2	4.2	70.2	17.0	0.43	1.06	2.88	4.07	4.35
2	1.5	980	49.9	4.4	70.3	17.0	0.39	0.96	2.82	4.02	4.50

Table 4.6 – Continued from previous page

 H_2O^i $\mathbf{2}$ $\mathbf{2}$ $\mathbf{2}$ $\mathbf{2}$ 2 $\mathbf{2}$ $\mathbf{2}$ $\mathbf{2}$ $\mathbf{2}$ $\mathbf{2}$ 2 $\mathbf{2}$ $\mathbf{2}$ $\mathbf{2}$ $\mathbf{2}$ $\mathbf{2}$ 2 $\mathbf{2}$ $\mathbf{2}$

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2.0

2.0

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2.0

1200

1190

1180

1170

1160

1150

1140

1130

89.6

88.6

87.5

86.5

85.4

84.2

83.0

81.0

2.3

2.3

2.4

2.4

2.4

2.5

2.5

2.6

69.5

69.5

69.4

69.3

69.3

69.2

69.1

69.1

16.8

16.9

17.0

17.1

17.3

17.4

17.6

17.7

0.91

0.86

0.80

0.75

0.70

0.64

0.59

0.53

1.89

1.84

1.77

1.70

1.63

1.55

1.47

1.39

3.65

3.63

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Table 4.6 - Continued from previous pagePTmelt H_2O^m SiO_2 Al_2O_3 MgO FeO_t CaO Na_2O K_2O												
Р	Т	melt	H_2O^m	SiO_2	Al_2O_3	MgO	${\rm FeO}_t$	CaO	Na_2O	K_2O		
1.5	970	47.7	4.7	70.4	17.0	0.35	0.86	2.77	3.96	4.64		
1.5	960	45.8	4.9	70.5	17.1	0.31	0.76	2.72	3.90	4.78		
1.5	950	44.0	5.1	70.5	17.1	0.27	0.67	2.67	3.84	4.92		
1.5	940	41.8	5.3	70.5	17.1	0.25	0.62	2.65	3.75	5.09		
1.5	930	39.6	5.6	70.5	17.2	0.22	0.57	2.62	3.68	5.20		
1.5	920	37.5	5.9	70.5	17.3	0.19	0.52	2.58	3.68	5.24		
1.5	910	35.6	6.2	70.4	17.5	0.17	0.47	2.54	3.68	5.26		
1.5	900	33.8	6.5	70.4	17.6	0.15	0.42	2.49	3.70	5.28		
1.5	890	32.2	6.8	70.3	17.7	0.13	0.38	2.45	3.71	5.29		
1.5	880	30.7	7.1	70.3	17.8	0.11	0.33	2.41	3.74	5.30		
1.5	870	29.2	7.5	70.2	18.0	0.10	0.30	2.36	3.76	5.31		
1.5	860	27.9	7.8	70.1	18.1	0.08	0.26	2.32	3.79	5.31		
1.5	850	26.6	8.2	70.0	18.3	0.07	0.23	2.27	3.82	5.31		
1.5	840	25.5	8.6	70.0	18.4	0.06	0.20	2.23	3.85	5.31		
1.5	830	24.4	8.9	69.9	18.5	0.05	0.17	2.19	3.88	5.31		
1.5	820	22.6	9.4	69.9	18.5	0.05	0.16	2.12	4.01	5.24		
1.5	810	20.1	10.0	70.1	18.2	0.04	0.16	2.04	4.29	5.09		
1.5	800	18.0	10.5	70.3	18.0	0.04	0.15	1.96	4.55	4.95		
1.5	790	16.4	11.0	70.5	17.8	0.04	0.14	1.90	4.76	4.85		
1.5	780	15.1	11.6	70.6	17.6	0.03	0.13	1.85	4.95	4.77		
1.5	770	14.0	12.1	70.8	17.5	0.03	0.11	1.80	5.13	4.68		
1.5	760	11.9	12.7	70.9	17.3	0.03	0.11	1.68	5.40	4.54		
1.5	750	11.7	12.7	70.9	17.0	0.02	0.07	1.71	4.78	5.53		
1.5	740	10.2	13.4	71.1	16.8	0.02	0.09	1.51	5.17	5.25		
1.5	730	9.3	14.1	71.2	16.8	0.02	0.08	1.40	5.49	5.00		
1.5	720	8.4	14.8	71.3	16.7	0.02	0.08	1.30	5.78	4.76		
1.5	710	7.6	15.6	71.4	16.7	0.02	0.07	1.21	6.05	4.54		
1.5	700	6.8	16.3	71.5	16.7	0.01	0.07	1.14	6.27	4.36		

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			Tabl	e 4.6 – C	Continue	ed from p	previous	page			
H_2O^i	Р	Т	melt	H_2O^m	SiO_2	Al_2O_3	MgO	FeO_t	CaO	Na ₂ O	K_2O
2	2.0	1120	76.0	2.8	69.1	17.8	0.49	1.33	3.39	4.63	3.25
2	2.0	1110	71.6	3.0	69.2	17.8	0.45	1.26	3.37	4.58	3.34
2	2.0	1100	67.5	3.1	69.2	17.9	0.41	1.17	3.34	4.52	3.44
2	2.0	1090	63.9	3.3	69.2	18.0	0.37	1.08	3.32	4.46	3.55
2	2.0	1080	60.6	3.6	69.3	18.0	0.34	0.99	3.28	4.40	3.66
2	2.0	1070	57.6	3.8	69.3	18.1	0.30	0.90	3.25	4.33	3.78
2	2.0	1060	54.9	4.0	69.4	18.2	0.27	0.80	3.22	4.26	3.91
2	2.0	1050	52.4	4.2	69.4	18.2	0.24	0.71	3.19	4.18	4.04
2	2.0	1040	50.1	4.4	69.4	18.3	0.21	0.63	3.16	4.11	4.18
2	2.0	1030	48.1	4.6	69.4	18.4	0.19	0.56	3.14	4.02	4.33
2	2.0	1020	46.1	4.8	69.4	18.5	0.16	0.49	3.11	3.93	4.48
2	2.0	1010	44.4	5.1	69.3	18.6	0.14	0.42	3.09	3.84	4.63
2	2.0	1000	42.7	5.3	69.3	18.6	0.12	0.37	3.07	3.74	4.79
2	2.0	990	41.2	5.5	69.2	18.7	0.11	0.31	3.05	3.64	4.96
2	2.0	980	39.8	5.8	69.1	18.9	0.09	0.27	3.03	3.54	5.14
2	2.0	970	38.5	6.0	69.0	19.0	0.08	0.23	3.01	3.43	5.31
2	2.0	960	37.3	6.2	68.9	19.1	0.07	0.19	2.99	3.35	5.45
2	2.0	950	36.0	6.5	68.8	19.2	0.06	0.16	2.96	3.35	5.49
2	2.0	940	34.8	6.8	68.6	19.4	0.05	0.14	2.93	3.34	5.53
2	2.0	930	33.6	7.1	68.5	19.5	0.04	0.11	2.91	3.33	5.57
2	2.0	920	32.6	7.4	68.3	19.7	0.04	0.10	2.89	3.32	5.61
2	2.0	900	27.1	8.2	68.6	19.5	0.04	0.09	2.73	3.80	5.27
2	2.0	890	22.7	8.8	69.0	19.1	0.04	0.11	2.52	4.40	4.79
2	2.0	880	18.9	9.5	69.4	18.9	0.05	0.14	2.27	5.15	4.16
2	2.0	870	16.4	10.1	69.6	18.8	0.05	0.15	2.02	6.07	3.30
2	2.0	860	14.7	10.6	69.8	18.7	0.05	0.14	1.83	6.75	2.68
2	2.0	850	13.5	11.1	69.9	18.7	0.04	0.14	1.69	7.25	2.23
2	2.0	840	12.5	11.6	70.0	18.7	0.04	0.13	1.58	7.63	1.89
2	2.0	830	11.6	12.2	70.0	18.8	0.04	0.12	1.50	7.93	1.62
2	2.0	820	10.9	12.7	70.1	18.8	0.03	0.10	1.43	8.17	1.41
2	2.0	810	10.1	13.2	70.1	18.8	0.03	0.09	1.37	8.36	1.24
2	2.0	800	9.3	13.7	70.1	18.8	0.02	0.08	1.32	8.53	1.11
2	2.0	790	8.7	14.5	70.3	18.7	0.02	0.08	1.26	8.61	1.05
2	2.0	780	8.2	15.5	70.4	18.6	0.02	0.08	1.22	8.60	1.05
2	2.0	770	7.8	16.5	70.6	18.5	0.02	0.07	1.18	8.60	1.04
2	2.0	760	7.4	17.6	70.7	18.4	0.02	0.07	1.15	8.58	1.04

Table 4.6 – Continued from previous page

			Tabl	e 4.6 – C	Continu	ed from p	previous	page			
H_2O^i	Р	Т	melt	H_2O^m	SiO_2	Al_2O_3	MgO	${\rm FeO}_t$	CaO	Na_2O	K_2O
2	2.0	750	7.1	18.8	70.9	18.3	0.02	0.07	1.12	8.56	1.04
2	2.0	740	6.7	20.0	71.0	18.2	0.02	0.07	1.09	8.53	1.04
2	2.0	730	6.4	21.3	71.2	18.1	0.02	0.07	1.06	8.50	1.04
2	2.0	720	6.1	22.7	71.4	18.0	0.02	0.06	1.04	8.46	1.05
2	2.0	710	5.9	24.2	71.6	17.9	0.02	0.06	1.01	8.42	1.05
5	0.5	1100	98.0	5.0	68.8	16.7	2.05	2.13	3.81	3.96	2.60
5	0.5	1090	97.7	5.0	68.8	16.7	1.97	2.11	3.82	3.97	2.61
5	0.5	1080	97.5	5.0	68.9	16.7	1.89	2.10	3.82	3.98	2.62
5	0.5	1070	97.3	5.0	68.9	16.8	1.81	2.08	3.83	3.99	2.62
5	0.5	1060	97.1	5.0	68.9	16.8	1.74	2.06	3.84	4.00	2.63
5	0.5	1050	96.9	5.0	69.0	16.8	1.67	2.04	3.85	4.01	2.64
5	0.5	1040	96.7	5.1	69.0	16.9	1.59	2.02	3.86	4.02	2.64
5	0.5	1030	96.5	5.1	69.0	16.9	1.53	2.00	3.86	4.03	2.65
5	0.5	1020	96.3	5.1	69.1	16.9	1.46	1.97	3.87	4.04	2.66
5	0.5	1010	96.1	5.1	69.1	17.0	1.39	1.94	3.88	4.05	2.66
5	0.5	1000	95.9	5.1	69.2	17.0	1.33	1.91	3.89	4.06	2.67
5	0.5	990	95.7	5.1	69.2	17.0	1.27	1.88	3.90	4.07	2.68
5	0.5	980	95.6	5.1	69.2	17.0	1.21	1.85	3.90	4.08	2.68
5	0.5	970	95.4	5.1	69.3	17.1	1.15	1.81	3.91	4.09	2.69
5	0.5	960	95.2	5.2	69.3	17.1	1.09	1.77	3.92	4.10	2.70
5	0.5	950	95.0	5.2	69.4	17.1	1.03	1.72	3.92	4.11	2.70
5	0.5	940	94.1	5.2	69.7	17.0	0.98	1.72	3.77	4.10	2.73
5	0.5	930	93.0	5.2	70.0	16.9	0.92	1.72	3.60	4.09	2.75
5	0.5	920	92.0	5.2	70.4	16.7	0.86	1.71	3.42	4.08	2.78
5	0.5	910	90.9	5.2	70.9	16.5	0.81	1.70	3.26	4.07	2.81
5	0.5	900	90.2	5.2	71.1	16.4	0.73	1.63	3.17	4.07	2.83
5	0.5	890	89.5	5.3	71.4	16.4	0.65	1.53	3.10	4.08	2.86
5	0.5	880	88.2	5.3	71.8	16.2	0.59	1.45	2.95	4.09	2.90
5	0.5	870	86.9	5.4	72.2	16.0	0.54	1.36	2.81	4.11	2.95
5	0.5	860	85.6	5.5	72.6	15.8	0.48	1.27	2.67	4.11	3.01
5	0.5	850	84.3	5.6	73.0	15.7	0.43	1.17	2.54	4.11	3.06
5	0.5	840	83.1	5.7	73.4	15.5	0.39	1.07	2.41	4.11	3.11
5	0.5	830	81.8	5.8	73.8	15.3	0.34	0.97	2.29	4.10	3.17
5	0.5	820	80.6	5.9	74.2	15.1	0.30	0.87	2.18	4.08	3.22
5	0.5	810	79.3	6.0	74.6	15.0	0.26	0.77	2.07	4.06	3.28
5	0.5	800	78.1	6.1	75.0	14.8	0.23	0.68	1.97	4.02	3.34

Table 4.6 – Continued from previous page

			Tabl	e 4.6 – C	Continue	ed from p	previous	page			
H_2O^i	Р	Т	melt	H_2O^m	SiO_2	Al_2O_3	MgO	FeO_t	CaO	Na ₂ O	K_2O
5	0.5	790	75.8	6.3	75.0	14.8	0.20	0.60	1.87	4.05	3.45
5	0.5	780	73.4	6.5	75.1	14.8	0.17	0.51	1.77	4.08	3.58
5	0.5	770	71.2	6.7	75.1	14.9	0.15	0.44	1.67	4.10	3.70
5	0.5	760	69.1	6.9	75.1	14.9	0.12	0.37	1.58	4.11	3.83
5	0.5	740	62.4	7.7	75.3	14.9	0.09	0.29	1.48	4.31	3.68
5	0.5	730	59.6	8.1	75.4	14.9	0.08	0.24	1.43	4.40	3.62
5	0.5	720	57.1	8.5	75.5	14.8	0.06	0.20	1.39	4.48	3.57
5	0.5	710	54.7	8.9	75.6	14.8	0.05	0.16	1.35	4.55	3.51
5	0.5	700	52.6	9.3	75.7	14.8	0.04	0.13	1.31	4.61	3.47
5	1.0	1100	96.4	5.1	69.1	16.9	1.48	2.02	3.87	4.03	2.65
5	1.0	1090	96.3	5.1	69.1	16.9	1.42	2.00	3.87	4.04	2.66
5	1.0	1070	95.9	5.1	69.2	17.0	1.30	1.96	3.89	4.06	2.67
5	1.0	1050	95.6	5.1	69.2	17.0	1.19	1.90	3.90	4.08	2.68
5	1.0	1030	95.2	5.1	69.3	17.1	1.09	1.84	3.91	4.10	2.69
5	1.0	1010	94.9	5.2	69.4	17.1	0.98	1.77	3.92	4.11	2.71
5	1.0	990	94.6	5.2	69.4	17.2	0.89	1.69	3.93	4.13	2.72
5	1.0	980	93.9	5.2	69.7	17.1	0.84	1.69	3.82	4.12	2.74
5	1.0	960	92.0	5.2	70.4	16.8	0.75	1.69	3.50	4.09	2.78
5	1.0	940	90.0	5.3	71.2	16.4	0.66	1.67	3.18	4.05	2.84
5	1.0	930	89.3	5.3	71.4	16.3	0.60	1.61	3.10	4.05	2.86
5	1.0	920	88.7	5.3	71.7	16.3	0.54	1.52	3.04	4.05	2.88
5	1.0	910	86.9	5.4	71.6	16.5	0.48	1.43	3.00	4.12	2.95
5	1.0	900	85.1	5.5	71.5	16.6	0.42	1.33	2.95	4.18	3.01
5	1.0	890	82.9	5.7	71.5	16.7	0.38	1.24	2.86	4.24	3.11
5	1.0	880	80.0	5.9	71.6	16.7	0.34	1.16	2.72	4.29	3.23
5	1.0	860	74.7	6.3	71.7	16.7	0.27	0.97	2.47	4.36	3.48
5	1.0	840	70.0	6.8	71.9	16.7	0.21	0.78	2.25	4.39	3.74
5	1.0	820	65.8	7.3	72.0	16.8	0.16	0.60	2.05	4.40	4.01
5	1.0	800	62.0	7.8	72.1	16.8	0.12	0.44	1.88	4.38	4.28
5	1.0	780	58.5	8.3	72.1	16.9	0.08	0.31	1.73	4.33	4.57
5	1.0	770	56.4	8.7	72.1	16.9	0.07	0.26	1.68	4.35	4.62
5	1.0	760	54.2	9.0	72.1	16.9	0.06	0.22	1.66	4.39	4.60
5	1.0	750	52.2	9.4	72.1	17.0	0.05	0.17	1.64	4.43	4.59
5	1.0	740	50.3	9.8	72.1	17.0	0.04	0.14	1.62	4.47	4.60
5	1.0	730	48.5	10.3	72.1	17.0	0.03	0.11	1.60	4.49	4.61
5	1.0	720	46.9	10.7	72.1	17.0	0.02	0.08	1.58	4.51	4.64

Table 4.6 – Continued from previous page

			Tabl	e 4.6 – C	Continu	ed from p	previous	page			
H_2O^i	Р	Т	melt	H_2O^m	SiO_2	Al_2O_3	MgO	${\rm FeO}_t$	CaO	Na ₂ O	K_2O
5	1.0	710	45.5	11.1	72.1	17.1	0.02	0.07	1.56	4.52	4.67
5	1.0	700	43.2	11.5	72.3	16.8	0.01	0.06	1.46	4.68	4.72
5	1.5	1100	95.4	5.1	69.3	17.0	1.12	1.92	3.90	4.09	2.69
5	1.5	1080	95.1	5.2	69.3	17.1	1.03	1.87	3.91	4.10	2.70
5	1.5	1070	94.7	5.2	69.5	17.0	0.97	1.80	3.86	4.13	2.71
5	1.5	1060	93.7	5.2	69.9	16.8	0.91	1.72	3.71	4.18	2.75
5	1.5	1040	91.9	5.4	70.7	16.5	0.78	1.54	3.41	4.28	2.82
5	1.5	1030	91.1	5.4	71.1	16.3	0.72	1.44	3.27	4.33	2.85
5	1.5	1010	90.0	5.5	71.5	16.3	0.58	1.23	3.13	4.39	2.89
5	1.5	1000	88.8	5.6	71.4	16.4	0.52	1.13	3.07	4.46	2.94
5	1.5	990	87.5	5.7	71.4	16.6	0.47	1.03	3.02	4.54	3.00
5	1.5	970	85.1	5.9	71.3	16.9	0.37	0.82	2.89	4.70	3.10
5	1.5	950	82.8	6.1	71.1	17.1	0.28	0.62	2.76	4.86	3.21
5	1.5	940	81.2	6.2	71.0	17.3	0.25	0.58	2.73	4.89	3.27
5	1.5	930	79.7	6.2	70.8	17.5	0.22	0.53	2.68	4.92	3.34
5	1.5	910	76.8	6.4	70.5	17.8	0.16	0.43	2.60	4.98	3.47
5	1.5	900	73.9	6.7	70.5	17.8	0.15	0.40	2.53	4.94	3.60
5	1.5	890	71.3	6.9	70.5	17.9	0.13	0.38	2.46	4.89	3.74
5	1.5	870	66.4	7.5	70.5	18.0	0.10	0.32	2.34	4.79	4.01
5	1.5	850	62.1	8.0	70.4	18.1	0.08	0.26	2.23	4.68	4.29
5	1.5	830	58.2	8.6	70.3	18.2	0.06	0.20	2.13	4.56	4.58
5	1.5	810	54.8	9.1	70.1	18.3	0.04	0.16	2.05	4.42	4.89
5	1.5	800	51.2	9.6	70.3	18.1	0.04	0.14	1.98	4.68	4.72
5	1.5	790	48.3	10.1	70.5	17.9	0.03	0.13	1.93	4.92	4.57
5	1.5	780	45.8	10.5	70.6	17.8	0.03	0.12	1.88	5.15	4.43
5	1.5	770	43.4	11.0	70.8	17.6	0.03	0.11	1.78	5.41	4.27
5	1.5	760	41.2		70.9		0.03	0.11	1.65	5.71	4.11
5	1.5	750	39.0	12.0	71.1	17.4	0.03	0.11	1.52	6.05	3.86
5	1.5	735	35.9	12.8	71.2	17.3	0.02	0.10	1.35	6.67	3.27
5	1.5	720	33.4	13.6	71.4	17.3	0.02	0.10	1.20	7.18	2.80
5	1.5	700	30.8	14.8	71.5	17.3	0.02	0.08	1.02	7.72	2.31
5	2.0	1200	95.0	5.2	69.6	16.4	1.35	2.11	3.67	4.11	2.70
5	2.0	1180	94.2	5.2	69.9	16.4	1.18	2.02	3.62	4.15	2.73
5	2.0	1160	93.4	5.3	70.2	16.4	1.03	1.91	3.55	4.19	2.76
5	2.0	1140	92.5	5.3	70.5	16.4	0.88	1.78	3.46	4.25	2.79
5	2.0	1120	91.6	5.4	70.8	16.3	0.74	1.61	3.35	4.30	2.83

Table 4.6 – Continued from previous page

			Tabl	e 4.6 – C	Continue	ed from p	previous	page			
H_2O^i	Р	Т	melt	H_2O^m	SiO_2	Al_2O_3	MgO	FeO_t	CaO	Na ₂ O	K_2O
5	2.0	1100	90.6	5.5	71.2	16.3	0.61	1.42	3.23	4.36	2.87
5	2.0	1090	90.1	5.5	71.4	16.3	0.55	1.32	3.16	4.39	2.89
5	2.0	1080	88.9	5.6	71.3	16.4	0.50	1.23	3.11	4.47	2.94
5	2.0	1070	87.7	5.7	71.3	16.6	0.45	1.13	3.06	4.54	2.99
5	2.0	1060	86.5	5.8	71.2	16.7	0.41	1.03	3.00	4.61	3.04
5	2.0	1045	84.8	5.9	71.1	17.0	0.34	0.88	2.91	4.71	3.11
5	2.0	1030	83.1	6.0	70.9	17.2	0.28	0.74	2.82	4.80	3.20
5	2.0	1020	81.9	6.1	70.8	17.4	0.25	0.66	2.78	4.85	3.25
5	2.0	1000	79.8	6.3	70.5	17.8	0.19	0.50	2.69	4.94	3.36
5	2.0	980	77.7	6.5	70.2	18.2	0.14	0.38	2.61	5.01	3.47
5	2.0	960	75.6	6.7	69.8	18.6	0.11	0.28	2.55	5.06	3.59
5	2.0	940	73.6	7.0	69.5	19.0	0.08	0.20	2.50	5.09	3.72
5	2.0	930	72.1	7.1	69.3	19.1	0.07	0.17	2.48	5.07	3.80
5	2.0	915	68.8	7.5	69.2	19.3	0.05	0.13	2.45	4.97	3.97
5	2.0	900	65.8	7.9	69.0	19.4	0.04	0.11	2.42	4.86	4.15
5	2.0	885	58.7	8.6	69.2	19.2	0.04	0.11	2.26	5.52	3.59
5	2.0	870	52.2	9.2	69.5	19.1	0.04	0.11	2.04	6.40	2.80
5	2.0	860	48.9	9.8	69.7	19.0	0.04	0.11	1.94	6.73	2.51
5	2.0	850	46.1	10.3	69.8	18.9	0.04	0.11	1.84	7.01	2.25
5	2.0	840	43.7	10.8	70.0	18.9	0.04	0.10	1.75	7.25	2.04
5	2.0	830	41.6	11.4	70.1	18.8	0.04	0.10	1.68	7.45	1.86
5	2.0	820	39.7	11.9	70.2	18.8	0.03	0.09	1.61	7.61	1.71
5	2.0	810	37.9	12.5	70.3	18.7	0.03	0.09	1.55	7.75	1.59
5	2.0	800	36.3	13.1	70.4	18.7	0.03	0.08	1.49	7.86	1.49
5	2.0	790	34.8	13.7	70.5	18.6	0.03	0.08	1.43	7.95	1.41
5	2.0	780	33.4	14.4	70.7	18.5	0.03	0.08	1.37	8.03	1.35
5	2.0	770	32.0	15.1	70.8	18.4	0.03	0.08	1.31	8.09	1.29
5	2.0	760	30.8	15.8	70.9	18.3	0.02	0.07	1.26	8.13	1.25
5	2.0	750	29.6	16.6	71.1	18.2	0.02	0.07	1.21	8.16	1.22
5	2.0	740	28.4	17.4	71.2	18.1	0.02	0.07	1.17	8.18	1.19
5	2.0	720	26.4	19.1	71.6	17.9	0.02	0.07	1.10	8.18	1.16
5	2.0	710	25.4	20.1	71.7	17.8	0.02	0.06	1.07	8.17	1.16
5	2.0	700	24.5	21.0	71.9	17.7	0.02	0.06	1.04	8.15	1.16
10	0.5	1100	96.5	10.4	68.8	16.6	2.33	2.04	3.78	3.93	2.58
10	0.5	1095	96.5	10.4	68.8	16.6	2.33	2.04	3.78	3.93	2.58
10	0.5	1085	96.4	10.4	68.8	16.6	2.33	2.04	3.78	3.93	2.58

Table 4.6 – Continued from previous page

			Tabl	e 4.6 – C	Continu	ed from p	previous	page			
H_2O^i	Р	Т	melt	H_2O^m	SiO_2	$\mathrm{Al}_2\mathrm{O}_3$	MgO	FeO_t	CaO	Na ₂ O	K_2O
10	0.5	1075	96.3	10.3	68.8	16.6	2.33	2.04	3.78	3.93	2.58
10	0.5	1065	95.9	10.3	68.8	16.6	2.22	2.03	3.79	3.94	2.59
10	0.5	1040	95.0	10.2	68.9	16.7	1.97	1.99	3.82	3.97	2.61
10	0.5	1015	94.1	10.2	69.0	16.8	1.74	1.94	3.84	4.00	2.63
10	0.5	990	93.4	10.1	69.1	16.9	1.54	1.88	3.87	4.03	2.65
10	0.5	965	92.7	10.1	69.2	17.0	1.34	1.80	3.89	4.06	2.67
10	0.5	940	92.0	10.1	69.3	17.1	1.17	1.70	3.91	4.09	2.69
10	0.5	930	91.4	10.1	69.5	17.1	1.10	1.68	3.84	4.09	2.70
10	0.5	915	89.7	10.1	70.0	16.9	1.01	1.69	3.54	4.09	2.74
10	0.5	900	88.1	10.1	70.6	16.7	0.91	1.67	3.28	4.08	2.78
10	0.5	885	87.1	10.1	70.9	16.7	0.77	1.55	3.18	4.10	2.82
10	0.5	870	86.1	10.1	71.3	16.6	0.64	1.41	3.08	4.12	2.85
10	0.5	855	85.1	10.1	71.7	16.6	0.53	1.25	2.97	4.14	2.88
10	0.5	840	84.2	10.2	72.1	16.5	0.43	1.09	2.86	4.16	2.91
10	0.5	825	83.3	10.2	72.5	16.4	0.34	0.92	2.75	4.18	2.95
10	0.5	810	82.5	10.2	72.8	16.3	0.27	0.75	2.64	4.19	2.98
10	0.5	795	81.7	10.3	73.2	16.2	0.21	0.60	2.53	4.20	3.01
10	0.5	780	81.0	10.3	73.6	16.1	0.15	0.46	2.42	4.21	3.04
10	0.5	765	80.4	10.4	73.9	16.0	0.11	0.34	2.31	4.22	3.06
10	0.5	750	79.9	10.4	74.3	15.9	0.08	0.25	2.21	4.23	3.09
10	0.5	745	79.6	10.4	74.4	15.8	0.07	0.23	2.16	4.23	3.10
10	0.5	730	78.0	10.5	74.9	15.5	0.06	0.17	1.95	4.23	3.17
10	0.5	715	76.2	10.5	75.4	15.2	0.04	0.13	1.76	4.20	3.24
10	0.5	700	74.3	10.6	76.0	14.8	0.03	0.10	1.58	4.15	3.33
10	1.0	1100	98.1	11.5	68.9	16.7	2.02	2.01	3.81	3.97	2.61
10	1.0	1075	97.7	11.6	69.0	16.8	1.81	1.98	3.84	3.99	2.63
10	1.0	1050	97.2	11.6	69.1	16.9	1.61	1.93	3.86	4.02	2.64
10	1.0	1025	96.8	11.7	69.2	17.0	1.43	1.88	3.87	4.04	2.66
10	1.0	1000	96.4	11.8	69.2	17.1	1.26	1.81	3.89	4.07	2.68
10	1.0	975	96.0	11.8	69.3	17.1	1.11	1.72	3.91	4.09	2.69
10	1.0	950	95.6	11.9	69.4	17.2	0.96	1.62	3.93	4.12	2.71
10	1.0	945	94.6	12.0	69.8	17.1	0.94	1.67	3.67	4.10	2.73
10	1.0	930	93.4	12.1	70.3	16.9	0.87	1.69	3.41	4.09	2.77
10	1.0	920	92.5	12.2	70.7	16.7	0.83	1.69	3.23	4.08	2.79
10	1.0	895	91.4	12.4	71.2	16.7	0.64	1.51	3.08	4.11	2.84
10	1.0	870	90.2	12.6	71.7	16.6	0.48	1.28	2.92	4.13	2.89

Table 4.6 – Continued from previous page

			Tabl	e 4.6 – C	Continu	ed from p	previous	page			
H_2O^i	Р	Т	melt	H_2O^m	SiO_2	Al_2O_3	MgO	FeO_t	CaO	Na ₂ O	K_2O
10	1.0	845	89.0	12.8	72.3	16.5	0.34	1.02	2.75	4.15	2.94
10	1.0	820	87.8	13.0	73.0	16.3	0.23	0.75	2.58	4.17	2.98
10	1.0	795	86.8	13.2	73.6	16.2	0.15	0.51	2.40	4.19	3.03
10	1.0	770	85.9	13.4	74.1	16.0	0.09	0.32	2.24	4.19	3.07
10	1.0	760	85.1	13.5	74.2	16.0	0.07	0.26	2.18	4.22	3.11
10	1.0	750	83.7	13.8	74.0	16.1	0.06	0.21	2.12	4.29	3.19
10	1.0	745	83.0	14.0	73.9	16.2	0.05	0.19	2.09	4.32	3.22
10	1.0	730	81.0	14.5	73.6	16.4	0.04	0.13	2.01	4.42	3.33
10	1.0	715	79.1	15.0	73.3	16.7	0.02	0.09	1.94	4.52	3.44
10	1.0	700	77.4	15.4	73.0	16.9	0.02	0.06	1.86	4.62	3.55
10	1.5	1100	97.1	11.6	69.1	16.9	1.56	1.95	3.86	4.02	2.65
10	1.5	1085	96.9	11.7	69.1	16.9	1.46	1.92	3.87	4.04	2.66
10	1.5	1070	96.7	11.7	69.2	17.0	1.37	1.89	3.88	4.05	2.66
10	1.5	1055	96.4	11.8	69.2	17.0	1.27	1.86	3.89	4.06	2.67
10	1.5	1040	96.2	11.8	69.3	17.1	1.18	1.82	3.90	4.08	2.68
10	1.5	1025	96.0	11.8	69.3	17.1	1.10	1.78	3.90	4.09	2.69
10	1.5	1010	95.8	11.9	69.4	17.2	1.02	1.73	3.91	4.11	2.70
10	1.5	990	95.3	12.0	69.5	17.3	0.92	1.66	3.81	4.13	2.72
10	1.5	985	95.1	12.0	69.6	17.3	0.89	1.63	3.76	4.14	2.73
10	1.5	975	94.3	12.1	70.0	17.1	0.82	1.54	3.63	4.16	2.76
10	1.5	970	93.7	12.2	70.2	16.9	0.80	1.55	3.54	4.15	2.77
10	1.5	960	92.8	12.3	70.7	16.8	0.75	1.49	3.36	4.16	2.80
10	1.5	950	91.9	12.4	71.1	16.6	0.70	1.44	3.18	4.16	2.83
10	1.5	940	91.4	12.5	71.3	16.6	0.62	1.33	3.11	4.19	2.86
10	1.5	930	90.9	12.6	71.5	16.6	0.55	1.23	3.04	4.21	2.88
10	1.5	920	90.4	12.7	71.8	16.5	0.48	1.11	2.96	4.24	2.90
10	1.5	905	89.7	12.9	72.2	16.5	0.39	0.93	2.84	4.28	2.94
10	1.5	890	89.0	13.0	72.5	16.4	0.31	0.77	2.72	4.32	2.97
10	1.5	875	88.4	13.2	72.9	16.3	0.24	0.62	2.60	4.34	3.01
10	1.5	860	87.8	13.3	73.2	16.3	0.19	0.49	2.49	4.36	3.03
10	1.5	850	87.3	13.4	73.3	16.3	0.16	0.42	2.43	4.37	3.06
10	1.5	845	86.6	13.5	73.2	16.4	0.14	0.39	2.40	4.40	3.09
10	1.5	830	84.6	13.9	72.9	16.6	0.11	0.32	2.34	4.49	3.19
10	1.5	815	82.7	14.4	72.6	16.9	0.09	0.25	2.27	4.58	3.29
10	1.5	800	80.8	14.8	72.3	17.2	0.07	0.20	2.21	4.65	3.39
10	1.5	785	79.0	15.3	72.0	17.4	0.05	0.15	2.16	4.73	3.50

Table 4.6 – Continued from previous page

			Tabl	e 4.6 – C	Continu	ed from p	previous	page			
H_2O^i	Р	Т	melt	H_2O^m	SiO_2	Al_2O_3	MgO	${\rm FeO}_t$	CaO	Na ₂ O	K_2O
10	1.5	770	77.3	15.7	71.7	17.7	0.04	0.11	2.10	4.79	3.61
10	1.5	760	76.1	16.1	71.5	17.8	0.03	0.10	2.04	4.84	3.68
10	1.5	750	73.4	16.8	71.6	17.7	0.03	0.10	1.88	5.03	3.64
10	1.5	740	70.4	17.6	71.9	17.5	0.03	0.10	1.74	5.29	3.51
10	1.5	730	67.8	18.5	72.1	17.3	0.03	0.10	1.62	5.52	3.39
10	1.5	720	65.4	19.3	72.3	17.1	0.03	0.10	1.51	5.76	3.26
10	1.5	710	63.2	20.2	72.4	16.9	0.02	0.10	1.40	5.98	3.14
10	1.5	700	61.2	21.1	72.6	16.8	0.02	0.09	1.31	6.20	3.01
10	2.0	1200	98.1	11.5	68.8	16.7	1.97	2.12	3.81	3.97	2.61
10	2.0	1185	97.8	11.5	68.9	16.7	1.85	2.10	3.83	3.98	2.62
10	2.0	1160	97.4	11.6	69.0	16.8	1.66	2.05	3.84	4.01	2.64
10	2.0	1135	97.0	11.7	69.1	16.9	1.49	2.00	3.86	4.03	2.65
10	2.0	1110	96.6	11.7	69.2	17.0	1.33	1.94	3.88	4.05	2.67
10	2.0	1100	96.2	11.8	69.3	16.9	1.26	1.91	3.82	4.08	2.68
10	2.0	1080	94.7	12.1	70.1	16.5	1.13	1.80	3.54	4.17	2.75
10	2.0	1070	94.2	12.2	70.3	16.5	1.05	1.73	3.45	4.21	2.77
10	2.0	1065	93.9	12.2	70.4	16.4	1.01	1.69	3.42	4.23	2.78
10	2.0	1050	93.3	12.4	70.7	16.4	0.88	1.57	3.33	4.27	2.81
10	2.0	1035	92.6	12.5	71.0	16.4	0.76	1.43	3.22	4.32	2.84
10	2.0	1020	91.9	12.7	71.3	16.4	0.65	1.28	3.10	4.37	2.88
10	2.0	1005	91.2	12.8	71.7	16.4	0.54	1.11	2.98	4.43	2.91
10	2.0	990	90.5	12.9	72.0	16.3	0.45	0.95	2.86	4.48	2.94
10	2.0	980	90.1	13.0	72.2	16.3	0.39	0.84	2.77	4.51	2.97
10	2.0	960	89.3	13.2	72.6	16.3	0.29	0.64	2.61	4.56	3.01
10	2.0	950	89.0	13.3	72.7	16.3	0.25	0.56	2.53	4.58	3.02
10	2.0	935	88.6	13.4	73.0	16.3	0.20	0.44	2.43	4.60	3.05
10	2.0	920	88.1	13.5	73.2	16.3	0.16	0.34	2.33	4.61	3.07
10	2.0	910	87.1	13.8	72.9	16.5	0.13	0.29	2.29	4.68	3.13
10	2.0	895	85.6	14.1	72.6	16.9	0.11	0.23	2.23	4.78	3.21
10	2.0	880	84.1	14.5	72.2	17.2	0.08	0.18	2.17	4.86	3.29
10	2.0	865	82.7	14.9	71.8	17.5	0.07	0.13	2.12	4.94	3.38
10	2.0	850	81.3	15.2	71.4	17.9	0.05	0.10	2.08	4.99	3.47
10	2.0	835	79.4	15.7	71.1	18.2	0.04	0.08	2.05	5.02	3.57
10	2.0	820	76.2	16.5	70.9	18.3	0.03	0.07	2.02	5.15	3.52
10	2.0	800	70.0	18.3	71.2	18.1	0.03	0.07	1.93	5.57	3.07
10	2.0	790	67.3	19.2	71.3	18.0	0.03	0.07	1.86	5.79	2.86

Table 4.6 – Continued from previous page

H_2O^i	Р	Т	melt	H_2O^m	SiO_2	Al_2O_3	MgO	FeO_t	CaO	Na_2O	K_2O
10	2.0	785	66.0	19.7	71.4	18.0	0.03	0.07	1.81	5.90	2.77
10	2.0	770	62.6	21.2	71.7	17.8	0.03	0.08	1.67	6.21	2.51
10	2.0	755	59.5	22.8	71.9	17.7	0.03	0.08	1.54	6.50	2.28
10	2.0	740	56.9	24.4	72.1	17.6	0.03	0.08	1.43	6.75	2.07
10	2.0	725	54.4	26.1	72.3	17.4	0.03	0.08	1.32	6.97	1.90
10	2.0	710	52.2	27.9	72.5	17.3	0.03	0.07	1.23	7.15	1.76
10	2.0	700	45.0	28.6	72.4	17.3	0.02	0.07	1.14	7.47	1.55

Table 4.6 – Continued from previous page

CHAPTER 5

Empirical estimate of temperature, pressure and H_2O at liquidus conditions in silicic melt based on major element chemistry via support vector machine regression

5.1 Preface

The impetus for this study is the question at which conditions the liquidus of Archean tonalites-trondhjemites-granodiorites (TTG) is located under different variables of P-T-H₂O. This study emerged as a side track project while visiting Nanjing University during my final year. After I was not able to finish my experimental work at Macquarie University due to the piston cylinder laboratory not being fully operational, I was discontent as the liquidus of PC-103 was not fully explored for 10 wt% H₂O and experiments on a second sample of the suite, the trondhjemite PC-187 were insufficient to construct a PT diagram. Therefore I had to find an alternative way to investigate TTG formation conditions, which resulted in using the experimental data of published studies to calibrate a model that estimates liquidus conditions based on the equilibrium major element composition of experimental melts. The whole research until finishing the first manuscript draft was done by myself. Gerhard Wörner and Tracy Rushmer reviewed the manuscript.

5.2 Abstract

I calibrated a statistical model via a support vector machine regression (SVR) based on a large dataset (n = 740) comprising major element compositions of glasses produced in hydrous melting experiments to predict temperature, pressure and dissolved H₂O at liquidus conditions of a silicate melt. The goal is to construct a model where temperature, pressure and H₂O are estimated simultaneously and interdependent, by iteratively calculating the most likely conditions of the liquidus.

However, the model setup contains several flaws that prevents it from reliably functioning: (i) an artificial correlation of pressure and temperature in the input dataset due to the general experimental design of individual studies, (ii) an uncertainty of the H_2O dissolved into experimental melts and (iii) the interference of major element features resulting from pressure and H_2O by the diversity of starting materials used for the experiments. A statistical model as calibrated here is not able to resolve these issues. Despite that, individual calibrations within the model return reliable results. Therefore I calculated a liquidus temperature range for Archean tonalite-trondhjemite-granodiorite (TTG) to be 850-1050 °C solely based on major element compositions. Based on a H₂O dependent calibration approximately 8 wt% of H₂O dissolved are required for this temperature range. Furthermore I calculated the H₂O content and pressure conditions for Ti saturated liquidus temperatures of TTGs from chapter 3. As independently predicted in the previous chapter, the amount of H₂O required is between 9-12 wt%. Pressure conditions for the liquidus give a broad span from 0.5-2.0 GPa.

5.3 Introduction

The physical conditions of formation of silicate melts can only be indirectly inferred from petrography, chemical and isotopic analysis of magmatic rocks. The simulation of magmatic processes under laboratory conditions by melting experiments also provides an important reference frame to understand magmatic systems. To compare experiments and natural rocks and to understand the underlying processes, graphical systems like the Qtz-Fo-An-Di tetrahedron and the granite system (Tuttle and Bowen, 1958; Yoder and Tilley, 1962) have been established. Within these simplified compositional spaces, experimental results are schematised into vectors displaying the chemical evolution of melts governed by equilibrium phases. The position of the vectors, called cotectic paths, depend on extrinsic factors as temperature, pressure, available volatiles, oxygen fugacity and source rock composition (Adam et al., 2016; Gao et al., 2016). By comparing natural magmatic rock suites and experimentally determined cotectic paths, inferences about the extrinsic parameters that shaped the natural rock suite are possible.

In this study, I test modern data analysis on an experimental dataset of hydrous melting experiments comprising 36 different studies. The aim is to examine the entity of the data and develop a model capable of estimating the liquidus conditions in respect to T-P-H₂O. A large focus in doing so is on the statistical robustness of the model to support these predictions.

For the statistic evaluation of the data, I use a support vector machine (SVM) algorithm (Noble, 2006). SVM can be applied as a tool for regression (support vector machine regression (SVR) Vapnik, 1995; Smola and Schölkopf, 2004) and classification (Kowalczyk, 2017) that has been successfully applied in the field of medical science (Kourou et al., 2015) and was introduced for petrological applications by Petrelli and Perugini (2016).

I apply the model to natural felsic compositions of Archean cratons. The mechanisms of continental crust production during the Archean are proposed to have been different to the recent, globally operating plate tectonic system (Moyen and Martin, 2012), where magmatic felsic rocks are dominantly formed in convergent plate settings. The zircon record suggests that 60% of the current continental crust was already stable by the end of the Archean (Belousova et al., 2010; Hawkesworth et al., 2019). Granitoid rocks, characteristic for Archean continental crust, differ significantly from rocks that are produced in modern continental growth settings.

The dominant rock types are an association of tonalite-trondhjemite-granodiorite (TTG). Their distinct characteristics are a depletion in heavy rare earth element (HREE) and a high Sr/Y ratio, interpreted as the involvement of garnet during formation, a depletion in Nb-Ta-Ti, no negative Eu-anomaly and low K₂O concentrations (Moyen and Martin, 2012). The high Sr/Y ratio, combined with no Eu anomaly and low-K₂O differentiation trends favour the absence of plagioclase during their formation and evolution. These peculiarities of TTGs are the reason for a lack of knowledge regarding the predominant geodynamic environment during the Archean.

There are three commonly considered scenarios in which TTGs might have been formed (Palin et al., 2016). The first is a steep "modern style" subduction setting (Turner et al., 2014) with slab melting (Laurie et al., 2013), similar as what is proposed for the genesis of modern adakites (Martin et al., 2005). However, the formation of adakites does not seem to be limited to slab melting (Castillo, 2012). Another formation scenario is a setting of shallow subduction, respectively the stacking of oceanic crust by thrusting and subsequent melting within the garnet stability field (Foley et al., 2003; Nutman et al., 2015; Hastie et al., 2016). In a third scenario Archean crust is produced by the interplay of a "proto-crust" and mantle plumes (Bédard, 2006a; Van Kranendonk et al., 2007) producing and subsequently melting a thick oceanic plateau, accompanied by crustal overturns (Collins et al., 1998; Wiemer et al., 2018) and delamination of depleted eclogitised oceanic crust (Sizova et al., 2015; Johnson et al., 2014).

To discuss the origin of TTGs it is critical to decide which compositional signatures in TTGs are the result of their formation process, which were modified by subsequent magmatic differentiation and which are inherited from the source rock. Chapter 3 showed with the behaviour of Nb, that Ti phases could only have had a minor role in shaping the trace element signature of TTGs and that most of the Nb depletion is caused by another mechanism, may it be another phase or inheritance. The major element composition on the other hand is the direct result of the underlying magmatic process. Understanding the major elements is inevitable for any further interpretation. Here, the calibrated model can provide an elementary framework for this.

5.4 Methods

For the regression in this study I use an ϵ -SVR from the R package e1071 (Meyer et al., 2018). A SVR is a supervised learning algorithm (Kowalczyk, 2017). In contrast to a normal regression method, that minimises the error, SVR allows deviation up to a definable threshold (ϵ) and the option to penalize outliers outside of the range between hyperplane and margin within a range of ξ . However, the largest advantage of SVR is the use of kernel functions. If data can not be described or separated by a linear function, a kernel function transforms it into a higher dimension to make it linearly describable. The aim is to find a function that deviates less than ϵ from all training data $\{(x_1, y_1), ..., (x_n, y_n)\} \in \mathbb{R}^d$, while still being as flat

as possible (Smola and Schölkopf, 2004). In case of a function

$$f(x) = \langle \omega, x \rangle + b \text{ with } \omega \in \mathbb{R}^d, b \in \mathbb{R}$$

$$(5.1)$$

where the hyperplane is described by the the dot product of the orthogonal vector ω and x, the optimal hyperplane describing the data is found via the minimisation of ω . This is handled as a constrained convex optimisation problem minimising $\frac{1}{2}||\omega||^2$. Together with ξ to penalise outliers, following formulation is used in Vapnik, 1995:

$$\operatorname{minimise} \frac{1}{2} ||w||^2 + C \sum_{i=1}^n (\xi_i + \xi_i^*)$$

$$\operatorname{subject to} = \begin{cases} y_i - \langle w, x_i \rangle - b &\leq \epsilon + \xi_i \\ \langle w, x_i \rangle + b - y_i &\leq \epsilon + \xi_i^* \\ \xi_i, \xi_i^* &\geq 0 \end{cases}$$
(5.2)

 ξ is scaled by the constant C > 0. A small C does allow outliers to the expense of a large margin, whereas with a large C the focus is on avoiding outliers with the risk to over determine the model. The constraints on equation 5.2 concern the margins with the distance ϵ to the hyperplane. Any support vector needs to be within $\epsilon + \xi_i$, respectively $\epsilon + \xi_i^*$. The desired model is found by constructing a Lagrange function (Smola and Schölkopf, 2004) that results in a linear SVR function

$$f(x) = \sum_{i=1}^{n} (\alpha_i - \alpha_i^*) \langle x_i, x \rangle + b$$
(5.3)

with α_i and α_i^* being Lagrange multipliers. For the application in this study I chose a radial basis function kernel

$$k(x,x') = e^{\frac{||x-x'||^2}{2\sigma^2}}$$
(5.4)

that replaces the dot product $\langle x_i, x \rangle$ in the linear SVR of eq. (5.3).

The optimisation of ϵ and C is performed via a build in grid search of R package e1071 (Meyer et al., 2018) that identifies models with the lowest mean square error.

To test the SVR model, I use a k-fold cross-validation. The dataset is randomly divided 10,000 times into 75 % training- and 25 % test data. Each time the trained model is applied to the 25 % test data. Based on approximately 2500 iterations per experiment, mean and uncertainty are calculated.

By comparing linear regression with SVR over the same set of data, the SVR outperforms the linear regression in precision and accuracy. This is exemplified in fig. 5.1, with the residuals for linear regression and SVR of temperature, pressure and H_2O predictions on an experimental

dataset described in section 5.5.1. The superior performance of the SVR is apparent for temperature and pressure with lower residuals, however in case of H_2O the difference is not as incisive.

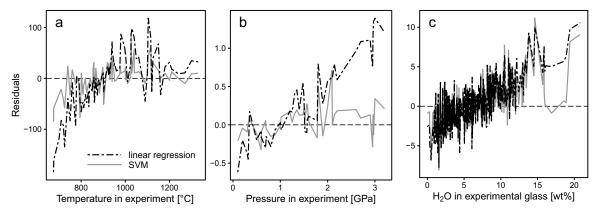


Figure 5.1: Residual plots for a linear regression and a SVR predicting temperature (a), pressure (b) and H₂O (c) of an experimental data compilation described in section 5.5.1. These and all subsequent diagrams are made with *ggplot2* (Wickham, 2016) in R (R Core Team, 2017).

5.5 Building the model

It is not possible to construct a thermo(baro)meter without a basic supporting physical principle. Good examples are cation exchange thermometers (e.g. amphibole - plagioclase of Holland and Blundy, 1994) or saturation thermometers (Ti-solubility, see chapter 3). Using the experimental glass compositions to build a statistical model is rather like the construction of isotherms in the granite system (Yoder and Tilley, 1962), an empirical approach to compare experimental and natural data.

In a first step I evaluate the potential to estimate each of the unconstrained parameters (P-T- H_2O) individually by training models to estimate them with the other two parameters being constrained. Furthermore I investigate the dependency and influence of the unconstrained parameters on each other by training several models that use different combinations of major elements and constrained parameters. As an example, temperature will be estimated by four different models: (i) major elements, (ii) pressure + major elements, (iii) H_2O + major elements, (iv) pressure + H_2O + major elements.

In the second step, I calibrate a self dependent model in which neither temperature, pressure or H_2O content are constrained. I overcome this limitation by determining T, P and H_2O parameters as functions of each other, additional to the major element data. I calculate T in a P-H₂O matrix, P in a T-H₂O matrix and H₂O in a P-T matrix, each to the extend that is covered by the data used for calibration. Considered as planes, the three matrices intersect in a 3-dimensional T-P-H₂O space, at which point the most likely liquidus condition is located.

5.5.1 The experimental dataset

The dataset used to train the model contains glass analyses from 789 individual hydrous melting experiments from 36 different studies (Conrad et al., 1988; Vielzeuf and Holloway, 1988; Beard and Lofgren, 1991; Holtz and Johannes, 1991; Patiño Douce and Johnston, 1991; Rapp et al., 1991; Skjerlie and Johnston, 1992; Skjerlie and Johnston, 1993; Sen and Dunn, 1994; Vielzeuf and Montel, 1994; Wolf and Wyllie, 1994; Gardien et al., 1995; Patiño Douce and Beard, 1995; Rapp and Watson, 1995; Skjerlie and Patiño Douce, 1995; Patiño Douce and Beard, 1996; Skjerlie and Johnston, 1996; Winther, 1996; Springer and Seck, 1997; Patiño Douce and Harris, 1998; Pickering and Johnston, 1998; Castro et al., 1999, 2000; Gardien et al., 2000; Koester et al., 2002; Skjerlie and Patiño Douce, 2002; Grant, 2004; Spicer et al., 2005; Patiño Douce, 2005; Sisson et al., 2005; Xiong et al., 2005; Alonso-Perez et al., 2009; Getsinger et al., 2009; Adam et al., 2012; García-Arias et al., 2012; Laurie and Stevens, 2012; Qian and Hermann, 2013; Hastie et al., 2016). It comprises major element composition, temperature, pressure, H₂O dissolved and the mode of the run products. The dataset covers an experimental temperature range from 675-1330 °C, pressure from 0.1-3.2 GPa (fig. 5.2a) and basaltic to rhyolitic melt compositions.

In many studies the amount of water dissolved in the experimental glasses is based on the

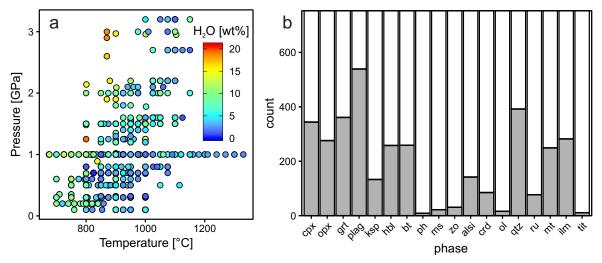


Figure 5.2: a: Pressure and temperature conditions and H_2O dissolved in the experimental melts. b: Abundance of different phases in the experimental dataset. cpx = clinopyroxene, opx = orthopyroxene, grt = garnet, plag = plagioclase, ksp = alkali feldspar, hbl = hornblende, bt = biotite, ph = phengite, ms = muscovite, zo = klinozoisite, alsi = alumina silicate, crd = cordierite, ol = olivine, qtz = quartz, ru = rutile, mt = magnetite, ilm = ilmenite, tit = titanite.

difference of the analytical total to 100 %. This estimation is too uncertain for the purpose of building a model. Therefore, I checked the reported H_2O dissolved into the melt carefully for each experiment and where applicable, recalculated the amount of water dissolved based on the initial water content of the experiment, the amount of glass and hydrous phases present by mass balance. Approximated H_2O concentrations for hydrous phases where taken from Gardien et al., 2000 (amphibole 2.0 wt% H₂O; mica (3.8 wt% H₂O). The H₂O content of amphiboles measured by Springer and Seck (1997) is also at 2 wt%. The corrected values are only valid if they are lower than the difference of the reported total to 100%. Subsequently I compared the theoretically calculated H₂O value with the reported H₂O of the study (fig. 5.3). The correction is applied to 291 experiments, the majority of samples have an appropriate H₂O estimate. As visible in fig. 5.3 most samples are corrected by 0-3 wt%, which is an appropriate error range for experimental glasses. However there are some experiments with corrections beyond 5 wt%. Due to the uncertainty regarding these experiments, they are excluded from the following calculations. The sample size is therefore decreased to 740. The reduced set also excludes experiments without reported H₂O. As a result, the reduced dataset contains experiments with dissolved H₂O concentrations covering a range from 0.0 to 20.8 wt% (fig. 5.2).

The abundance of different phases in the experiments is displayed in fig. 5.2b. Three quarters

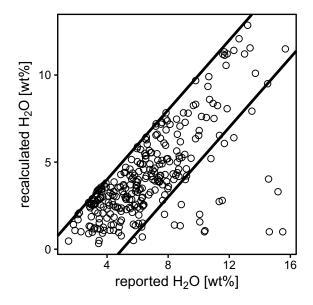


Figure 5.3: Recalculated H_2O concentration plotted against reported values for 291 samples. The upper line is the 1:1 ratio for calculated and reported values, the lower line marks a 5 wt% difference.

of the experiments are saturated in plagioclase, approximately half in quartz, garnet and cpx, and one third in biotite, opx and amphibole. A minority of experiments is saturated in alumino-silicates, K-feldspar and cordierite. Most common accessory phases are magnetite and ilmenite, present in about one third of the experiments.

Major elements used for the temperature estimate are SiO₂, Al₂O₃, FeO_t, MgO, CaO, Na₂O and K₂O. TiO₂ and P₂O₅ concentrations are left out intentionally because both elements tend to form excess phases (Hellman and Green, 1979; Harrison and Watson, 1984). Their concentration in silicate melts is closely linked to their saturation and dependent on the amount of the respective element in the host rock. The nescience regarding their saturation

in natural rocks is a factor of uncertainty that is best avoided by excluding both elements.

5.5.2 Temperature calibration

The model describing temperature is based on pressure, H_2O , SiO_2 , Al_2O_3 , FeO_t , MgO, CaO, Na₂O and K₂O. Four different models are calibrated and tested, the first one only based on major elements (fig. 5.4a), the second one also including pressure (fig. 5.4b), a third model based on H_2O and major elements and a fourth model based on pressure, H_2O and major elements (fig. 5.4d). By this approach the influence of the two unconstrained parameters pressure and H_2O can be evaluated.

Determining the temperature solely via selected major elements (fig. 5.4a) returns a good fit

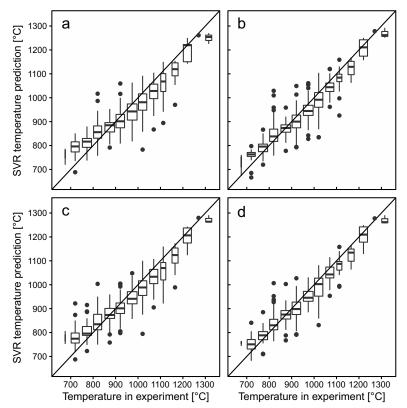


Figure 5.4: Box plots comparing estimated with recorded temperatures. The box width is ≤ 50 °C. a: Temperature estimate based on major element composition. b: Temperature estimate based on H₂O and major element composition d: Temperature estimate based on pressure, H₂O and major element composition.

between 850 and 950 °C. Temperatures below 850 °C are overestimated and above 950 °C underestimated within an range of approximately 50 °C. High temperature experiments at 1200 °C are well described. However, there are a few outliers that deviated in their estimated temperature from the recorded one by more than 100 °C. On average, over and underestimation cancel each other out resulting in a mean temperature deviation of 0.4 °C with a root mean square error (RMSE) of 54.4 °C. The \mathbb{R}^2 for estimated and recorded

temperature is 0.72. The performance of all models is summarised in table 5.1.

The model using pressure and major elements (fig. 5.4b) improves in fit compared to the model using only major elements. Temperatures are well described over the whole range, however there are outliers with a deviation of more than 200 °C. The model produces a negligible low bias with a mean deviation of 0.1 °C (table 5.1) The RMSE decreases to 45.6 °C and \mathbb{R}^2 increases to 0.81. It is unexpected that adding pressure to the equation improves the model significantly. A possible explanation might be that the experimental dataset is biased by the positive correlation between temperature and pressure, artificially produced by the general experimental design of high pressure experiments at higher temperatures (fig. 5.2). The model based on water and major elements. Temperatures below 850 °C are overestimated and temperatures above 950 °C are slightly underestimated. The performance in the low temperature range is the weakest for all four models by having the most and biggest outliers in that interval. As discussed in section 5.5.1, the H₂O content of the melt is much more difficult to constrain and therefore prone to error and uncertainty. On average the deviation from the recorded temperature is at -0.3 °C with a RMSE of 50.2 °C. \mathbb{R}^2 is 0.76.

Adding both pressure and H_2O to the model (fig. 5.4d) decreases the mean temperature deviation to -0.3 °C with a RMSE of 41.9 °C. As graphically visible, the addition improves the prediction over the whole range of conditions, by shortening of the box plot whiskers. The greatest improvement is in the low temperature range, where temperatures are now only slightly overestimated. This is due to the high H_2O content of low temperature melts. The overall improvement is reflected by R^2 of 0.83.

In section 5.8 the temperature estimation is further discussed with respect to the individual studies contributing to the database.

5.5.3 Pressure calibration

As for temperature, four different models are calibrated to estimate pressure conditions at which the experiments were conducted (fig. 5.5). The performance of the individual models is summarised in table 5.1. Pressure conditions estimated by the first model, using only major element data, are displayed as box plot in fig. 5.5a. The pressure is well estimated on average between 0.5 to 2.0 GPa based on the major element chemistry, however there is a broad scatter and big outliers. Low pressure estimates are generally overestimated, while high pressures above 2.0 GPa are underestimated. Outstanding is the box describing pressure between 2.75-3.00 GPa due to an underestimation of 1.5 GPa. In average, the over- and underestimates cancel each other out, resulting in a mean pressure deviation of -0.005 GPa however the scatter results in a RMSE of 0.419 GPa. The R² between estimated and recorded pressure is 0.59.

Adding temperature to the estimate improves the pressure prediction (fig. 5.5b). On average there is a good pressure prediction below 1.75 GPa. Within this range most boxes and

parameter	model input	mean deviation	RMSE	\mathbb{R}^2						
Т	ME	0.4	54.4	0.72						
Т	P + ME	0.1	45.6	0.81						
Т	$H_2O + ME$	-0.3	50.2	0.76						
Т	$P + H_2O + ME$	-0.3	41.9	0.83						
Р	ME	-0.005	0.419	0.59						
Р	T + ME	-0.018	0.364	0.69						
Р	$H_2O + ME$	-0.016	0.384	0.66						
Р	$T + H_2O + ME$	-0.008	0.328	0.74						
H ₂ O	ME	-0.19	2.51	0.46						
H_2O	T + ME	-0.10	2.28	0.55						
H_2O	P + ME	-0.15	2.28	0.55						
H_2O	T + P + ME	-0.15	2.14	0.61						
Interdependent T-P-H ₂ O model										
Т	$P + H_2O + ME$	17.2	63.2	0.65						
Р	$T + H_2O + ME$	0.120	0.493	0.46						
H_2O	T + P + ME	-0.24	2.65	0.40						
Least squares approach										
Р	T + ME	0.378	0.75	0.22						
H_2O	T + ME	2.83	5.50	0.05						

Table 5.1: Statistical evaluation of the cross validation on the various SVR models describing temperature [°C], pressure [GPa] and H₂O [wt%]. Abbreviations: T = temperature, P = pressure and ME = major elements.

whiskers are reduced in size and the amount and deviation of outliers are both decreased. The estimate of higher pressures is better as well, however they are still underestimated. The box containing 2.75-3.00 GPa is strongly underestimated. In summary, pressures are slightly underestimated on average with -0.018 GPa and a RMSE of 0.364. R^2 is 0.69. The reason of temperature improving the prediction might at least be partially caused by the artificial positive correlation with pressure, as already discussed. An additional method to constrain pressure by using a least squares approach on the temperature prediction model (fig. 5.4b) is shown in the appendix fig. 5.15b. However the cross validation reveals a weak performance (table 5.1)

Estimating pressure with H_2O and major elements (fig. 5.5c) is slightly worse as with temperature. While the estimation below 2.0 GPa is similar to the estimate including temperature, the amount of outliers increased. High pressures are underestimated, however the strong deviation of the box containing 2.75-3.00 GPa estimates is abrogated. The reason for H_2O improving these experiments that significant might be that the box contains very high H_2O content experiments by Laurie and Stevens (2012). On average the pressure is slightly underestimated by -0.016 GPa and a RMSE of 0.384 GPa. R^2 is 0.66.

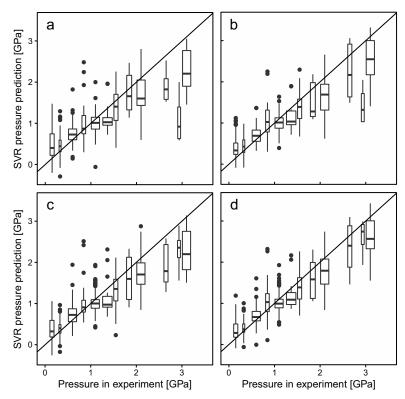


Figure 5.5: Box plots comparing estimated with recorded pressures. The box width is ≤ 0.25 GPa. a: Pressure estimate based on major element composition. b: Pressure estimate based on temperature and major element composition. c: Pressure estimate based on H₂O and major element composition. d: Pressure estimate based on temperature, H₂O and major element composition.

Using temperature, H_2O and major elements improves the estimate over the whole pressure range (fig. 5.5d) and returns the best result of all four models. This is reflected by an increased R^2 of 0.74. While the number of outliers is not reduced, most boxes and whiskers decrease in range. The prediction of the high pressure experiments around 3 GPa is improved, however they are still underestimated. In general, the pressure is slightly underestimated by -0.008 GPa with a RMSE of 0.328 GPa.

In summary, pressure can be estimated roughly. The RMSE of the best working model with known temperature and H_2O is still at 0.328 GPa, being more than 10 % of the whole pressure range of the dataset. In section 5.8 the pressure estimation is further discussed in respect to the individual studies contributing to the database.

5.5.4 H_2O calibration

With the same approach as for temperature and pressure, the amount of water present in the experimental glasses is estimated. Results for the calibration on solely major elements are displayed in fig. 5.6a. An overestimation of H_2O content below 5 wt% is observable, as well as an increasing underestimation of experiments containing more than 10 wt% of H_2O . The

 H_2O content is on average underestimated by -0.19 wt% with a RMSE of 2.51 wt%. R^2 for estimated and recorded H_2O content is 0.46.

The addition of temperature to the model improves the H₂O estimate (fig. 5.6b), mainly observable in a decrease of outliers to the cost of slightly increased whisker lengths. The overall result of the model has not significantly changed in comparison to the major element dependent model. H₂O contents are overestimated below 5 wt% while they are underestimated above 8 wt%. On average, H₂O is underestimated by -0.10 wt% with a RMSE of 2.28 wt%. R^2 is 0.55. An additional method to constrain H₂O using a least squares approach on the temperature prediction model (fig. 5.4c) is shown in the appendix fig. 5.15a. As for the least squares calculation to estimate pressure, the model performance is very weak (table 5.1).

The model based on pressure and major elements (fig. 5.6c) performs quite similar to the two models already described, except for an improvement in estimates for H₂O contents above 15 wt%. On average, H₂O contents are overestimated below 5 wt% and underestimated above 7 wt%. The mean deviation of estimates is -0.15 wt% with a RMSE of 2.28 wt%. R^2 is 0.55, the same as for the model using temperature and major elements.

Using pressure, temperature and major elements for the H₂O estimate improves the model by

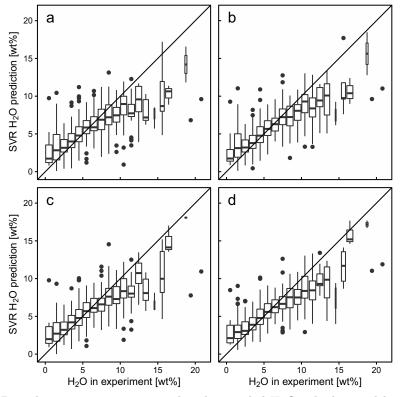


Figure 5.6: Box plots comparing estimated with recorded H₂O. The box width is $\leq 1 \text{ wt\%}$. a: H₂O estimate based on major element composition. b: H₂O estimate based on temperature and major element composition. c: H₂O estimate based on pressure and major element composition. d: H₂O estimate based on temperature, pressure and major element composition.

a reduction of the overall scatter (fig. 5.6d). However, low H_2O contents are still overestimated

and H_2O above 7 wt% underestimated. Again, over- and underestimates cancel each other out resulting in a mean underestimation of -0.15 wt% with a RMSE of 2.14 wt%. The R^2 is 0.61.

As for pressure, the estimate of H_2O dissolved works only roughly with a high uncertainty and bias. Complicating the estimate is the systematic offset that low contents are overestimated and high contents are underestimated. This leads to the situation in which the whiskers of the 1 wt% and the 15 wt% box overlap. Even though H_2O contents in between these values are better constrained, especially the poor estimates on high H_2O contents will cast uncertainty on any lower H_2O estimate, when applied to natural samples.

A possible reason for the poor estimate is that H_2O dissolved in the experimental melts are not well enough constrained, even though they were checked by mass balance. Another explanation might be that H_2O simply can not be that well constrained by the parameters used. The major element features influenced by H_2O might be superimposed by other factors as the diversity of starting compositions for the experiments. An example for that is the K_2O/Na_2O ratio. At high H_2O content the crystallisation of plagioclase is suppressed which results in a nearly constant ratio through a differentiation sequence (chapter 4). At low H_2O concentrations the ratio would rise with differentiation. However, when the source of the melt is already rich in K_2O , the model cannot tell the difference, as information about the source are not included. This will bias the model.

In section 5.8 the H_2O estimation is further discussed in respect to the individual studies contributing to the database.

5.5.5 Interdependent T-P-H₂O estimate

In a next step the three individual models for temperature, pressure and H_2O are combined, so that the only input parameters are major elements. As for the individual models, I use a k-fold cross validation with 75 % training and 25 % test data. The calculation process though is different. For each sample three matrices are created based on the extend of the dataset:

- (i) a temperature calculation matrix ranging from 0 to 3.5 GPa by 0.25 GPa increments and 0 to 20 wt% H_2O with 1 wt% increments;
- (ii) a pressure calculation matrix ranging from 700 to 1350 °C by 25 °C increments and 0 to 20 wt% H₂O by 1 wt% increments;
- (iii) a H₂O calculation matrix ranging from 700 to 1350 °C by 25 °C increments and 0 to 3.5 GPa by 0.25 GPa increments.

Subsequently, values for each element in the matrices are calculated and stored as a three column data frames. The intersection of the three data frames in the T-P-H₂O space is calculated via an euclidean distance nearest neighbour search *matchpt* of the R package *Biobase* (Huber et al., 2015). The function is limited to finding the nearest neighbour of 2 matrices, wherefore it was run multiple times to define the nearest neighbour of the three

matrices and an average intersect was calculated. Due to the computational intensive code, the number of iterations was decreased to 1000. The results of the T-P-H₂O estimate are displayed in fig. 5.7 and table 5.1.

There is a significant overestimation of temperatures below 900 $^{\circ}C$ and a slight underestima-

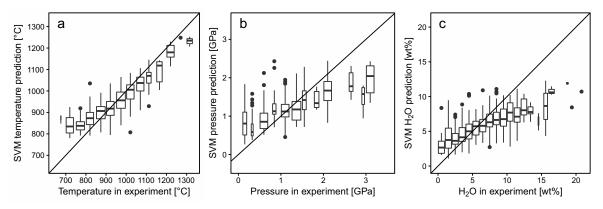


Figure 5.7: Boxplots for temperature (\mathbf{a}) , pressure (\mathbf{b}) and $H_2O(\mathbf{c})$ estimates based on the interdependent model.

tion of temperatures above 1000 °C (fig. 5.7a). The model performs worse than the previous predictions (fig. 5.4) having a \mathbb{R}^2 of 0.65. On average the temperature is overestimated by 19.3 °C with a RMSE of 59.0 °C. The estimation of pressure (fig. 5.7b) is worse as well. \mathbb{R}^2 is decreased to 0.46. Pressure conditions below 1.0 GPa are overestimated and pressure above 1.5 GPa is underestimated. On average the pressure is overestimated by 0.14 GPa and has a RMSE of 0.5 GPa. H₂O estimates are also inferior to the predictions displayed in fig. 5.6. \mathbb{R}^2 is 0.40. H₂O concentrations below 5 wt% are overestimated and concentrations above 5 wt% are underestimated. On average, H₂O is underestimated by -0.30 wt% with an RMSE of 2.89. The results show that the model does not work satisfactorily. It is not possible to extract information about pressure and H₂O conditions from the model. However, temperatures above 900 °C are acceptably well described, though worse than the model using major elements only. As already discussed, the poor performance of the model might be due to poor constraints on H₂O in the dataset, which biases the estimates on temperature and pressure. As a feedback loop, this worsens the estimate for H₂O. The underestimation of high H₂O content is reflected in the overestimation of low temperatures.

However, this can not be sole reason, as the temperature prediction that includes determined H_2O and pressure (fig. 5.4b) works well. It could be a systematic problem of the model, that uncertainties are too large to use three unconstrained parameters to iteratively define each other.

5.6 Application to Archean TTGs

I apply different models to the same filtered dataset TTG as used in chapter 3. First, only the liquidus temperature based on major elements and different H_2O contents is estimated.

 H_2O and pressure can not be estimated based on major elements due to identified weaknesses of the respective models (section 5.5.3 & 5.5.4). Secondly, temperature, pressure and H_2O are estimated via the interdependent model and thirdly, pressure and H_2O are estimated for Ti saturated liquidus temperatures from chapter 3.

The TTG dataset comprises the data compilations of Moyen (2011) and Johnson et al. (2019), and further data from Nutman et al. (1999), Laurent et al. (2014) and O'Neil and Carlson (2017). The dataset is filtered for tonalitic, trondhjemitic and granodioritic compositions based on the feldspar diagram of O'Connor (1965). Furthermore samples are discarded if they have La < 10, Yb > 2 and an Eu-anomaly below 0.9 or above 1.1. To ensure that the TTGs are within the compositional range of the used experiments, I compare them in appendix fig. 5.16 via harker diagrams. Most TTGs plot well within the range of experimental melt compositions, however there are 12 samples that stand out by their high MgO content (fig. 5.16c). I remove them as they are most likely cumulates. This results in 345 out of 1860 samples. This filtering effort assures that only samples that could have been a magmatic liquid are considered for the model. A portion of TTGs might be at least partially affected by accumulation of plagioclase and amphiboles as described by Laurent et al. (2020) for samples from the Barberton.

The first model applied to TTGs is the temperature estimation solely based on the major element composition. This results in temperatures between 800-1100 °C with the majority of samples between 900 and 1000 °C (fig. 5.8). Statistical parameters of the model results and subsequent temperature estimate models are displayed in table 5.2.

Table 5.2: Statistical indices of the temperature distribution of TTGs from fig. 5.8 estim	ated by
the models displayed in fig. 5.4a and fig. 5.4c.	
H ₂ O [wt%] min 1 st an median mean 3^{rd} an max	

H_2O [wt%]	min.	1^{st} qn.	median	mean	3^{rd} qn.	max.
-	774	921	952	948	979	1122
4	834	967	990	990	1014	1119
8	774	905	950	948	988	1097
12	705	827	882	882	936	1093

In a second step I estimate the temperature with the model based on H_2O and the major element composition, which is displayed in fig. 5.8. Since H_2O is not constrained I select a range of water contents based on the liquidus temperature calculations from the Ti solubility study in chapter 3. There the amount of water dissolved in the melt was defined as 8-12 wt%. Additionally I select 4 wt% H_2O to see if the model performs as expected. With 4 wt% H_2O present TTG liquidus temperatures are estimated to be between 900 and 1100 °C, with most samples between 950 and 1050 °C. At 8 wt% H_2O present, the estimated temperatures are between 900 and 1100 °C. With 12 wt% H_2O the estimated temperatures are between 700 and 1100 °C. More than half of the samples have temperatures between 800 and 950 °C. As expected there is a decrease in

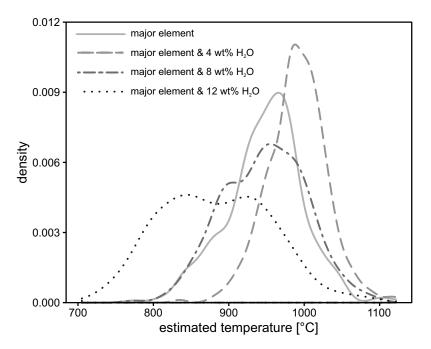


Figure 5.8: Temperature estimate distribution for natural TTGs (Nutman et al., 1999; Moyen, 2011; Laurent et al., 2014; O'Neil and Carlson, 2017; Johnson et al., 2019) calculated with the models displayed in fig. 5.4a and fig. 5.4c. The H₂O dependend model is set with fixed values of 4, 8 and 12 wt% H₂O.

temperature with increasing H_2O content, however the interval of temperatures also widens. A few high temperature samples only decrease marginal as displayed in table 5.2. Furthermore a trend to a bimodal distribution with increasing H_2O content is observable, which might be an artight of the model. A possible explanation is the conflict of high H_2O and high MgO content, a combination that is outside the calibration range of the model (appendix fig. 5.17). The model without a H_2O input and the model with 8 wt% H_2O have similar distributions. As both model calibrations perform similar (fig. 5.4a and c, 5.1) it is reasonable to assume that the amount of H_2O in TTGs was around 8 wt% and the temperature range for the majority of TTGs around 850-1050 °C. This temperature range is in good agreement with TTG liquid producing experiments (Rapp and Watson, 1995; Winther, 1996; Skjerlie and Patiño Douce, 2002; Adam et al., 2012; Laurie and Stevens, 2012; Hastie et al., 2016). The models also reflect the internal differentiation of TTGs, spanning over more than 15 wt% SiO_2 by returning a temperature interval of 300-400 °C (table 5.2). However, without any further constraints on conditions, the informative value of these calculations regarding the formation conditions of TTGs remains limited as the temperature span can be arbitrarily shifted depending on the assumed H_2O content.

5.6.1 T-P-H₂O estimate for TTGs with the interdependent model

Even though the performance of the interdependent model is weak and biased (section 5.5.5) I apply the natural TTG compositions to the model. The results are displayed in fig. 5.9 as

histograms. The temperature estimates (fig. 5.9a) lie between 750-1125 $^{\circ}$ C, with a majority between 900 and 1050 $^{\circ}$ C. Temperatures in the low range might be overestimated as it is for experimental data in section 5.5.5.

The results of the pressure estimates (fig. 5.9b) show a bimodal distribution for the pressure. The first peak is at 1.2 GPa and the second at 1.8 GPa. Pressure estimates range from 0.7 to 3.2 GPa. A peculiar result is the occurrence of the high pressure results because the cross validation of experimental data (fig. 5.7b) returned a strong underestimation in this range without any estimates greater than 2.5 GPa.

The results for H_2O (fig. 5.9c) are almost a Gaussian distribution around 8 wt%, with a total range from 2 to 13 wt%. This range is unambiguously a reflection of the model calibration (fig. 5.7c) that strongly underestimates H_2O contents above 10 wt%, and overestimates H_2O below 5 wt%.

The generally low H₂O contents most likely causes the high temperature range, that is comparable to the ranges calculated for 4, 8 wt% and independently of H₂O (fig. 5.8 and table 5.2). A P-T diagram of the estimated results (fig. 5.9d) shows a positive correlation of pressure and temperature, quite similar to the one of the experimental data used for calibration (fig. 5.2). The error bars for temperature and pressure are the RMSE, as calculated by cross validation (63.2 °C and 0.493 GPa, table 5.1). H₂O shows an expected behaviour with low concentration at high temperatures and high concentration at low temperatures. There is only a weak or no correlation of estimated pressure and pressure sensitive trace element ratios (fig. 5.9e and f) supporting the previous suggestion that pressure estimates are strongly biased.

As expected from the cross validation results, the interdependent model does not work sufficiently well and therefore the results calculated here do not have any real significance.

5.6.2 H_2O and pressure estimate for Ti saturated liquidus temperatures

Solely using the calibrated models, it is not possible to state anything definite about the formation conditions of TTGs as the temperature shifts with H_2O and the interdependent model does not work sufficiently. However, in chapter 3 we independently calculated Ti saturated liquidus temperatures for TTGs which can be compared to the results of this study (fig. 5.10). The Ti saturation temperatures of potentially saturated TTGs (750-900 °C) match the temperature estimates by choosing a H_2O content between 8-14 wt% for the model. This is slightly higher than the H_2O in chapter 3 (8-12 wt% H_2O) based upon graphical comparison of Ti saturated experiments and TTGs. The Ti study has a different methodology and database, that marginally overlaps with the database used here, but results in similar H_2O estimates for Ti saturated liquidus temperatures of TTGs.

Furthermore, I use the Ti temperatures as an input for a H_2O estimate using the calibration comprising temperature and major elements (fig. 5.6b). The resulting distribution of H_2O content required for the samples to be at the liquidus is displayed in fig. 5.11a. It ranges from

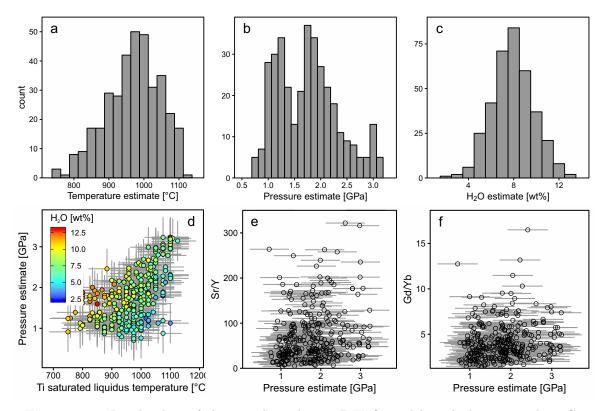


Figure 5.9: Result plots of the interdependent T-P-H2O model applied to natural TTGs (Nutman et al., 1999; Moyen, 2011; Laurent et al., 2014; O'Neil and Carlson, 2017; Johnson et al., 2019): a: Temperature results. b: Pressure results. c: H_2O results. d: P-T diagram combining the estimates on pressure temperature and H_2O content. The error bars represent the RMSE of the model calibration (5.1). e: Gd/Yb ratio of natural TTGs plotted against the estimated pressure. f: Sr/Y ratio of natural TTGs plotted against the estimated pressure.

3-17 wt% with the majority of samples in between 9 and 12 wt\%. However, this prediction needs to be set into context of the model bias, resulting in an underestimation of elevated H₂O contents.

As for H_2O , we can estimate pressure based on Ti temperatures and major elements. The results cover a range of 0.5-2.1 GPa with the majority of TTGs within 1.0-1.5 GPa (fig. 5.11b). In context of the model bias (fig. 5.5b) high pressure might be underestimated.

With pressure, temperature and H₂O given, a P-T diagram can be constructed (fig. 5.11c). The temperature error bars are the 11 % 1 σ uncertainty of the Ti saturation model. Error bars for pressure where calculated accounting for the 11 % input temperature uncertainty and the RMSE of 0.364 GPa (table 5.1) of the model itself. On average, the error bars extend to 0.84 GPa. There is an issue with a few samples, especially the high temperature samples predictions. They plot at the verge or even outside of their error bars, which hints towards an over-determination of the model in these regions.

The P-T diagram reveals a slight negative correlation of pressure and temperature, exactly the opposite as the results of the interdependent estimates (fig. 5.9d). H_2O behaves as expected

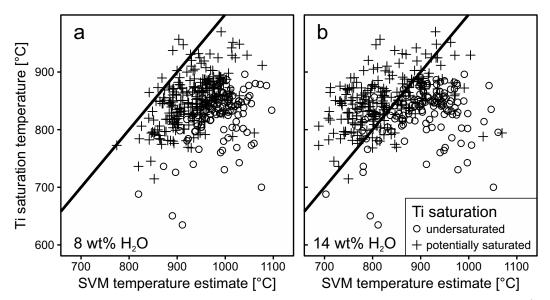


Figure 5.10: SVM based TTG temperature estimate calculated for different H_2O contents ($\mathbf{a} = 8 \text{ wt\%}$, $\mathbf{b} = 14 \text{ wt\%}$) compared with Ti saturation temperatures (chapter 3) for natural TTGs (Nutman et al., 1999; Moyen, 2011; Laurent et al., 2014; O'Neil and Carlson, 2017; Johnson et al., 2019). The black line as a 1:1 slope.

in regard to temperature and there is a positive correlation with pressure, accounting for the increased solubility even though pressure and H_2O were estimated independently.

It remains uncertain if the estimated pressures have any real significance, even though there are slight positive correlations of pressure estimates and pressure sensitive trace element ratios (fig. 5.11d, e). Even in case of a correct estimate, the uncertainty of the estimates are extremely high with almost 0.5 GPa. The estimated H_2O content is more reliable than pressure, especially due to the overlapping in estimation with results from chapter 3. This amount of water favours the presence of a fluid during melting as suggested by Laurie and Stevens (2012), Kleinhanns et al. (2003) and in chapter 3.

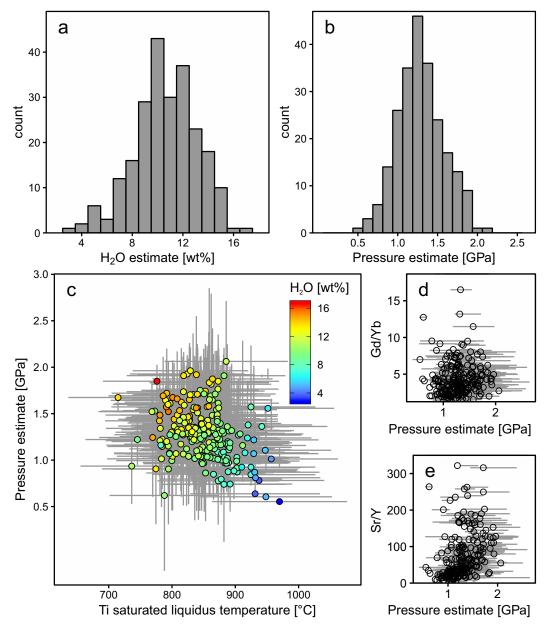


Figure 5.11: a: H₂O content of melts estimated for the Ti saturated liquidus temperature (chapter 3) of natural TTGs (Nutman et al., 1999; Moyen, 2011; Laurent et al., 2014; O'Neil and Carlson, 2017; Johnson et al., 2019). b: Pressure estimate for TTGs at the Ti saturated liquidus based on temperatures (chapter 3) and major elements. c: P-T diagram for the Ti saturated liquidus of TTGs based on temperatures from (chapter 3). Pressure and H₂O are estimated as displayed in fig. 5.11a & b. Temperature error bars are based on 11 % 1 σ uncertainty of the Ti temperatures (chapter 3.) Pressure error bars are based on the pressure RMSE of 0.328 and the 11 % 1 σ interval for temperature. d: Gd/Yb ratio of natural TTGs plotted against the pressure estimate of fig. 5.11c. Error bars are the same as in fig. 5.11c. e: Sr/Y ratio of natural TTGs plotted against the pressure estimate of fig. 5.11c.

5.7 Summary and conclusions

The calibration of a statistical model based on a SVR algorithm to predict temperature, pressure and H_2O dissolved in the melt at liquidus conditions using a large database of hydrous melting experiments results in several models that each bear their own benefits and limitations. The objective to calibrate an interdependent model that accounts for the three unconstrained parameters simultaneously could not be achieved due to an artificial correlation of temperature and pressure in the experimental dataset, uncertainty in the H_2O content of the experimental glasses and a masking of the influence of pressure and H_2O on major element composition due to the diversity of starting materials. Therefore, the application of the model to TTGs solely based on their major element composition does not result in reasonable or reliable estimates.

Applying only a major element dependent temperature estimate on TTGs returns a temperature span with most samples being in between 850-1050 °C. A H₂O dependent temperature estimate using 8 wt% set as input parameter results in a very similar distribution. Therefore 850-1050 °C with approximately 8 wt% H₂O present is the most reasonable output of the model for TTG formation temperatures.

Using Ti saturated liquidus temperatures for TTGs as an input parameter allows the usage of pressure and H_2O prediction models that return reasonable results for H_2O with most samples between 9-12 wt%, in good agreement with previous findings. The pressure estimates between 0.5-2.0 GPa are realistic, but there is a large uncertainty and flaws of the model prohibit further conclusions. However, the elevated amount of H_2O favours the presence of a free fluid during TTG melt formation, hence a convergent, subduction-like setting.

5.8 Appendix

Figure 5.12 displays the mean temperature deviations grouped by publication to evaluate the consistency of experimental data in between different studies. For the temperature estimate, the model comprising pressure, H₂O and major elements is used (fig. 5.4d). The broad majority of studies plot within the RMSE of the model, irrespective of the number of experiments used from the studies. It is apparent that studies with many experiments (e.g. Beard and Lofgren, 1991 n = 85) influence the model stronger than studies with lesser experiments. Despite this, small studies like Skjerlie and Patiño Douce (1995) (n = 3), Getsinger et al. (2009) (n = 6) or Laurie and Stevens (2012) (n = 6) are consistent with the rest of the data. However there is data that is inconsistent with the majority, which can be seen by the median of a study being outside of the RMSE range as for Skjerlie and Johnston (1993) and Springer and Seck (1997), or by broad whiskers and outliers (Rapp et al., 1991). Excluding individual mismatching experiments or studies does not improve the model. It reduces the amount of data, the model changes and in doing so produces other outliers or mismatching studies.

Figure 5.13 displays the mean pressure deviation grouped by publication to evaluate the consistency of experimental data in between different studies. The model used for the pressure estimate comprises temperature, H_2O and major elements (fig. 5.5d). As for temperature (fig. 5.12), most studies are consistent within the dataset and only few differ significantly in their average pressure estimate. The study of Hastie et al. (2016) strongly diverges from the rest of the data and experiments of Rapp and Watson (1995) deviate strongly towards over and underestimation. The number of samples that individual studies contribute does not influence the consistency with studies of low sample size being in good alignment (Skjerlie and Johnston, 1992; Wolf and Wyllie, 1994; Skjerlie and Patiño Douce, 1995; Getsinger et al., 2009; Laurie and Stevens, 2012).

Figure 5.14 displays the mean H_2O deviation grouped by publication to evaluate the consistency of experimental data in between different studies. The model used for the H_2O estimate comprises temperature, pressure and major elements (fig. 5.6d). The majority of studies are consistent with three studies having their median outside of the 1 RMSE range (Wolf and Wyllie, 1994; Castro et al., 1999; García-Arias et al., 2012). There are more outliers present than for temperature and pressure (fig. 5.12 and ??), indicating the difficulties in constraining an accurate H_2O content in experimental glasses. The consistency of a study is independent of the number of experiments it contributes to the model. Studies only comprising a few experiments are well predicted (Vielzeuf and Holloway, 1988; Skjerlie and Johnston, 1992; Gardien et al., 1995; Pickering and Johnston, 1998).

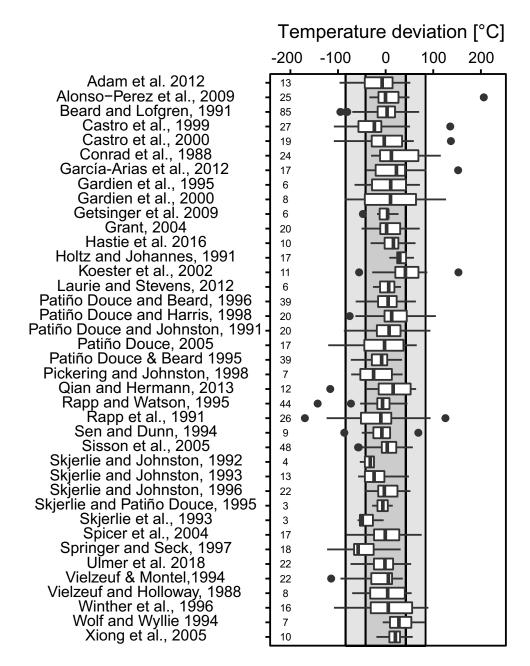


Figure 5.12: Box plot of temperature deviation based on the model estimating temperature by pressure, H_2O and major elements (fig. 5.4d) with the results sorted by their studies. Leftside of the diagram the count of experiments from the respective study is displayed. The shaded areas represent the RMSE and 2*RMSE of the model (table 5.1).

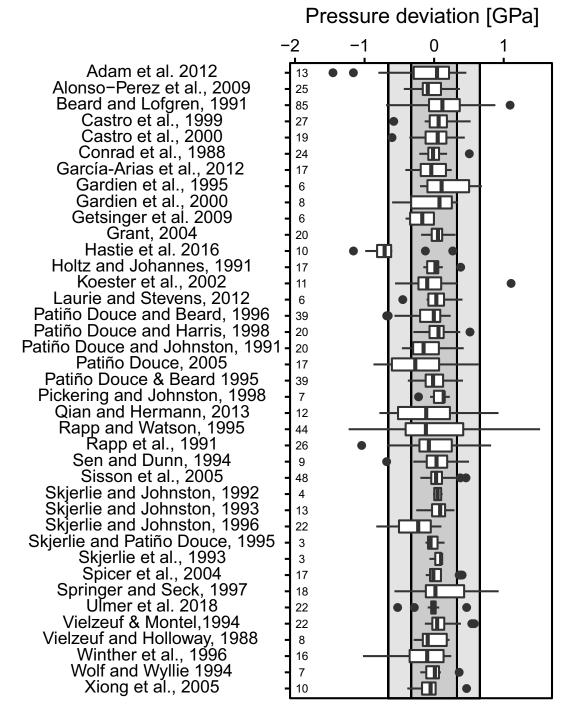


Figure 5.13: Box plot of pressure deviation based on the model estimating pressure by temperature, H_2O and major elements (fig. 5.5d) with the results sorted by their studies. Leftside of the diagram the count of experiments from the respective study is displayed. The shaded areas represent the RMSE and 2*RMSE of the model (table 5.1).

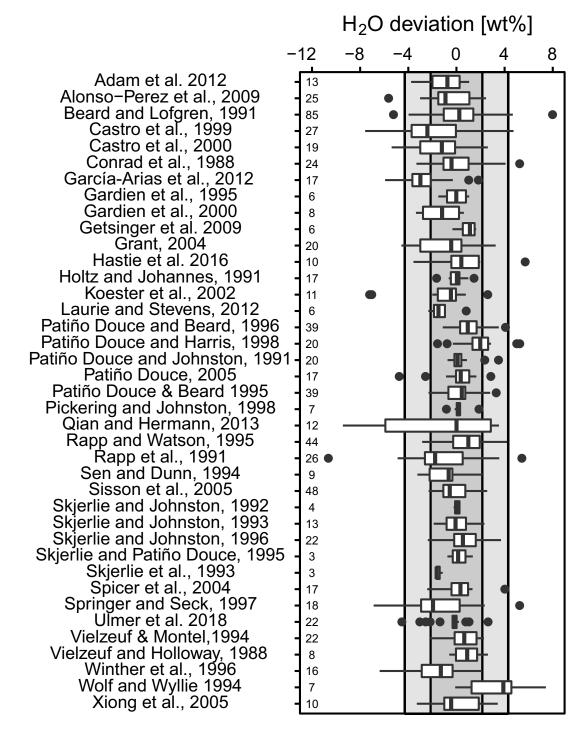


Figure 5.14: Box plot of H_2O deviation based on the model estimating H_2O by temperature, pressure and major elements (fig. 5.6d) with the results sorted by their studies. Left side of the diagram the count of experiments from the respective study is displayed. The shaded areas represent the RMSE and 2*RMSE of the model (table 5.1).

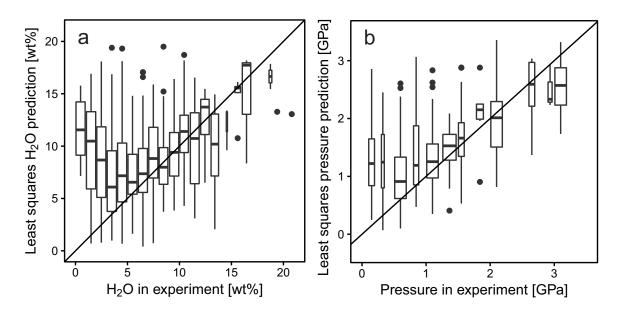


Figure 5.15: a: Evaluation of H_2O prediction via least squares with the temperature estimating SVM model that depends on H_2O and major elements (fig. 5.4c). H_2O is varied as an input variable to minimise the difference between target and estimated temperature. The model is tested via k-fold cross validation with 4000 iterations. The diagram is based on 707 experiments that have a difference of target- and estimated temperatures ≤ 1 °C. b: Evaluation of pressure prediction via least squares with the temperature estimating SVR model that depends on pressure and major elements (fig. 5.4b). Pressure is varied as an input variable to minimise the difference between target and estimated temperature. The model is tested via k-fold cross validation with 4000 iterations. The diagram is based on for pressure and major elements (fig. 5.4b). Pressure is varied as an input variable to minimise the difference between target and estimated temperature. The model is tested via k-fold cross validation with 4000 iterations. The diagram is based on 693 experiments that have a difference of target and estimated temperatures ≤ 1 °C.

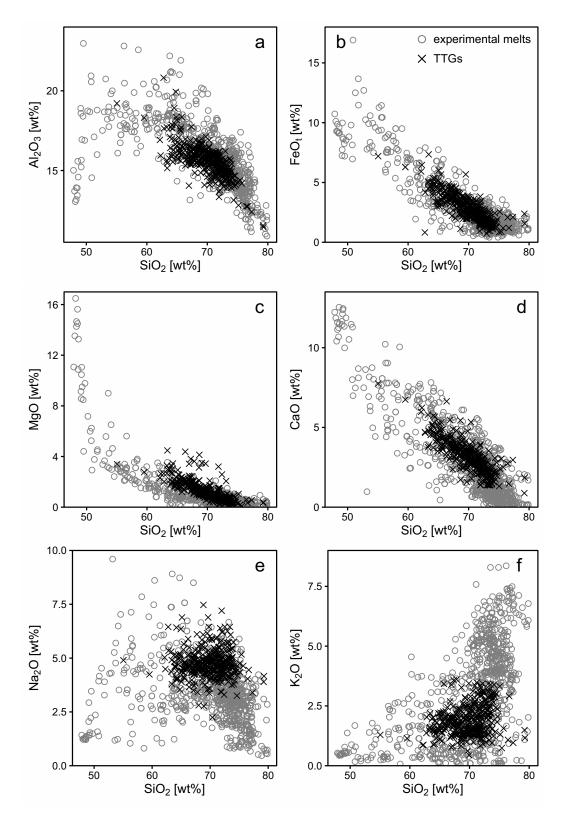


Figure 5.16: Harker diagrams displaying major elements of natural TTGs (Nutman et al., 1999; Moyen, 2011; Laurent et al., 2014; O'Neil and Carlson, 2017; Johnson et al., 2019) and the experimental glasses used for the model calibration.

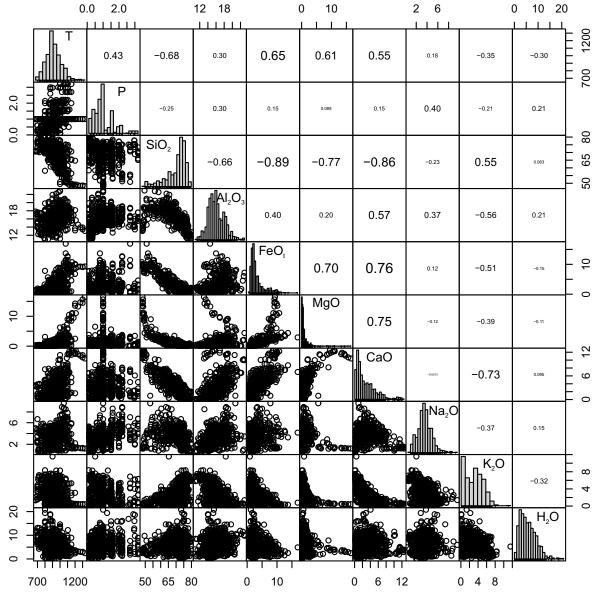


Figure 5.17: Correlation matrix for hydrous melting experiments from (Conrad et al., 1988; Vielzeuf and Holloway, 1988; Beard and Lofgren, 1991; Holtz and Johannes, 1991; Patiño Douce and Johnston, 1991; Rapp et al., 1991; Skjerlie and Johnston, 1992; Skjerlie and Johnston, 1993; Sen and Dunn, 1994; Vielzeuf and Montel, 1994; Wolf and Wyllie, 1994; Gardien et al., 1995; Patiño Douce and Beard, 1995; Rapp and Watson, 1995; Skjerlie and Patiño Douce, 1995; Patiño Douce and Beard, 1996; Skjerlie and Johnston, 1996; Winther, 1996; Springer and Seck, 1997; Patiño Douce and Harris, 1998; Pickering and Johnston, 1998; Castro et al., 1999, 2000; Gardien et al., 2000; Koester et al., 2002; Skjerlie and Patiño Douce, 2002; Grant, 2004; Spicer et al., 2005; Patiño Douce, 2005; Sisson et al., 2005; Xiong et al., 2005; Alonso-Perez et al., 2009; Getsinger et al., 2009; Adam et al., 2012; García-Arias et al., 2012; Laurie and Stevens, 2012; Qian and Hermann, 2013; Hastie et al., 2016) with recalculated H₂O as shown in fig. 5.3. T is temperature in °C and P pressure in GPa. Pearson correlation coefficients are displayed in the upper right half of the matrix. The diagram was created via the *R* package *PerformanceAnalytics* by Peterson and Carl (2020).

CHAPTER 6

Conclusions

There are several aspects to consider when investigating the formation of TTGs. As discussed and shown in chapter 2, the composition of TTGs is the result of an interplay between partial melting, crystal fractionation and accumulation. Individual trace or major element ratios cannot be used to constrain processes. The Sr/Y ratio is a great example for this as it is primarily used to constrain the depth of TTG melt formation, however is sensitive to the fractionation of hornblende and/or accumulation of plagioclase which can be constrained by the Eu-anomaly.

For TTGs that do not appear to have been affected by crystal fractionation or accumulation, I calculated Ti saturated liquidus temperatures with a Ti solubility model that I calibrated based on an extensive literature database comprising rutile and ilmenite bearing melting experiments. The critical assumption of the approach is that the selected TTGs represent primary magmatic liquids. Ti solubility is described as a function of temperature, non bridging oxygen per tetrahedra (NBO/T) and the ratio of single to doubly charged cations (Na+K)/(Fe+Mg+Ca). Resulting temperatures are on average between 750 to 900 °C. Many TTGs have temperatures that are below liquidus temperatures that would be expected based on their major element composition. Consequently these TTGs were most likely not saturated in either rutile or ilmenite during melt formation. This has an effect on the interpretation of the Nb depletion present in TTGs, irrespective if they could have been saturated with a Ti phase or not. The depletion must be either inherited from earlier processes or caused by other Ti-bearing minerals, for example amphibole or mica. The phases ilmenite and rutile might have played only a subordinate role in shaping the trace element pattern of TTGs, hence their saturation at liquidus conditions is uncertain. An implication of the low Ti saturated liquidus temperatures is that melt formation must have been hydrous with 8-12 wt% dissolved H_2O within the produced melt. At melting degrees of 20 - 30 % this translates to a H_2O content of the source rock between 2 - 4 wt%. Hydrous low degree melting by amphibole breakdown can not account for these elevated concentrations, as the source would be either monomineralic, or a mixture of hydrous minerals which is implausible as it does not match the required TTG source composition. Hence fluid flux melting is a more realistic scenario. The requirement for high H_2O contents is confirmed by the SVR based prediction model. The model estimates between 9-12 wt% H₂O required to reach Ti saturated liquidus conditions.

In crystallisation experiments and thermodynamic modelling conducted on the Eoarchean Nuvvuagittuq granodiorite PC-103 (chapter 4), the importance of H_2O is apparent for the evolution/differentiation paths of TTGs. The suppression of feldspar crystallisation under hydrous conditions (>5 wt%) allows for crystal fractionation from tonalitic to trondhjemitic compositions by maintaining an almost constant K_2O/Na_2O ratio. Under dryer conditions, the suite evolves towards granodioritic to granitic compositions by feldspar fractionation dominating the liquid line of descent. The amount of H_2O present might therefore be one of the major differences compared to post-Archean magmatic systems.

A further necessity for the generation of TTG liquids is the availability of a K₂O poor source.

The calibration of an interdependent T-P-H₂O model was unsuccessful due to several reasons. One source of error is the dataset of experiments used to calibrate the model. Temperature and pressure have an artificial correlation, the H₂O dissolved in glasses is not well constrained and the variety of starting materials overlay major element variations caused by pressure and H₂O. The second source of error, or limitation of the model is its inability to differentiate appropriately with these effects as it is of pure statistical nature. However, the temperature prediction based on major elements and H₂O content works sufficiently. By using both models together, the most probable formation temperature of TTGs is between 850-1050 °C at approximately 8 wt% H₂O.

In respect of the geodynamic environment in which TTGs form, a subduction-like setting is most plausible based on the investigation in this thesis. While it is not possible to directly infer a geodynamic process from the results, the constraints set by them require an elevated amount of H₂O. Especially the formation of trondhjemites requires more H₂O than possibly provided by dehydration melting. Subduction is a convenient mechanism to transport H₂O to the region of melt formation. However, where structural field relations refute a convergent setting, as in the Pilbara, H₂O must have had a different source.

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